

October 8, 2024

Mr. Michael B. Leat Iowa Department of Natural Resources Land Quality Bureau Solid Waste Section 502 East 9<sup>th</sup> Street Des Moines, Iowa 50319

RE: Industrial Monofill Permit Renewal Application Continental Cement Davenport Plant CKD Landfill 301 East Front Street Buffalo, Iowa IDNR Permit #82-SDP-16-97P

Dear Mr. Leat:

Blackstone Environmental, Inc. (Blackstone), on behalf of Continental Cement Company, LLC (Continental) is pleased to present this Monofill Permit Renewal Application for the Continental Davenport Plant Cement Kiln Dust (CKD) Landfill. The landfill is operated under Iowa Department of Natural Resources (IDNR) Permit Number 82-SDP-16-97P, Revision #4, which was issued on May 1, 2023, and is the fourth revision to the permit issued on January 6, 2022 and is set to expire on January 6, 2025. This Renewal Application has been prepared in general accordance with 567 Iowa Administrative Code 115.

We appreciate your consideration of the attached. Please feel free to contact either of the undersigned if you have any questions or need further information.

Respectfully, BLACKSTONE ENVIRONMENTAL, INC.

Maren Williams

Maren Williams, EIT Project Engineer

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Kyle Kukuk, P.E. Senior Project Manager



## **Industrial Monofill Permit Renewal Application**

Continental Cement Davenport Plant CKD Landfill 301 East Front Street Buffalo, Iowa IDNR Landfill Permit Number 82-SDP-16-97P

> Prepared for: Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by: Blackstone Environmental, Inc. 16200 Foster Street Overland Park, Kansas 66085



October 8, 2024

INDUSTRIAL MONOFILL PERMIT APPLICATION CONTINENTAL CEMENT DAVENPORT PLANT CKD LANDFILL 301 EAST FRONT STREET BUFFALO, IOWA IDNR LANDFILL PERMIT NUMBER 82-SDP-16-97P

Prepared for: Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by:

Maren Williams

Maren Williams, EIT Project Engineer

Reviewed by:

· Vhal

Kyle Kukuk, P.E. Senior Project Manager

### TABLE OF CONTENTS

Sectio	onPage
	E OF CONTENTS
1.2	Site Activities 1
1.3	Permit Renewal 1
<b>2.0</b> 2.1	EXECUTIVE SUMMARY
2.2	Summary of Permit Revisions2
2.	2.1 Permit Revision #1
2.	2.2 Permit Revision #2
2.	2.3 Permit Revision #3
2.	2.4 Permit Revision #4
2.3	Summary of Permit Amendments 4
4.0 5.0	SITE BOUNDARIES
7.0 8.0 9.0 PLAN	EQUIPMENT CONTINGENCY PLAN
10.0	SITE OPERATIONS PLAN (SOP) AND DESIGN PLANS
	CLOSURE/POST CLOSURE PLAN
-	EXPLOSIVE GAS CONTROL PLAN
	CERTIFICATION

#### FIGURES

- Site Topographic Vicinity Map
   Site Plan
   Landfill Location
   Wetland Map

#### APPENDICES

- Industrial Monofill Permit Application Form 50 Α
- Legal Description В
- C Hydrologic Monitoring System Plan
   D Site Operations Plan
   E Facility Development Drawings
   F Closure/Post Closure Plan

- Emergency Response and Remedial Action Plan G
  - H Comprehensive Waste Plan



#### 1.0 INTRODUCTION

#### 1.1 Site Location and Background

Continental Cement Company, LLC (Continental) is located at 301 Front Street in Buffalo, Scott County, Iowa (Site). Quarrying and manufacturing of Portland cement products have been conducted at the Continental facility since 1924 and other uses are not anticipated in the future. The cement manufacturing process includes the heating of limestone with silica, alumina, and iron minerals to form clinker. The clinker (nodules of sintered material) is ground into a fine powder and mixed with gypsum to form cement. As part of the manufacturing process, removal of particulate is required to control the composition of the cement product. This material is known as cement kiln dust (CKD). Continental operates an approximately 20-acre monofil for the disposal of CKD. The southern portion of the landfill has been filled to original grade and closed in general accordance with the requirements of the Iowa Department of Natural Resources (IDNR) Permit Number 82-SDP-15-96C. An active landfill disposal cell (Phase II) is operated under IDNR Permit Number 82-SDP-16-97P. The amount of CKD per day disposed at the landfill varies by day. Continental continues to operate with the overall goal of minimizing landfilled CKD and beneficially reusing material when able.

#### 1.2 Site Activities

Placement of CKD material has continued in the Phase II area since issuance of the current permit. These activities are planned to continue until the Phase II area is to grade.

The Phase I landfill area was closed in late 2005.

#### 1.3 Permit Renewal

A Completed Industrial Monofill Permit Application Form 50 is attached in Appendix A as well as required plans and specifications.

#### 2.0 EXECUTIVE SUMMARY

#### 2.1 Summary of Modifications to Approved Plans and Specifications

Modifications to the permit were approved on:

- Revision #1 April 20, 2022
- Revision #2 August 25, 2022
- Revision #3 November 11, 2022
- Revision #4 May 1, 2023



#### 2.2 Summary of Permit Revisions

The following provides a summary of the permit revisions that have occurred since the permit issuance date of January 6, 2022. There has been a total of four (4) revisions to the permit with the most recent version issued on May 1, 2023, by IDNR.

#### 2.2.1 Permit Revision #1

Permit Revision #1 was issued on April 20, 2022. A summary of the changes to the Special Provisions from that date are as follows:

- 1. Updated the Licensed Design Engineer to:
  - a. Eric Sonsthagen, P.E.
    Blackstone Environmental, Inc.
    P.O. Box 540458
    Omaha, NE 68154
    Phone: 402/208-2014
    Iowa License Number: 248444
- 2. Special Provision No. 1 No changes to the January 6, 2022, permit.
- 3. Special Provision No. 2 No changes to the January 6, 2022, permit.
- 4. Special Provision No. 3 No changes to the January 6, 2022, permit.
- 5. Special Provision No. 4 No changes to the January 6, 2022, permit.
- 6. Special Provision No. 5 No changes to the January 6, 2022. permit.
- 7. Special Provision No. 6 No changes to the January 6, 2022, permit.

#### 2.2.2 Permit Revision #2

Permit Revision #2 was issued on August 25, 2022. A summary of the changes to the Special Provisions from that date are as follows:

- 1. Special Provision No. 1 No changes to the April 20, 2022, permit, Revision #1.
- 2. Special Provision No. 2 No changes to the April 20, 2022, permit, Revision #1.
- 3. Special Provision No. 3 No changes to the April 20, 2022, permit, Revision #1.
- 4. Special Provision No. 4b was modified. The revision stated, "The Groundwater Remedial Action Mitigation Plan (RAMP; doc #103289) dated May 31, 2022 and amended by the response letter dated August 12, 2022 (doc #103879), both submitted by Blackstone Environmental, was approved on August 25, 2022 and are incorporated into this permit. This plan has been designed to alleviate or reduce contamination to the fullest extent possible at site monitoring points MW-2CR, MW-3L, MW-4, MW-4L, MW-5, MW-7, MW-11, MW-12, MW-14, and MW-18, in accordance with 567 IAC 115.26(9)"d" and as described in the IDNR letter dated September 9, 2020 (doc #98407). The RAMP includes ongoing evaluations of alternatives to the disposal of cement kiln dust in this landfill. The permit holder shall include updates of these evaluations in the semiannual engineering inspection reports required in the permit's general provisions."
- 5. Special Provision No. 5 No changes to the April 20, 2022, permit, Revision #1.



- Special Provision No. 6 was modified. The revision stated, "The permit holder shall close the landfill site in accordance with the Closure, Post Closure Plan (doc #103290) dated May 31, 2022, as submitted by Blackstone Environmental and approved on August 25, 2022."
- 7. Special Provision No. 6a was removed from the April 20, 2022, permit, Revision #1 because the Closure, Post Closure Plan was updated (doc #103290). No. 6b-d from the April 20, 2022, permit, Revision #1 were relabeled as No. 6a-c, respectively.

#### 2.2.3 *Permit Revision #3*

Permit Revision #3 was issued on November 21, 2022. A summary of the changes to the Special Provisions from that date are as follows:

- 1. Special Provision No. 1 No changes to the August 25, 2022, permit, Revision #2.
- 2. Special Provision No. 2 No changes to the August 25, 2022, permit, Revision #2.
- 3. Special Provision No. 3f was added and stated, "The UL Replacement CQA Certification Report, dated October 24, 2022 (doc #104643), as submitted by Blackstone Environmental was approved on November 21, 2022 and incorporated into the permit. This report documents the replacement of leachate piezometers UL-2 and UL-3, as a required component of the Remedial Action Mitigation Plan described in special provision #4b."
- 4. Special Provision No. 4 No changes to the August 25, 2022, permit, Revision #2.
- 5. Special Provision No. 5 No changes to the August 25, 2022, permit, Revision #2.
- 6. Special Provision No. 6 No changes to the August 25, 2022, permit, Revision #2.

#### 2.2.4 Permit Revision #4

Permit Revision #4 was issued on May 1, 2023. A summary of the changes to the Special Provisions from that date are as follows:

- 1. Special Provision No. 1 No changes to the November 21, 2022, permit, Revision #3.
- 2. Special Provision No. 2 No changes to the November 21, 2022, permit, Revision #3.
- 3. Special Provision No. 3b was modified regarding updated landfill design plans. The revision stated, "The requirement to submit updated landfill design plans is placed on hold due to the permit holder's ongoing evaluations of alternatives to disposal of cement kiln dust. IDNR shall reinstitute this requirement if we determine that either (1) insufficient progress regarding these evaluations is made, (2) the evaluation concludes that on-site disposal is the preferred management method, or (3) the groundwater remedial action mitigation plan (special provision #4b) goals are not met. If required, the revised design must include closure and/or hydraulic isolation of the current disposal area with a high performance final cover that minimizes infiltration, and for future cells to include a flexible membrane layer and more efficient leachate collection layer to improve overall liner efficiency."
- 4. Special Provision No. 4 No changes to the November 21, 2022, permit, Revision #3.



- 5. Special Provision No. 5 No changes to the November 21, 2022, permit, Revision #3.
- 6. Special Provision No. 6 No changes to the November 21, 2022, permit, Revision #3.

#### 2.3 Summary of Permit Amendments

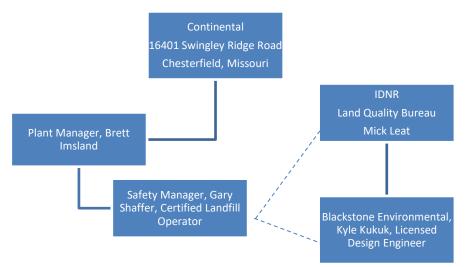
Permit Amendments have not been conducted since the issuance of the permit dated January 6, 2022.

#### 3.0 SITE BOUNDARIES

The Site is shown on Figure 1 and is located approximately four miles west of Davenport, Iowa within Sections 14, 15, 22, and 23 of Township 77 North, - Range 2 East (Buffalo Township), Scott County, Iowa. The development fill area is located between N 1500 to N 2300 and W 300 to E 500. The facility has been in operation, under various ownership, from 1924 for the quarrying of limestone rock and the manufacture of Portland cement. The CKD landfill is located in an inactive portion of the quarry approximately 2,000 feet east of the active quarry area and comprises approximately 20 acres. Figure 2 is a map of the Continental facility that includes the zoning and land use, haul routes, homes and buildings within a half-mile, and section lines and legal boundaries. Airports or runways are not located near the Site. Figure 3 is the landfill location and layout which includes monitoring well locations and cell boundaries. Figure 4 is a wetland map of the area.

#### 4.0 ORGANIZATIONAL CHART

The Site is owned and operated by Continental. Mr. Brett Imsland is the Plant Manager and is the landfill operator responsible for the overall operation of the Continental facility. The certified landfill operator is Mr. Gary Shaffer, Continental Safety Manager. Mr. Shaffer, as well as other personnel, report to Mr. Imsland. An organization chart is below.



The Licensed Design Engineer for Continental should be revised to:



Kyle Kukuk, P.E., Iowa License Number: 22790 Blackstone Environmental, Inc. 16200 Foster Street Overland Park, Kansas 66085 913-495-9990

#### 5.0 DISPOSAL PROCESS

The CKD area operates in a consistent and predictable manner because the source and nature of the CKD are known. Other waste materials are not allowed in the area.

The CKD is captured with air quality control equipment and stored in a silo located south of the landfill. When the silo is filled, the CKD is wetted to control dust and transported by haul truck to the landfill where it is dumped. End loaders and bulldozers level and push the piles as needed. In general, the landfill is raised uniformly over the surface. The CKD is placed by dumping the trucks onto the landfill working face. The placement is determined by the landfill operator on a weekly basis.

The CKD is hauled from the silo on an on-site gravel access road, across East Front Street, and then again on an on-site gravel access road to the landfill. The gravel access roads have speed limits and are wetted as necessary. East Front Street also has a speed limit. Continental personnel are responsible for maintaining the access roads in a suitable condition for traffic by vehicles.

Due to the cementitious nature of the conditioned CKD, the material tends to bind together when placed at the landfill forming a relatively uniform and solid deposit. The material is able to stand at a relatively steep angle of repose with negligible risk of slumping or slope failure. Further, the material is relatively impervious thereby reducing the likelihood of saturation which could reduce the shear strength and lead to slope instability.

Employees with duties associated with the storage, handling, transport, or disposal of CKD are trained to place CKD in a manner which will reduce the likelihood of slope failures, waste shifts, and waste subsidence. Transport vehicle drivers are instructed to place material at a safe distance back from the edge of the active cell to avoid surcharging the edge of the cell. Accumulated material is periodically pushed into the active cell with earthmoving equipment. The landfill is also inspected weekly so that situations which would lead to mass movement of waste are avoided or quickly corrected.



#### 6.0 EQUIPMENT PLAN

Generally, end loaders and bulldozers are used for placement, compaction, and cover of CKD. Other equipment is available for the operators as needed from the maintenance building located south of the landfill.

#### 6.1 Equipment

The table below details the equipment to be used, capacities, and expected loads.

Equipment	Capacity	Expected Loads
End loader	12 yards	12 yards
Haul trucks	60 tons	60 tons
Bulldozer	none	none
Leachate Pump	20 gallons per minute	20 gallons per minute

#### 7.0 EQUIPMENT CONTINGENCY PLAN

In the event of equipment breakdown, the equipment is either repaired where it broke down or the CKD is removed from the equipment with an excavator and placed into another operating vehicle for disposal.

During maintenance downtime of equipment, Continental has other equipment stored in the maintenance building that will be used.

In the event of a fire in equipment or vehicles, the fire would be extinguished using fire extinguishers located in each vehicle. If the equipment is drivable and safe to be driven after the fire has been extinguished, the CKD will be disposed at the landfill. If the equipment is not drivable/safe, the CKD will be removed from the equipment with an excavator and placed into another operating vehicle for disposal.

#### 8.0 PROOF OF OWNERSHIP

A copy of the legal description is provided in Appendix B.

# 9.0 HYDROGEOLOGIC INVESTIGATION REPORT/HYDROLOGIC MONITORING SYSTEM PLAN

A Hydrogeologic Investigation Report has not been prepared. Components of this document were included in the Hydrologic Monitoring System Plan (HMSP) and Revised HMSP referenced below.

An HMSP dated March 29, 2021 and Revised HMSP dated April 19, 2021 were prepared by Blackstone and submitted to IDNR. The IDNR approved the Revised HMSP in Permit Revision # 4 dated April 27, 2021. A copy of the Revised HMSP is included in Appendix C.



#### 10.0 SITE OPERATIONS PLAN (SOP) AND DESIGN PLANS

An SOP dated August 27, 2021 and Revised SOP dated November 5, 2021 were prepared by Blackstone and submitted to IDNR. There have been no modifications to the SOP since that time. A copy of the November 5, 2021. Revised SOP is included in Appendix D.

Changes were made to the facility closure drawings and submitted with the Closure, Post-Closure Plan prepared by Blackstone and dated May 31, 2022. Copies of the facility development drawings from the previous permit and May 31, 2022, closure drawings are included in Appendix E.

#### 11.0 CLOSURE/POST CLOSURE PLAN

Changes were made to the Closure/Post Closure Plan for the Site with the issuance of an updated Closure, Post-Closure Plan prepared by Blackstone on May 31, 2022. A copy of the Closure, Post-Closure Plan is included in Appendix F. The updated plan includes landfill closure design drawings.

#### 12.0 EXPLOSIVE GAS CONTROL PLAN

An Explosive Gas Control Plan is not applicable to the Site.

#### 13.0 EMERGENCY RESPONSE AND REMEDIAL ACTION PLAN (ERRAP)

Continental has updated the ERRAP as of September 2024. A copy of the updated ERRAP is included in Appendix G.

#### 14.0 COMPREHENSIVE WASTE MANAGEMENT PLAN

Continental has a Comprehensive Waste Management Plan from June 1997. A copy of the Comprehensive Waste Management Plan is included in Appendix H.



#### 15.0 CERTIFICATION

I hereby certify that this engineering document was prepared by me or under my direct supervision and that I am a duly licensed Professional Engineer under the laws of the State of Iowa.

Kyle Kukuk, PE

24 Date 10/8

Reg. No. 22790

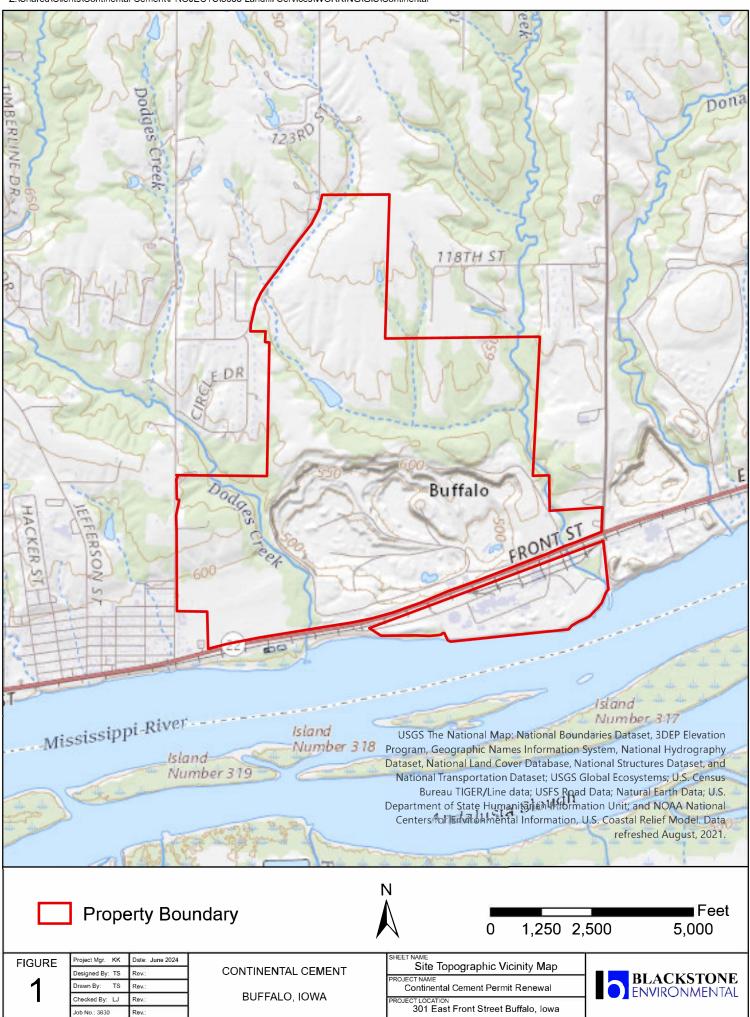
My license renewal date is December 31, 2025.



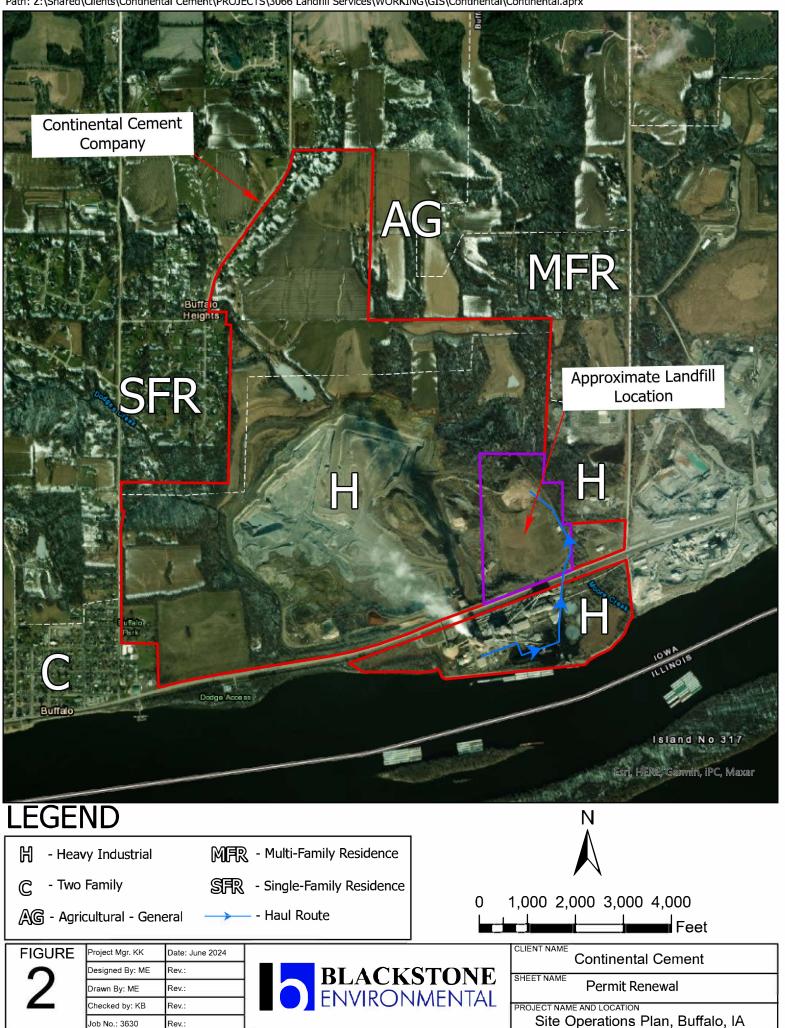
**FIGURES** 

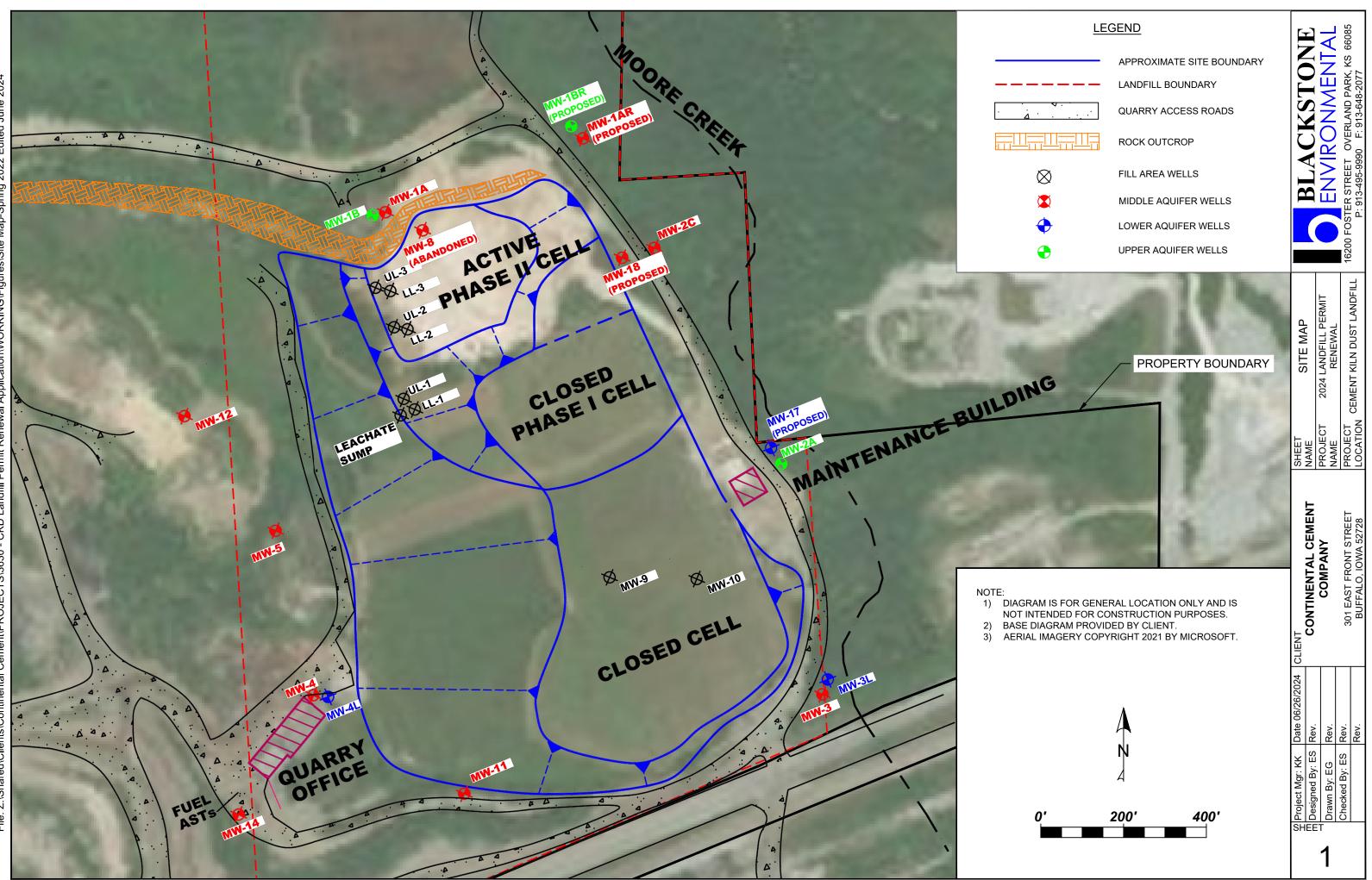
- Site Topographic Vicinity Map
   Site Plan
- 3 Landfill Location
- 4 Wetland Map

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### U.S. Fish and Wildlife Service National Wetlands Inventory

### Continental Cement CKD Landfill



- Estuarine and Marine Wetland

Estuarine and Marine Deepwater

- Freshwater Forested/Shrub Wetland
  - **Freshwater Pond**

Other Riverine Wetlands Mapper web site.



**APPENDIX A** 

**Industrial Monofill Permit Application Form 50** 

IOWA DEPARTMENT OF Municipal Solid PERMIT APPLICA	Waste	e Landfil		ÞRR
New Permit X Permit Renewal (permit number) 82 - SI	DP- 10	5	- 97	MLF
Closure Permit	<u> </u>	, 	- 51	IVILI
SECTION 1: PERMIT APPLICATION REQUIREMENTS				
Owner of site				
Name: Continental Cement Company, LLC			Phone:	636-532-7440
Address: 16401 Swingley Ridge Road, Suite 320			Fax:	
City, State, Zip: Chesterfield, MO 63017	E-mail:	Brett.Imsla	nd@conti	nentalcement.com
Certified Operator Responsible for Operation at Facility	e.			
Name: Gary Shaffer			Phone:	563-328-6204/563-328-6234
Address: 301 East Front Street			Fax:	
City, State, Zip: Buffalo, IA 52728	E-mail:	Gary.Shaffe	er@contin	entalcement.com
Permit Applicant				
Name: Continental Cement Company, LLC			Phone:	563-328-6236
Address: 301 East Front Street			Fax:	
City, State, Zip: Buffalo, IA 52728	E-mail:	Shawn.Mag	es@conti	nentalcement.com
Design Engineer (PE)				
Name: Kyle Kukuk			Phone:	913-495-9990
Address: 16200 Foster Street			Fax:	
City, State, Zip: Overland Park, KS 66085	E-mail:	kkukuk@bla	ackstone-	env.com
lowa Engineer License #: 22790 Expiratio		12/31/2024		
Responsible Official for the Facility				_
Name: Brett Imsland/Continental Cement Company, LLC			Phone:	563-328-6236
Address: 301 East Front Street			Fax:	
City, State, Zip: Buffalo, IA 52728	E-mail:	Brett.imsla		nentalcement.com
Agency and Responsible Official of Agency Served (if any)	E man			
Nama			Phone:	
			Fax:	
City Chata Zin	E-mail:		1 874	
Facility	e man.			
Name: Continental Cement Company, LLC				
Address: 301 East Front Street	City	State, Zip:	Buffal, IA	52728
Legal Description:		State, Lipt	burran	
See attached				
······································				
Landfill is part of the following solid waste comprehensive planning area:         Planning Area Name:       Continental Cement Davenport Plant CKD Landfill				
Date of Last Approved Plan: 12/21/2021				
Service area of the landfill (include unincorporated areas and out o	of state ge	nerators):		
Continental Cement Plant CKD waste only				
Population Served:				

#### SECTION 2: PERMIT APPLICATION SUPPORTING DOCUMENTATION

#### PLANS AND SPECIFICATIONS

Checking the appropriate boxes below certifies that the documents submitted in conjunction with this application form are complete and in compliance with the applicable chapters of the Iowa Administrative Code. While some of the documents below may have been submitted previously, updated copies of each are required to be provided with each permit renewal application, unless a prior document remains current and is identified by Doc ID#, Section, and Page.

	Required Plans and Specifications
X	<ul> <li>Executive Summary</li> <li>An executive summary shall address the following:</li> <li>Summary of modifications, if any, to the approved plans and specifications that occurred during the current permit cycle.</li> <li>Summary of each special provision of the current permit to determine if it is to remain the same, be revised or be removed.</li> <li>Provide documentation and certification as required for new permit amendment requests, if any.</li> <li>Provide documentation and certification as required for new variance requests from Iowa Administrative Code requirements, if any.</li> </ul>
X	An organizational chart in accordance with Iowa Administrative Code 567 paragraph <u>113.5(1)"b"</u> . No Revision Required - See Doc ID#, Section, and Page:
X	A site exploration and characterization report for the facility that complies with the requirements of subrule <u>113.6(4)</u> . No Revision Required - See Doc ID#, Section, and Page:
X	Design plans and specifications for the facility, and quality control and assurance plans, that comply with the requirements of rule <u>113.7(455B)</u> . No Revision Required - See Doc ID#, Section, and Page:
X	A development and operations (DOPS) plan for the facility, an emergency response and remedial action plan (ERRAP), and proof of MSWLF Operator Certification that comply with the requirements of rule <u>113.8(455B)</u> . No Revision Required - See Doc ID#, Section, and Page:
X	An environmental monitoring plan that complies with the requirements of rules <u>113.9(455B)</u> and <u>113.10(455B)</u> . No Revision Required - See Doc ID#, Section, and Page:
X	The project goals and time lines, and other documentation as necessary to comply with subrule <u>113.4(10)</u> and other requirements of the Department if an RD&D permit is being requested or renewed. No Revision Required - See Doc ID#, Section, and Page:
X	Proof of financial assurance in compliance with rule <u>113.14(455B)</u> . No Revision Required - See Doc ID#, Section, and Page:
X	A closure and postclosure plan that complies with the requirements of rules <u>113.12(455B)</u> and <u>113.13(455B)</u> . No Revision Required - See Doc ID#, Section, and Page:
X	Comprehensive plan requirements. Attach a copy of the most recent comprehensive plan approval or amendment letter. No Revision Required - See Doc ID#, Section, and Page:
X	Household Hazardous Materials (HHM) collection certification. If applicable, include a plan for HHM temporary collection and storage in accordance with IAC 567 <u>Chapter 123</u> (455B, 455D, 455F). No Revision Required - See Doc ID#, Section, and Page:

In addition to the documents required above, the permit holder shall comply with the implementation plan requirements of subrule  $\underline{113.2(9)}$ , the public notice requirements of subrule  $\underline{113.4(12)}$ , and the record-keeping and reporting requirements of rule  $\underline{113.11(455B)}$ .

If the department finds the permit application information to be incomplete, the department shall notify the applicant of that fact and of the specific deficiencies. If the applicant fails to correct the noted deficiencies within 30 days, the department may reject the application and return the application materials to the applicant. The applicant may reapply without prejudice.

SECTION		

Signature of Permit Applicant: Bchul	Date: 10/8/214
Printed Name: BRETT IMSUMM	Title: PLANT MANAGOR

Applications for sanitary disposal projects must be accompanied by the plans, specifications and additional information required by the applicable solid waste rules under Iowa Administrative Code.

Send completed applications with attached information to the DNR project officer via email or file sharing platform.

For questions concerning this application contact Brian Rath at 515-537-4051, brian.rath@dnr.iowa.gov



**APPENDIX B** 

Legal Description

#### CONTINENTAL CEMENT COMPANY, L.L.C.

#### **ASSISTANT SECRETARY'S CERTIFICATE**

#### May 9, 2018

The undersigned, being the duly appointed and acting Assistant Secretary of Continental Cement Company, L.L.C., a Delaware limited liability company (the "<u>Company</u>"), hereby certifies, as of the date hereof, on behalf of the Company, solely in such person's capacity as Assistant Secretary of the Company and not in such person's individual capacity, as follows:

- Pursuant to that certain Asset Purchase Agreement, dated as of April 16, 2015, by and among the Company, Lafarge North America, Inc., a Maryland corporation ("Seller") and certain other parties, as guarantors for the Company, the Company purchased from Seller and Seller sold to the Company certain assets of Seller, including, among other assets, (a) a cement plant located in Buffalo, Iowa (the "Cement Plant"), (b) a quarry located in Davenport, Iowa (the "Quarry") and (c) a cement distribution terminal located in West Des Moines, Iowa (the "Terminal"), in each case more particularly described on the attached <u>Exhibit A</u> (collectively, the "Davenport Properties"), each of which are used in the business of (i) mining aggregates at the Quarry and (ii) producing, marketing, distributing and selling portland cement and related products at or from the Cement Plant and the Terminal (the "Transferred Business").
- 2. The Company owns all right, title and interest in and to the Davenport Properties used in connection with the Transferred Business.

[Signature page follows]

IN WITNESS WHEREOF, the undersigned has hereunto set his hand on behalf of the Company as of the date first written above.

1/ By:

Name: Chris Gaskill Title: Assistant Secretary

#### EXHIBIT A

#### **Davenport Properties**

#### WEST DES MOINES

THAT PART OF LOT ONE (1) OF THE WEST 854 FEET OF LOT F VALLEY FUNCTION; PART OF LOTS D, E, F AND THE VACATED STREET NORTH OF LOT E IN VALLEY JUNCTION, MORE PARTICULARLY DESCRIBED AS FOLLOWS;

A TRACT OF LAND LYING IN THE NORTHEAST QUARTER OF SECTION 15, TOWNSHIP 78 NORTH, RANGE 25 WEST OF THE FIFTH PRINCIPAL MERIDIAN, MORE PARTICULARLY DESCRIBED AS FOLLOWS. COMMENCING AT THE NORTHWEST CORNER OF LOT F OF THE RECORDED PLAT OF VALLEY JUNCTION, IOWA, WITH SAID NORTHWEST CORNER BEING ON THE LINE BETWEEN THE NORTH QUARTER CORNER AND THE CENTER OF SAID SECTION 15, AND HAVING AN ASSUMED TRUE BEARING SOUTH 0°00' WEST WITH ALL SUBSEQUENT BEARINGS REFERENCED THEREFROM; THENCE SOUTH 87°24' EAST ALONG THE NORTH LINE OF SAID LOT F, A DISTANCE OF 858.3 FEET; THENCE SOUTH 0°00' EAST, A DISTANCE OF 375 FEET; THENCE SOUTH 90°00' EAST, A DISTANCE OF 200 FEET TO THE POINT OF BEGINNING, SAID POINT ALSO BEING THE NORTHEAST CORNER OF PROPERTY DESCRIBED IN DEED DATED AUGUST 31,1953, FROM THE CHICAGO, ROCK ISLAND AND PACIFIC RAILROAD COMPANY TO PENN-DIXIE CEMENT CORPORATION AND AS RECORDED ON PAGE 207, BOOK 2631 IN THE OFFICE OF THE RECORDER OF POLK COUNTY, IOWA; THENCE SOUTH 0°00' EAST A DISTANCE OF 1016.34 FEET; THENCE SOUTH 30°54' WEST, A DISTANCE OF 172.84 FEET TO A POINT OF INTERSECTION WITH A LINE 200 FEET NORTHWESTERLY OF, AS MEASURED AT RIGHT ANGLES TO, AND PARALLEL WITH THE CENTERLINE OF THE MAIN TRACT OF SAID RAILROAD COMPANY; SAID LAST TWO BEARING LINES BEING THE TWO NORTHERLY LINES OF THE EASTERLY BOUNDARIES OF THE PROPERTY DESCRIBED IN SAID DEED DATED AUGUST 31, 1953; THENCE NORTH 47°44' EAST ALONG SAID LINE PARALLEL AND 200 FEET NORTHWESTERLY FROM THE CENTERLINE OF SAID MAIN LINE TRACK, A DISTANCE OF 557.65 FEET TO THE WESTERLY LINE OF ELEVENTH STREET IN THE CITY OF WEST DES MOINES, POLK COUNTY, IOWA; THENCE NORTH 39°46' WEST ALONG THE WESTLINE OF SAID ELEVENTH STREET; A DISTANCE OF 51.7 FEET; THENCE SOUTH 50°14' WEST ALONG SAID WEST LINE OF SAID STREET, A DISTANCE OF 10 FEET; THENCE NORTHERLY ALONG SAID WEST LINE OF SAID STREET, A DISTANCE OF 251.25 FEET ALONG A 316.5 FOOT RADIUS CURVE CONCAVE NORTHEASTERLY AND TANGENT TO THE FOLLOWING COURSE; THENCE NORTH 0°00' EAST ALONG THE SAID WEST LINE OF SAID STREET, A DISTANCE OF 529.87 FEET; THENCE NORTHERLY ALONG SAID WEST LINE OF SAID STREET ON A 256.5 FOOT RADIUS CURVE CONCAVE SOUTHWESTERLY AND

TANGENT TO THE PRECEDING COURSE, A DISTANCE OF 3.2 FEET; THENCE NORTH 90°00' WEST, A DISTANCE OF 197.8 FEET TO THE POINT OF BEGINNING.

AND

COMMENCING AT THE NORTH 1/4 CORNER OF SECTION 15-T78NR25 WEST OF THE 5TH P.M., WEST DES MOINES, POLK COUNTY, IOWA, THENCE S 0°00 E, ALONG THE WEST LINE OF THE N.E. 1/4 OF SAID SECTION 15, 185.15 FEET, TO THE SOUTH RIGHT-OF-WAY LINE OF THE MINNEAPOLIS AND ST. LOUIS RAILROAD, AS II IS PRESENTLY ESTABLISHED, THENCE S 87°26' 1/2" E, ALONG SAID SOUTH RIGHT-OF-WAY LINE, 87.12 FEET. THENCE CONTINUING S 87°26' 1/2" E, ALONG THE SOUTH RIGHT-OF-WAY LINE OF THE MINNEAPOLIS AND ST. LOUIS RAILROAD. AND PARALLEL WITH AND 50.0 FEET NORMALLY DISTANT FROM AND SOUTH OF THE CENTER LINE OF SAID MINNEAPOLIS AND ST. LOUIS RAILROAD, 567.53 FEET, TO THE POINT OF BEGINNING, THENCE CONTINUING S 87°26 1/2' E ALONG SAID SOUTH RIGHT-OF-WAY LINE OF THE MINNEAPOLIS AND ST. LOUIS RAILROAD, 200.2 FEET, THENCE S 0°00' E, PARALLEL TO AND 854.0 FEET EAST OF THE WEST LINE OF THE NE 1/4 OF SAID SECTION 15, 375.0 FEET, THENCE N 90°00 E, 200.0 FEET, THENCE S 0°00' E, PARALLEL WITH AND 1054.0 FEET EAST OF THE WEST LINE OF THE NE 1/4 OF SAID SECTION 15, 1018.8 FEET, THENCE S 30°44' W 173.86 FEET, TO THE NORTHWESTERLY RIGHT-OF-WAY LINE OF THE CHICAGO-ROCK ISLAND AND PACIFIC RAILROAD, AS IT IS PRESENTLY ESTABLISHED, THENCE S 47°42 1/2' W, PARALLEL WITH AND 200.0 FEET NORMALLY DISTANT FROM AND NORTHWESTERLY OF THE CENTER LINE OF THE MAIN LINE TRACK OF THE CHICAGO-ROCK ISLAND PACIFIC RAILROAD, AND ALONG THE NORTHWESTERLY RIGHT-OF-WAY OF SAID CHICAGO-ROCK ISLAND AND PACIFIC RAILROAD 420.63 FEET TO A POINT ON SAID NORTHWESTERLY RIGHT-OF-WAY OF THE CHICAGO-ROCK ISLAND AND PACIFIC RAILROAD, THENCE N 0°00' W, PARALLEL WITH AND 654.0 FEET EAST OF THE WEST LINE OF THE NE 1/4 OF SAID SECTION 15,1834.21 FEET TO THE POINT OF BEGINNING.

ALL BEING AN OFFICIAL PLAT, NOW INCLUDED IN AND FORMING A PART OF THE CITY OF WEST DES MOINES. POLK COUNTY, IOWA (EXCEPT THAT PART PLATTED AS SCHRODER INDUSTRIAL PARK).

DAVENPORT (BUFFALO, IOWA):

CHAIN ONE AND TWO:

PARCEL NO. 1: PART OF THE NORTHEAST QUARTER OF SECTION 23 IN TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING ON THE NORTH LINE OF SAID QUARTER SECTION AT A POINT 15 CHAINS AND 40 LINKS WEST OF THE NORTHEAST CORNER OF SAID NORTHEAST QUARTER; THENCE RUNNING WEST 24 CHAINS AND 60 LINKS TO THE NORTHWEST CORNER OF SAID QUARTER SECTION; THENCE SOUTH 40 CHAINS AND 55 LINKS TO THE NORTH BANK OF THE MISSISSIPPI RIVER; THENCE NORTH 66 DEGREES EAST, 1 CHAIN AND 43 LINKS TO A POINT ON SAID RIVER BANK; THENCE NORTH 84 DEGREES EAST, ON AND ALONG SAID RIVER BANK TO A POINT 24 CHAINS AND 1 LINK DISTANT; THENCE NORTH 37 CHAINS AND 47 LINKS TO THE PLACE OF BEGINNING.

EXCEPTING THEREFROM THE RIGHT OF WAY OF THE CHICAGO, ROCK ISLAND AND PACIFIC RAILWAY COMPANY; AND EXCEPTING PUBLIC HIGHWAYS.

PARCEL NO. 2: THE WEST ONE-HALF OF THE SOUTHEAST QUARTER OF SECTION 4, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M., SCOTT COUNTY, IOWA.

PARCEL NO. 3: LOTS 3 AND 4 OF THE SUBDIVISION OF THE ESTATE OF ELIAS MOORE, DECEASED, IN THE NORTHEAST QUARTER OF SECTION 23, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M. MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING AT A POINT IN THE EAST LINE OF SECTION 23 WHICH IS 8 CHAINS 59 LINKS SOUTH OF THE NORTHEAST CORNER OF SAID SECTION; THENCE RUNNING DUE WEST 15 CHAINS AND 40 LINKS; THENCE RUNNING DUE SOUTH 28 CHAINS AND 88 LINKS TO A STAKE STANDING ON THE BANK OF THE MISSISSIPPI RIVER; THENCE WITH THE MEANDERS OF THE SAID RIVER NORTH 84 DEGREES EAST 12 CHAINS AND 99 LINKS; THENCE WITH THE MEANDERS OF SAID RIVER NORTH 62 DEGREES EAST 2 CHAINS 82 LINKS; MORE OR LESS, TO A EAST LINE OF SAID SECTION; THENCE DUE NORTH ALONG THE EAST LINE OF SAID SECTION 26 CHAINS AND 13 LINKS TO THE PLACE OF BEGINNING, SUBJECT TO RAILROAD RIGHTS-OF WAY AND TO PUBLIC HIGHWAYS.

PARCEL NO. 4: THE EAST HALF OF THE SOUTHWEST QUARTER OF SECTION 14, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M. (DOES NOT INCLUDE PARCEL NO. 5 TRACT.)

PARCEL NO. 6: ALL THAT PART OF THE LAND INCLUDED IN THE PLAT OF THE ESTATE OF LEROY DODGE RECORDED IN PARTITION SUIT NO. 13437 IN THE DISTRICT COURT OF IOWA IN AND FOR SCOTT COUNTY, SAID PLAT INCLUDING LAND SITUATED IN SECTIONS 14, 15, 22 AND 23, TOWNSHIP 77 NORTH, RANGE 2 EAST, DESCRIBED AS FOLLOWS:

ALL OF LOT 1, ACCORDING TO SAID PLAT,

ALL OF LOT 2, ACCORDING TO SAID PLAT,

ALL OF LOT 3, ACCORDING TO SAID PLAT,

ALL OF THAT PART OF THE LOT 7, ACCORDING TO SAID PLAT, WHICH LIES SOUTH OF THE SECTION LINE BETWEEN SAID SECTIONS 15 AND 22,

ALL OF LOT 8, ACCORDING TO SAID PLAT, EXCEPT (A) THAT PART CONVEYED BY FRANK L. DODGE TO DAVENPORT PAVING BRICK & TILE COMPANY BY DEED RECORDED IN BOOK 57 OF LAND DEEDS, AT PAGE 490, (B) THAT PART CONVEYED BY FRANK L. DODGE TO HORACE H. CASS BY DEED RECORDED IN BOOK 48 OF LAND DEEDS, AT PAGE 283, AND IN BOOK 49 OF LAND DEEDS, AT PAGE 288, (C) THAT PART CONVEYED BY FRANK L. DODGE TO DORMAN & MOOREHEAD BY DEED RECORDED IN BOOK 52 OF LAND DEEDS, AT PAGE 83, (D) THAT PART THERETOFORE CONVEYED BY FRANK L. DODGE TO THE CHICAGO, ROCK ISLAND & PACIFIC RAILWAY COMPANY FOR STATION GROUNDS, (E) THAT PART CONVEYED BY DEWEY PORTLAND CEMENT COMPANY TO BUFFALO, IOWA, INDEPENDENT SCHOOL DISTRICT NO. 1 BY DEED RECORDED IN BOOK 90 OF LAND DEEDS, AT PAGE 45, AND (F) THAT PART CONVEYED BY DEWEY PORTLAND CEMENT COMPANY TO IOWA-ILLINOIS GAS AND ELECTRIC COMPANY BY DEED RECORDED IN BOOK 243 OF DEEDS, AT PAGE 238.

ALL OF LOT 9, ACCORDING TO SAID PLAT.

EXCEPTING THEREFROM THAT PORTION THEREOF CONVEYED TO THE CITY OF BUFFALO, IOWA, BY QUIT CLAIM DEED DATED JULY 22, 1980 AND RECORDED AS DOCUMENT #7502-81 IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

EXCEPTING THEREFROM THAT PORTION THEREOF CONVEYED TO THE STATE OF IOWA BY DEED DATED AUGUST 3, 1982 AND RECORDED AS DOCUMENT #12944-82 IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

PARCEL NO. 7: THAT 8 ACRE PORTION OF THE BED OF THE MISSISSIPPI RIVER WHICH LIES ADJACENT TO THE IOWA BANK OF SAID RIVER AND ADJACENT TO THE SOUTHERLY LINE OF GOVERNMENT LOTS TWO (2) AND THREE (3) OF SECTION TWENTY-THREE (23) OF TOWNSHIP SEVENTY-SEVEN (77) NORTH, RANGE TWO (2) EAST OF THE FIFTH PRINCIPAL MERIDIAN, MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING AT THE NORTHEAST CORNER OF SAID SECTION THENCE SOUTH 1740.10 FEET ALONG THE EAST LINE OF SAID SECTION: THENCE SOUTH 32 DEGREES 40 MINUTES WEST 1162.25 FEET TO THE NORTHEAST CORNER OF THE PRESENT SEA-WALL; THENCE ALONG THE FACE OF SAID SEA-WALL AND ALONG THE IOWA BANK OF SAID RIVER, SOUTH 33 DEGREES 48 MINUTES WEST 51.20 FEET; THENCE SOUTH 82 DEGREES 6 MINUTES WEST 455.70 FEET; THENCE SOUTH 81 DEGREES 39 MINUTES WEST 419.70 FEET TO THE WESTERLY END OF SAID SEA-WALL; THENCE SOUTH 85 DEGREES 16 1/2 MINUTES WEST 310 FEET TO THE POINT OF BEGINNING; THENCE SOUTH 85 DEGREES 16 1/2 MINUTES WEST 1100 FEET TO THE EASTERLY BANK OF A PRESENT CREEK OUTLET AT A POINT APPROXIMATELY 2930 FEET WEST OF AND 3000 FEET SOUTH OF THE NORTHEAST CORNER OF SAID SECTION; THENCE NORTHERLY ALONG SAID CREEK OUTLET BANK TO THE PRESENT IOWA SHORE LINE OF SAID RIVER AT ELEVATION OF 547 FEET ABOVE MEAN SEA-LEVEL; THENCE EASTERLY ALONG SAID SHORE LINE TO A POINT 1860 FEET WEST OF AND 2550 FEET SOUTH OF THE NORTHEAST CORNER OF SAID SECTION; THENCE SOUTHERLY 330 FEET ALONG THE WEST LINE OF THE

PREMISES OWNED BY DEWEY PORTLAND CEMENT COMPANY TO THE POINT OF BEGINNING.

#### EXCEPTIONS TO ALL THE ABOVE PARCELS

EXCEPT THAT PORTION DEEDED TO THE STATE OF IOWA BY DEED DATED AUGUST 31, 1982 AND RECORDED AS DOCUMENT NO. 12944-82 IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA, AND EXCEPTING THOSE LANDS CONDEMNED BY THE UNITED STATES OF AMERICA UNDER ORDER DATED AUGUST 11, 1939 AND RECORDED IN THE OFFICE OF THE SCOTT COUNTY, IOWA RECORDER AT BOOK 82 LAND DEEDS, PAGE 264 AND EXCEPTING THE TRACT CONVEYED TO THE CITY OF BUFFALO, IOWA BY DEED DATED JULY 22, 1980 AND RECORDED IN THE OFFICE OF THE SCOTT COUNTY, IOWA RECORDER AS DOCUMENT NO. 7502-81.

PARCELS NO. 10 AND 11: THE NORTHWEST QUARTER OF THE SOUTHWEST QUARTER OF SECTION 14, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M. ALSO DESCRIBED AS LOT 4 IN THE PARTITION OF THE ESTATE OF LEROY DODGE.

ALSO PART OF THE SOUTHEAST QUARTER OF SECTION 15, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5<sup>TH</sup> P.M., DESCRIBED AS COMMENCING AT THE NORTHEAST CORNER OF THE SOUTHEAST QUARTER OF SAID SECTION 15; THENCE WEST ON THE NORTH LINE OF SAID SOUTHEAST QUARTER OF SECTION 15, 15 CHAINS; THENCE SOUTH ON THE EAST LINE OF LOT 6, 20 CHAINS; THENCE EAST ON THE NORTH LINE OF LOT 1, 15 CHAINS; THENCE NORTH ON THE WEST LINE OF LOT 4, 20 CHAINS TO THE PLACE OF BEGINNING, WHICH REAL ESTATE IS ALSO DESCRIBED AS LOT 5 IN THE PARTITION OF THE ESTATE OF LEROY DODGE, DECEASED.

THE ABOVE DESCRIBED TRACTS OF REAL ESTATE ARE PARTICULARLY DESCRIBED BY SURVEY AS FOLLOWS:

BEGINNING AT THE NORTHEAST CORNER OF THE SOUTHEAST ¼ OF SECTION 15, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH PRINCIPAL MERIDIAN SAID POINT BEING ALSO THE NORTHWEST CORNER OF THE SOUTHWEST ¼ OF SECTION 14, TOWNSHIP AND RANGE AFORESAID, THENCE NORTH 89 DEGREES 52 MINUTES 14 SECONDS EAST ALONG THE NORTH LINE OF THE SAID SOUTHWEST

<sup>1</sup>⁄<sub>4</sub> OF SECTION 14 A DISTANCE OF 1331.0 FEET; THENCE SOUTH 0 DEGREES 42 MINUTES 49 SECONDS WEST 1331.34 FEET; THENCE NORTH 89 DEGREES 52 MINUTES 41 SECONDS WEST 2325.32 FEET TO THE SOUTHEAST CORNER OF LOT 44 DEVIL'S CREEK ESTATES ADDITION; THENCE NORTH 0 DEGREES 37 MINUTES 00 SECONDS EAST ALONG THE EAST LINE OF SAID DEVIL'S CREEK ESTATES ADDITION A DISTANCE OF 1325.43 FEET; THENCE SOUTH 89 DEGREES 52 MINUTES 53 SECONDS EAST 996.64 FEET TO THE PLACE OF BEGINNING. SITUATED IN BUFFALO TOWNSHIP, SCOTT COUNTY, IOWA.

#### CHAIN THREE:

PARCEL 12

THE NORTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 14; THE NORTH 16 ACRES OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 14; THE EAST 20 ACRES OF THE NORTHEAST QUARTER OF THE NORTHEAST QUARTER OF SECTION 15; EXCEPT THOSE PORTIONS THERE CONVEYED BY DOCUMENT NUMBERS 13993-82 AND 18202 83, RECORDS OF THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

ALSO, THE NORTH HALF OF THE SOUTHEAST QUARTER OF THE NORTHEAST QUARTER OF SECTION 15 EXCEPT THAT PART DESCRIBED AS COMMENCING AT A POINT ON SECTION LINE BETWEEN SECTIONS 14 AND 15; THENCE NORTH 20 FEET FROM CENTER LINE OF SOUTHEAST QUARTER OF THE NORTHEAST QUARTER OF SECTION 15; THENCE WEST 73 RODS, THENCE SOUTH 20 FEET; THENCE EAST 73 RODS TO THE PLACE OF BEGINNING, AND ALSO EXCEPTING THEREFROM THAT PORTION SOLD ON CONTRACT RECORDED AS DOCUMENT NUMBER 9033 75, RECORDS OF THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA, ALL IN TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH PRINCIPAL MERIDIAN.

CHAIN FOUR:

PARCEL 13

THE SOUTH 16 ACRES OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 14, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M. THE NORTH 8 ACRES OF THE SOUTH 24 ACRES, BEING LOT THREE OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 14, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M.

THE SOUTH 20 ACRES OF THE SOUTHEAST QUARTER OF THE NORTHEAST QUARTER OF SECTION 15, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M., EXCEPTING THEREFROM THE LAND INCLUDED IN LOTS 15 AND 16 IN BUFFALO HEIGHTS, AS APPEARS FROM THE PLAT OF SAID SUBDIVISION RECORDED IN BOOK 63 OF MISCELLANEOUS RECORDS, ON PAGE 291, IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

ALSO, A STRIP OF LAND COMMENCING AT THE NORTHWEST CORNER OF LAST TRACT ABOVE, THENCE WEST 73 RODS, NORTH 20 FEET, EAST 73 RODS, AND SOUTH 20 FEET TO THE PLACE OF BEGINNING.

EXCEPT THAT PORTION OF THE ABOVE DESCRIBED REAL ESTATE THAT WAS CONVEYED TO ALBERT VINER AND WINONA B. VINER BY THE QUIT CLAIM DEED DATED JANUARY 18, 1973, AND RECORDED AS DOC. #963-73 IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

#### CHAIN 5:

PARCEL 14

ALL THAT PORTION OF THE LAND INCLUDED IN THE PLAT OF THE ESTATE OF LEROY DODGE, RECORDED IN PARTITION SUIT NO 13437 IN THE DISTRICT COURT OF IOWA, AND SCOTT COUNTY, SAID PLAT INCLUDING LAND SITUATED IN SECTIONS 14, 15, 22 & 23 OF TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH PRINCIPAL MERIDIAN SCOTT COUNTY, IOWA, LYING SOUTH OF THE SOUTHERLY RIGHT-OF-WAY LINE OF IOWA STATE HIGHWAY 22 AND NORTH OF THE ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER, MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING AS A POINT OF REFERENCE AT THE NORTHEAST CORNER OF SECTION 23, TOWNSHIP 77 NORTH, RANGE 2 EAST;

THENCE SOUTH 00°1'51" WEST 1139.58 FEET ALONG THE EAST LINE OF THE NORTHEAST QUARTER OF SAID SECTION 23 TO A POINT ON THE SOUTHERLY RIGHT-OF-WAY LINE OF THE CHICAGO, ROCK ISLAND AND PACIFIC RAILROAD SAID RIGHT-OF-WAY LINE BEING 50 FEET IN PERPENDICULAR DISTANCE SOUTHEASTERLY FROM THE CENTERLINE OF THE WEST-BOUND MAIN LINE (NORTHERLY OF TWO) TRACK (FOR PURPOSES OF THIS DESCRIPTION, THE SAID EAST LINE OF THE NORTHEAST QUARTER OF SECTION 23 IS ASSUMED TO BEAR SOUTH 00°1'51" WEST);

THENCE SOUTH 68° 24''17" WEST 3916.36 FEET ALONG THE SAID SOUTHERLY RIGHT-OF-WAY LINE OF THE CHICAGO, ROCK ISLAND AND PACIFIC RAILROAD PARALLEL TO THE CENTERLINE OF THE SAID WEST-BOUND MAIN LINE TRACK, TO A POINT OF TANGENCY OF THE SAID RAILROAD RIGHT-OF-WAY LINE;

THENCE SOUTHWESTERLY 799.65 FEET ALONG THE SAID SOUTHERLY RIGHT-OF- WAY LINE OF THE CHICAGO, ROCK ISLAND AND PACIFIC RAILROAD ALONG A

5799.58 FEET RADIUS CURVE, CONCAVE NORTHWESTERLY, PARALLEL TO THE CENTERLINE OF THE SAID WEST-BOUND MAIN LINE TRACK TO THE POINT OF BEGINNING (THE CHORD OF SAID CURVE BEARS SOUTH 77° 22' 03" WEST 79.03 FEET);

THENCE SOUTH 61° 13'53" EAST 307.06 FEET TO A POINT AT THE ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER;

THENCE ALONG THE FOLLOWING DESCRIBED MEANDER OF THE ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER;

NORTH 87° 50'58" WEST 418.37 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 80° 10" 32" WEST 325.68 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 76° 47' 55" WEST 293.01 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 6° 40' 17" WEST 351.51 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 4° 36'47" WEST 74.21 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 36° 24'29" WEST 191.26 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 6° 56'22" WEST 250.63 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 6° 24' 17" WEST 245.81 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE NORTH 88° 05'04" WEST 276.83 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE NORTH 88° 51' 27" WEST 254.28 FEET ALONG THE SAID ORDINARY HIGH WATER POINT OF THE MISSISSIPPI RIVER TO A POINT;

THENCE NORTH 88° 06' 32" WEST 422.12 FEET ALONG THE SAID ORDINARY HIGH WATER POINT OF THE MISSISSIPPI RIVER TO A POINT.

#### SPECIAL WARRANTY DEEL

### KNOW ALL MEN BY THESE PRESENTS:

15.00 That MARTIN MARIETTA CORPORATION, a corporation organized and existing under the laws of the State of Maryland, in the consideration of the sum of one dollar and other valuable consideration in band paid does hereby CONVEY unto Davenport Cement Company, 35 TSLIA

The following described real estate situated in Scott County, Iowa:

Parcel No. 11 Part of the Northeast Quarter of Section 23 in Township 77 North, Range 2 Bast of the 5th P.M., more particularly described as follows:

Commencing on the North line of said quarter section at a point 15 chains and 40 links West of the Northeast corner of said Northeast Quarter; thence running West 24 chains and 60 links to the Northwest corner of said quarter section; thence South 40 chains and 55 links to the North bank of the Mississippi River; thence North 66 degrees East, 1 chain and 43 links to a point on said river bank; thence North 84 degrees East, on and along said river bank to a point 24 chains and 1 link distant; thence North 37 chains and 47 links to the place of beginning.

Excepting therefrom the right of way of The Chicago, Rock Island and Pacific Railway Company; and excepting public highways.

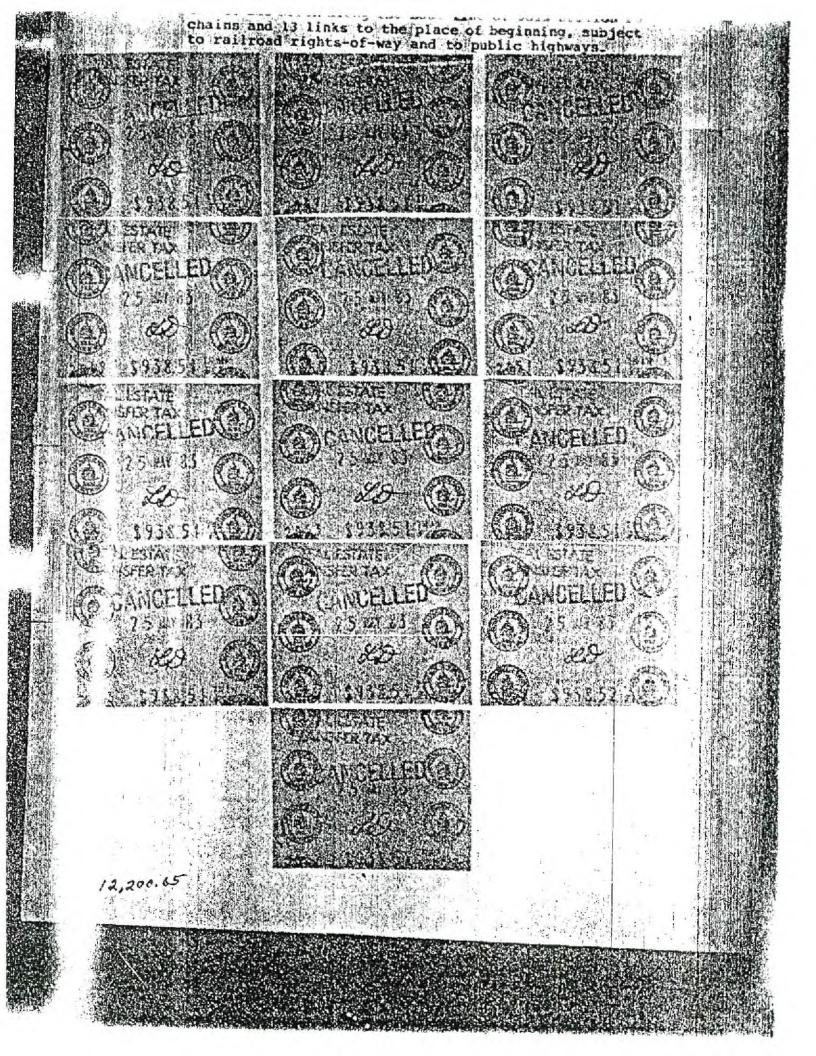
Parcel No. 2: The West one-half of the Southeast Quarter of Section 14, Township 77 North, Range 2 East of the 5th P.M., Scott County, Iowa:

2.5 1 1 4

Parcel No. 3: Lots 3 and 4 of the subdivision of the Estate of Elias Moore, deceased, in the Northeast Quarter of Section 23, Township 77 North, Range 2 East of the 5th P.M., more particularly described as follows:

Commencing at a point in the East line of Section 23 which is 8 chains 59 links South of the Northeast corner of said section; thence running due West 15 chains and 40 links; thence running due South 28 chains and 88 links to a stake standing on the bank of the Hississippi River; thence with the meanders of the said river worth 84 degrees East 12 chains and 99 links; theace with the meanders of said river North 62 degrees East 2 chains 82 links; more or less, to the East line of said section; thence due North along the East line of said Section 26 chains and 13 links to the place of beginning, subject to railroad rights-of-way and to public highways.

ST CHENNE



Parcel Nor 4. The East Half of the Southwest Quarter of Section 14. Township 77 North, Range 2 East of the 5th 2 P.N. (This Deed does not contain a Parcel 5 tract.)

Parcel No. 6. All that part of the land included in the plat of the Estate of LeRoy Dodge recorded in partition suit No. (13437 in the District Court of Iowa in and for Scott County, said plat including land situated in Sections 14, 15, 22 and 23, Township 77 North, Range 2 East, described as follows:

All of Lot 1. according to said plat.

All of Lot 2, according to said plat,

All of Lot 3, according to said plat,

All that part of the Lot 7; according to said Plat, which lies south of the section line between said Sections 15 and 22,

All of Lot 8, according to said plat, <u>EXCEPT</u> (a) that part conveyed by Frank L. Dodge to Davenport Paving Brick & Tile Company by deed recorded in Book 57 of Land Deeds, at page 490, (b) that part conveyed by Frank L. Dodge to Horace H. Cass by deed recorded in Book 48 of Land Deeds, at page 283, and in Book 49 of Land Deeds, at page 288, (c) that part conveyed by Frank L. Dodge to Dorman & Moorehead by deed recorded in Book 52 of Land Deeds, at page 83, (d) that part heretofore conveyed by Frank L. Dodge to The Chicago, Rock Island & Pacific Railway Company for station grounds, (e) that part conveyed by Dewey Portland Cement Company to Buffalo, Iowa, Independent School District No. 1 by deed recorded in Book 90 of Land Deeds, at page 45, and (f) that part conveyed by Dewey Portland Cement Company to Iowa-Illinois Gas and Electric Company by deed recorded in Book 243 of Deeds, at page 238.

All of Lot 9, according to said plat.

18 A

Excepting therefrom that portion thereof conveyed to the City of Buffalo, Iowa, by Quit Claim Deed dated July 22, 1980 and, recorded as Document #7502-81 in the office of the Recorder of Scott County, Iowa.

Excepting therefrom that portion thereof conveyed to the State of Towa by Deed dated August 3, 1982 and recorded as Document #12944-82 In the office of the Recorder of Scott County, Iowa.

Parcel No. 7. That 6 acre portion of the bed of the Mississippi River which lies adjacent to the Iowa Bank of said river and adjacent to the Southerly line of Government Lots Two (2) and Three (3) of Section Twenty-Three (23) of Township Seventy-seven (77) North, Range Two (2) East of the Fifth Principal Meridian, more particularly described as follows:

Commencing at the Northeast corner of said Section; thence south 1740.10 feet along the East line of said section; thence south 32 degrees 40 minutes west 1162.25 feet to the northeast corner of the present sea-wall; thence along the face of said sea-wall and along the Iowa

Bar Anna Anthen Contraction in the Line

12.11

Further subject to all other existing leases and rights of tenants in possession, existing railroad rights of way and depot grounds, easements, restrictions, reservations, or agreements of record, the rights of the public and the State of Iowa in roads and highways through the same, taxes and

1 garage

Further subject to the terms, provisions, covenants, conditions and restrictions contained in and rights and obligations created by a Lease Agreement dated May 21, 1971 and filed for record February 8, 1978 in the Office of the Scott County, Iowa Recorder as Document Number 2311-78 by and between Martin Marietta Corporation, Linwood Stone Products Company, an Iowa Corporation and Schwerman Trucking Company a Wisconsin corporation; and

Subject to a certain Grant of Easement to the Town of Buffalo, Iowa, dated December 1, 1972 and filed for record in the Office of the Recorder of Scott County, Iowa, as Document Number 1100-73 on January 24, 1973 and a certain Lease Agreement between the Town of Buffalo, Iowa, as lessor, and Marietta Facilities, Inc., a Delaware Corporation as lessee dated December 1, 1972 and recorded in the Office of the Recorder of Scott County, Iowa, as Document No. 1101-73 on January 24, 1973 and a certain Indenture of Trust dated December 1, 1972 between the Town of Buffalo, Iowa, and Trustee which Indenture of Trust is dated December 1, 1972 and is recorded in the Office of the Scott County, Iowa Recorder as Document No. 1102-73 on January 24, 1973; and

ALL OF THE FOREGOING PARTICULARLY DESCRIBED PARCELS OF REAL ESTATE ARE CONVEYED SUBJECT TO THE FOLLOWING:

Except that portion deeded to the State of Iowa by Deed dated August 31, 1982 and recorded as Document No. 12944-82 in the office of the Recorder of Scott County, Iowa, and excepting those lands condemned by the United States of America under order dated August 11, 1939 and recorded in the office of the Scott County, Iowa, Recorder at Book 82 Land Deeds, Page 264 and excepting the tract conveyed to the City of Buffalo, Iowa by deed dated July 22, 1960 and recorded in the office of the Scott County, Iowa Recorder as Document No. 7502-81.

# EXCEPTIONS TO ALL OF THE ABOVE PARCELS

51.20 feet; thence South 33 degrees 48 minutes West 455.70 feet; thence South 81 degrees 6 minutes West 419.70 feet; to the Westerly end of said sea-wall; thence South 85 degrees 16.1/2 minutes West 310 feet to the point of beginning; thence South 85 degrees 16.1/2 minutes West 1100 feet to the Easterly bank of a present creek outlet at a point approximately 2930 feet West of and 3000 feet South of the Northeast corner of said section; thence Northerly along said creek outlet bank to the present lowa shore line of said river at elevation of 547 feet above mean sea-level; thence Easterly along said shore line to a point 1860 feet West of and 2550 feet South of the Northeast corner of said section; thence Southerly 330 feet along the West line of the premises owned by Dewey Portland Cement Company to the point of beginning. assessments; general and special, not now due and payable, and a certain boundary adjustment Agreement between Grantor and the State of lows recorder on October 4, 1982 in the office of the Recorder of Scott County, lows as Document No. 12345-82, and TOGETHER NITH any easements appurchant or of record for the benefit of the real estate herein conveyed; and further subject to any rights or claims of the United States of America in and its the subject premises acquired pursuant to a certain order vesting title entered in the United States District Court for the Southern District of Iowa, Davenport Division, dated August 11, 1939 and filed in the office of the Recorder of Scott County, Iowa on August 18, 1939 at Book 82 Land Deeds 264; and

Further subject to the rights of the United States of America, the State of Iowa, the City of Buffalo, Iowa, and the Public in and to that part of the subject premises falling in the bed of the Mississippi River; also rights of property owners in and to the free and unobstructed flow of the waters of said river.

THE GRANTOR HEREIN ALSO CONVEYS TO THE GRANTEE HEREIN THE FOLLOWING ADDITIONAL PARCELS OF REAL ESTAVE SITUATED IN SCOTT COUNTY, IOWA: Parcel No. 8: That part of the Southwest Quarter of the Southeast Quarter of Section 17, Township 77 North, Range 2 East of the 5th P.M., which lies West of the highway running through said quarter section as the same was located and established by Easement dated November 3, 1926 and recorded in Book 77 of Land Deeds at Page 235, records of the office of the Recorder of Scott County, Iowa.

Except that portion thereof included in the tract conveyed by Jacob Fridley and wife to Christ Rautz by Deeds dated June 14, 1862 and November 22, 1864 and recorded in Book 32 of Land Deeds, Page 150 and 159, respectively; and excepting the piece one rod in width conveyed by Jacob Fridley and wife to Conrad Appel by Deed dated March 12, 1872 and recorded in Book 43 of Land Deeds at Page 13, records of the office of the Recorder of Scott County; Iowa;

Also excepting that portion thereof conveyed to Scott County, Iowa by Quit Claim Deed dated April 29, 1964 and recorded in Book 278 of Deeds on Page 571 in the office of the Recorder of Scott County, Iowa.

Parcel No. 91 All of the Southeast Quarter of the Southwest Quarter in Section 17. Township 77 North, Range 2 East of the 5th P.M., excepting 3 acres, more or less, lying and being situated Northeast of the Blue Grass Road, which was conveyed to Stephen A. Collins by deeds recorded in Book 53 of Land Deeds, Page 626, and in Book 66 of Land Deeds, Page 601 in the office of the Recorder of Scott County, Iowa, and also excepting 3 acres, more of less, which was conveyed to Jack 0. Phillips, et al, by deed recorded in Book 87 of Land Deeds, Page 352 in the office of the Recorder of Scott County, Iowa.

Except that portion thereof conveyed to Scott County, Iowa, by Quit Claim Deed dated April 29, 1964 and recorded in Book 278 of Deeds on Page 571 in the office of the Recorderiof Scott County, Iowa, Parcels no. (10 and 11) The Northwest Quarter of the Southwest Quarter of Section 14, township 77 North, Range 2 East of the 5th P.N., Also described as Lot 4

In the partition of the Estate of LeRoy Dodge. Also part of the Southeast Quarter of Section 15. Township 77 North, Range 2 East of the 5th P.N., described as commencing at the Northeast corner of the Southeast Quarter of said Section 15; thence West on the North line of said Southeast Quarter of Section 15, 15 chains; thence South on the East line of Lot 6, 20 chains; thence East on the North line of Lot 1, 15 chains; thence East on the North line of Lot 4, 20 chains; thence North on the West line of Lot 4, 20 chains to the place of beginning, which real estate is also described as Lot 5 in the partition of the Estate of LeRoy Dodge, deceased.

The above described tracts of real estate are particularly described by survey as follows:

Beginning at the Northeast corner of the Southeast 1/4 of Section 15, Township 77 North, Range 2 East of the 5th Principal Meridian said point being also the Northwest corner of the Southwest 1/4 of Section 14, Township and Range aforesaid, thence North 89 degrees 52 minutes 14 seconds East along the North line of the said Southwest 1/4 of Section 14 a distance of 1331.0 feet; thence South 0 degrees 42 minutes 49 east Corner of Lot 44 Devil's Creek Estates Addition: thence North 0 degrees 37 minutes 00 seconds East along the Bast line of said Devil's Creek Estates Addition a distance of 1325.43 feet; thence South 83 degrees 52 minutes 53 seconds East 996.64 feet to the place of beginning. Situated in Buffalo Township, Scott County, Iowa.

ALL OF THE FOREGOING PARTICULARLY DESCRIBED PARCELS OF REAL ESTATE ARE CONVEYED SUBJECT TO THE FOLLOWING:

Subject to existing leases and rights of tenants in possession, easements, restrictions, reservations, or agreements of record, the fights of the public and the State of Iowa in roads and highways through the same, taxes and assessments, general and special, not now due and payable, and TOGETHER WITH any easements appurtenant or of record for the benefit of the real estate herein conveyed.

Martin Marletta Corporation hereby convenants with said grantee, and successors in interest, to Warrant and Defend the said premises against the lawful claims of all persons claiming by, through or under it, except as may be above stated

IN WITNESS WHEREOF said corporation has caused this instrumentito be duly executed this \_\_\_\_\_\_ day of May, 1983.

MARTIN MARIETTA CORPORATION

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State of state of the seal of said corporation; that said instru-ment was signed, and sealed on behalf of said corporation by COUNTY, ment was signed and sealed on behalf of said corporation by authority of its Board of Directors; and that the said  $\frac{P_{\rm b}}{P_{\rm b}} = \frac{A_{\rm b}}{A_{\rm b}} = \frac{A_{\rm b}}{A_{\rm b}}$ as such officers, acknowledged the execution of said instrument to be the voluntary act and deed of said corporation, by it and by them voluntarily executed. Edward S. Rosenthal Notary Public in and for said State EDWARD S. ROSCHTHAL Hotary Public, Bute of New York No. 31-771304 Ocseffed In New York County Completion Expires Namiti 30, 1963



**APPENDIX C** 

Hydrologic Monitoring System Plan



# Revised Hydrologic Monitoring System Plan

Continental Cement CKD Monofill Landfill Buffalo, Iowa IDNR Landfill Permit Number 82-SDP-16-97P

> Prepared for: Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by: Blackstone Environmental 514 17<sup>th</sup> Street, #206 Moline, Illinois 61265



March 29, 2021 (Revised April 19, 2021)

REVISED HYDROLOGIC MONITORING SYSTEM PLAN Continental Cement CKD Monofill Landfill Buffalo, Iowa IDNR Landfill Permit Number 82-SDP-16-97P

Prepared for: Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by:

Lindsay E. James, R.G. Senior Project Manager

**Reviewed by:** 

Krista A. Brodersen Senior Project Manager

Kyle Kukuk, P.E. Senior Project Manager



# TABLE OF CONTENTS

Section				
TABL	E OF	CONTENTS	. ii	
1.0	INTR	ODUCTION	. 1	
1.1	Sit	e Location and Background	1	
1.2	Sit	e Topography	1	
2.0	HYD	ROGEOLOGIC SETTING	. 2	
2.3	SI	TE GEOLOGY	2	
2	.3.1	Cedar Valley Group	2	
2	.3.2	Wapsipinicon Group	2	
2	.3.3	Gower Formation	3	
2	.3.4	Scotch Grove Formation	3	
2.4	GF	ROUNDWATER OCCURRENCE	3	
3.0	GRO	UNDWATER MONITORING SYSTEM	. 3	
3.1	Up	per Groundwater Bearing Zone	4	
3.2	Mie	ddle Groundwater Bearing Zone	4	
3.3	Lo	wer Groundwater Bearing Zone	4	
3.4	Lea	achate Monitoring	4	
3.5	Sit	e Lithology and Groundwater Network	5	
3.6	Gr	oundwater Elevations	5	
3.7	Ge	eochemical Data Evaluation	6	
3.8	Gr	oundwater Monitoring System Observations and Recommendations	6	
4.0	GRO	UNDWATER SAMPLING PROCEDURE	. 6	
4.1	Fie	eld Information Forms	7	
4.2	De	contamination and Equipment Preparation	7	
4.3	Wa	ater Level Measurement	8	
4.4	We	ell Inspection and Maintenance	9	
4.5	Sa	mple Collection Procedures	9	
4	.5.1	Groundwater Samples	9	



Z	1.5.2	.2 Lysimeter Samples	10
4.6	5	Sample Labeling	11
4.7	,	Sample Preservation	11
4.8	}	Chain-of-Custody Forms	11
4.9	)	Monitoring Well Redevelopment	12
5.0	G	ROUNDWATER ANALYSIS PROCEDURES	12
5.1		Sample Frequency	12
5.2	2	Instrument Calibration	13
5.3	5	Field Quality Assurance/Quality Control Samples	13
5.4	Ļ	Laboratory QA/QC Samples	13
5.5	5	Laboratory QA/QC Evaluation	14
5	5.5.	.1 Detection Limits	14
5	5.5.2	.2 Precision and Accuracy	14
5	5.5.3	.3 Representativeness	16
5	5.5.4	.4 Comparability	16
~ ~	C	ROUNDWATER ANALYSIS PROCEDURES	47
6.0	G		17
<b>6.0</b> 6.3		Reporting Requirements	17 17
	5		17
6.3	G	Reporting Requirements	17
6.3 <b>7.0</b>	GI	Reporting Requirements	17 <b>18</b>
6.3 <b>7.0</b> 7.3	GI	Reporting Requirements <b>ROUNDWATER STATISTICAL ANALYSIS PROCEDURES</b> Outlier Determination	17 <b>18</b> 18
6.3 <b>7.0</b> 7.3 7.4	GI	Reporting Requirements <b>ROUNDWATER STATISTICAL ANALYSIS PROCEDURES</b> Outlier Determination Interwell Prediction Limit Analysis	17 <b>18</b> 18 19
6.3 <b>7.0</b> 7.3 7.4 7.5	GI	Reporting Requirements <b>ROUNDWATER STATISTICAL ANALYSIS PROCEDURES</b> Outlier Determination Interwell Prediction Limit Analysis Intrawell Prediction Limit Analysis	17 <b>18</b> 18 19 20
6.3 <b>7.0</b> 7.3 7.4 7.5 7.6	GI	Reporting Requirements <b>ROUNDWATER STATISTICAL ANALYSIS PROCEDURES</b> Outlier Determination Interwell Prediction Limit Analysis Intrawell Prediction Limit Analysis Confidence Interval Analysis	17 <b>18</b> 18 19 20 20
6.3 <b>7.0</b> 7.3 7.4 7.5 7.6 7.7	GI	Reporting Requirements <b>ROUNDWATER STATISTICAL ANALYSIS PROCEDURES</b> Outlier Determination Interwell Prediction Limit Analysis Intrawell Prediction Limit Analysis Confidence Interval Analysis Data Distribution	17 <b>18</b> 18 19 20 20 20
6.3 <b>7.0</b> 7.3 7.4 7.5 7.6 7.7 7.8	GI	Reporting Requirements <b>ROUNDWATER STATISTICAL ANALYSIS PROCEDURES</b> Outlier Determination Interwell Prediction Limit Analysis Intrawell Prediction Limit Analysis Confidence Interval Analysis Data Distribution Treatment of Non-detects	17 <b>18</b> 19 20 20 20 21
6.3 <b>7.0</b> 7.3 7.4 7.5 7.6 7.7 7.8 7.9	<b>G</b> G G G G G	Reporting Requirements <b>FROUNDWATER STATISTICAL ANALYSIS PROCEDURES</b> Outlier Determination Interwell Prediction Limit Analysis Intrawell Prediction Limit Analysis Confidence Interval Analysis Data Distribution Treatment of Non-detects Comparison of Groundwater Contaminant Concentration	17 <b>18</b> 19 20 20 20 21 21
6.3 <b>7.0</b> 7.3 7.4 7.5 7.6 7.7 7.8 7.9 7.1	<b>G</b> G G G G G G G	Reporting Requirements <b>ROUNDWATER STATISTICAL ANALYSIS PROCEDURES</b> Outlier Determination Interwell Prediction Limit Analysis Intrawell Prediction Limit Analysis Confidence Interval Analysis Data Distribution Treatment of Non-detects Comparison of Groundwater Contaminant Concentration Verification Resampling	17 18 19 20 20 20 21 21 21 22
6.3 <b>7.0</b> 7.3 7.4 7.5 7.6 7.7 7.8 7.9 7.1 7.1	<b>G</b> <b>G</b> <b>G</b> <b>G</b> <b>G</b> <b>G</b> <b>G</b> <b>G</b> <b>G</b> <b>G</b>	Reporting Requirements <b>ROUNDWATER STATISTICAL ANALYSIS PROCEDURES</b> Outlier Determination Interwell Prediction Limit Analysis Intrawell Prediction Limit Analysis Confidence Interval Analysis Data Distribution Treatment of Non-detects Comparison of Groundwater Contaminant Concentration Verification Resampling Time Series Graphs	17 18 18 19 20 20 20 21 21 21 22 22



8.0	LIMITATIONS	24
9.0	REFERENCES	24

# TABLES

- 1a Existing Monitoring System Specifications
- 1b Proposed Monitoring System Specifications
- 2 Groundwater Elevation Data
- 3 Sample Collection, Method, Preservation, and Holding Times

#### FIGURES

- 1a Topographic Map
- 1b Site Plan
- 2 Hydrograph
- 3 Potentiometric Surface Map Lower GBZ February 2021
- 4 Potentiometric Surface Map Middle GBZ February 2021
- 5 Potentiometric Surface Map Upper GBZ February 2021
- 6 Potentiometric Surface Map Combined Middle and Lower February 2021
- 7 Cross Section A-A'
- 8 Cross Section B-B'
- 9 Cross Section C-C'
- **10 Cross Section Plan View**
- 11 Groundwater Model Monofill Area
- 12 Potentiometric Surface Map All wells with Sump
- 13 Site Groundwater Surface Model

#### **APPENDICES**

- A. Boring Logs and Well Construction Diagrams
- **B. Example Field Forms**
- C. Example Chain of Custody
- D. HydraSleeve® Field Manual
- E. Time Series Plots



# 1.0 INTRODUCTION

This Revised Hydrologic Monitoring System Plan (HMSP) presents sampling and analysis procedures for the Cement Kiln Dust (CKD) Monofill operated by Continental Cement Company (Continental) and replaces the previous HMSP dated January 30, 2015.

The purpose of this document is to update the HMSP to address comments received in the Iowa Department of Natural Resources (IDNR) letters dated September 9, 2020, December 3, 2020, and January 29, 2021. The HMSP describes the hydrogeologic setting of the facility, the groundwater monitoring network, groundwater bearing zones, background and compliance monitoring parameters and frequencies, sampling procedures, groundwater flow characteristics, and statistical methodology. This document was prepared to meet the requirements of the Continental Cement Davenport Plant Operating CKD Landfill Permit Number 82-SDP-16-97P and the applicable regulatory requirements of Iowa Administrative Code (IAC) Chapter 115.

#### 1.1 Site Location and Background

The Continental CKD Monofill (Site) is located within a portion of Continental's former rock quarry at the Continental facility located in the Southeast Quarter of Section 23, Township 77 North, Range 02 East, in Scott County, Iowa. The Landfill is located approximately 1.3 miles east/northeast of the City of Buffalo in Scott County, Iowa, and approximately 700 feet north of the Mississippi River.

The Site currently operates a monofill under IDNR Permit Number 82-SDP-16-97P. A portion of the monofill has been closed under Permit Number 82-SDP-15-96C. The monofill is used for the disposal of CKD resulting from cement manufacturing processes. A Site Plan showing the approximately 88 acres of the property with existing and closed CKD monofill landfill cells, the existing monitoring well network, and general site details are included as Figures 1a and 1b.

The quarry sump is used to control surface water runoff and to dewater active quarry operation areas. Water is pumped from the quarry sump and discharged to the Mississippi River under a National Pollutant Discharge Elimination System (NPDES) Permit.

# 1.2 Site Topography

The topography in the area of the Monofill consists of hilly terrain sloping generally southward toward the Mississippi River floodplain. As shown on Figure 1a, the base elevation of the quarry near the monofill is approximately 490 feet mean sea level (msl). Surface elevations of the closed and active portions of the monofill range from approximately 590 to 610 feet msl.



# 2.0 HYDROGEOLOGIC SETTING

The area around the Site consists of rolling hills characteristic of the Southern Iowa Drift Plain Physiographic Region and the valley floor of the Mississippi River floodplain. The area is dissected by southerly trending streams that flow into the Mississippi River.

Local stratigraphy consists of basin fill deposits from the Middle to Lower Devonian and Upper Silurian marine sequences. Some regions of Scott county also have Lower Pennsylvania outcrops. Regional dip of the strata is expected to be gently dipping to the southwest/west. Bedrock in the region of the Site consists of units of the Cedar Valley Group, Wapsipinicon Group, Gower Formation, and Scotch Grove Formation (in descending order). These strata are detailed below.

# 2.3 SITE GEOLOGY

# 2.3.1 Cedar Valley Group

At the Site, the Cedar Valley Group consists of the Lithograph City, Coralville, and Little Cedar formations in descending order (Day, 1994). The Lithograph City formation consists of dolomite with some interbedded argillaceous dolomite or shale members, while the Coralville and Little Cedar formations are dominantly fossiliferous limestone. The Cedar Valley Group is up to 500 feet thick (Horick, 1984). However, regionally, the Cedar Valley Group is approximately 80 feet thick (Terracon, 2020). The Cedar Valley Group underlies or is adjacent to CKD fill in the north/northeast portion of the Landfill. Due to quarry activities, the Cedar Valley Group is not present in the west/southwest portion of the Landfill (Terracon, 2020). Boring logs for piezometers set in the Cedar Valley Group indicate dominantly limestone bedrock with some shale bearing zones.

#### 2.3.2 Wapsipinicon Group

The Wapsipinicon Group consists of the Pinicon Ridge and Otis formations. The Pinicon Ridge formation is dominantly fossiliferous limestones and unconformable dolomites lower in the formation with some associated argillaceous members. The Otis formation is dominantly coarsely to finely crystalline limestone (Hickerson and Anderson, 1994). In the vicinity of the quarry, the Otis Member of the Wapsipinicon reportedly forms a local confining bed separating the Devonian and Silurian age limestones (Terracon, 2020). The Wapsipinicon Group is approximately 100 feet thick locally (Terracon, 2020). According to boring logs of piezometers set within the Wapsipinicon Group, dolomitic limestone is the dominant rock present at the Site.



# 2.3.3 Gower Formation

Generally, the Gower Formation consists of non-laminated and stromatolitic laminated dolomite and limestone. The thickness of the formation at the Site is approximately 100 feet (Terracon, 2020)

# 2.3.4 Scotch Grove Formation

The Scotch Grove Formation consists of fossiliferous and less fossiliferous units of dolomite. The thickness of the formation on the site is approximately 120 feet. It was previously reported that the Silurian Groundwater zone is set within the Blanding Formation. However, review of the literature suggests that piezometers within the Silurian Groundwater zone are set within the Gower or Scotch Grove Formations (Hickerson and Anderson, 1994; Horick, 1984).

# 2.4 GROUNDWATER OCCURRENCE

The groundwater at the Site is contained within the regional Silurian-Devonian aquifer. This aquifer is confined by the Lime Creek Formation in the upper Devonian and the Maquoketa Formation in the upper Ordovician. In the east/northeastern portion of Iowa, the Lime Creek Formation has been eroded and the Silurian-Devonian aquifer is unconfined. Due to the Site being located within a river valley, the aquifer is locally expected to be mature with higher secondary porosity from carbonate chemical erosion and generally will have higher well yields and faster recovery. The aquifer is generally expected to drain into the Mississippi river.

#### 3.0 GROUNDWATER MONITORING SYSTEM

The current groundwater monitoring system at the Continental Cement CKD monofill Landfill includes three Groundwater Bearing Zones (GBZs) identified as the Upper GBZ (Cedar Valley), Middle GBZ (Devonian), and Lower GBZ (Silurian). The Upper GBZ is reportedly present in limestone bedrock adjacent to the CKD fill areas but is not found in downgradient portions of the fill area; the Middle GBZ is located in limestone bedrock beneath the monofill area and at least partially contained by the cone of depression associated with the Quarry Sump; and the Lower GBZ is located in Silurian-aged limestone and dolomite bedrock beneath the Middle GBZ. The Otis Formation of the Wapsipinicon Group is also reportedly a local confining unit between the overlying Devonian strata and underlying Silurian strata (Komex International, 1996; Terracon, 2020). Evidence exists in the literature suggesting that the Otis Formation is considered a local confining unit (Horick, 1984, Komex International, 1996).

The current groundwater monitoring system for the Landfill consists of 18 groundwater monitoring wells, nine monitoring points, associated sumps, and a stope well. The groundwater monitoring



network consists of MW-1A, MW-1B, MW-2A, MW-3, MW-3L, MW-4, MW-4L, MW-5, MW-7, MW-11, MW-12, MW-13, MW-14, MW-15, MW-16, MW-16L, MW-18, MW-19, and the Quarry Sump. The monitoring points of the closed CKD monofill consist of MW-9, MW-10, UL-1, LL-1, and the Leachate Sump. The monitoring points of the active CKD monofill consist of UL-2, LL-2, UL-3, and LL-3. The stope well MW-2CR is associated with a stope intercepted from the underground workings of the neighboring Linwood mine. Available boring logs and monitoring well construction diagrams for the monitoring wells are included in Appendix A. Monitoring System specifications are provided in Table 1. Gradient designations presented in Table 1 are based upon potentiometric surface maps prepared from groundwater level measurements collected in February 2021 (Figures 3-6) and are subject to change based on future observations.

Groundwater is monitored by wells in three GBZs on the site: The Upper GBZ, the Middle GBZ, and the Lower GBZ. The wells historically used to monitor these three zones are described below.

# 3.1 Upper Groundwater Bearing Zone

Monitoring wells MW-1B and MW-2A are screened within the Upper GBZ and will be monitored according to the procedures described in the sections below. Monitoring well MW-1B has historically served as an upgradient/background well.

# 3.2 Middle Groundwater Bearing Zone

Monitoring wells MW-1A, MW-3, MW-4, MW-5, MW-11, MW-12, MW-13, MW-14, MW-15, MW-16, MW-18, and the Quarry Sump are screened within the Middle GBZ and will be monitored according to the procedures described in the sections below. Monitoring wells MW-1A, MW-13, and MW-15 have historically served as upgradient/background wells.

# 3.3 Lower Groundwater Bearing Zone

Monitoring wells MW-3L, MW-4L, MW-7, MW-16L, and MW-19 are screened within the Lower GBZ and will be monitored according to the procedures described in the sections below. Monitoring well MW-7 has historically served as an upgradient/background well.

# 3.4 Leachate Monitoring

Monitoring points MW-9, MW-10, LL-1, UL-1, and Leachate Sump are screened within the closed cell and LL-2, LL-3, UL-1, UL-2, and UL-3 are screened within the active monofill. These monitoring points will be gauged monthly and purged if the water column is greater than 1 foot. Purged water will be discharged into the leachate sump. Monitoring points will be sampled



according to the procedures described below. Monitoring points MW-9, MW-10, and UL-1 are historically dry.

# 3.5 Site Lithology and Groundwater Network

# 3.6 Groundwater Elevations

Groundwater elevations are measured monthly to determine groundwater flow direction within the GBZs. Monthly groundwater elevations from January 2020 through February 2021 are presented in Table 2. A hydrograph representing the past 12 months is presented in Figure 2. Groundwater potentiometric maps will be prepared for each month to evaluate the changes in elevations and flow direction throughout the year.

Groundwater flow direction within the Middle GBZ has historically been towards the west, southwest, south, and southeast. In 2010 or early 2011 there was reportedly a change in groundwater flow direction in the Lower GBZ of more towards the east, which appears to be seasonally influenced (Terracon, 2015).

The Lower GBZ contour map produced from February 2021 groundwater level measurements appears to show radial flow, with predominant flow in a southward direction toward the Mississippi River. Review of available information and literature appears to support that the Otis Formation may be acting as a leaky confining unit, allowing communication between what is currently being called the Lower GBZ and the Middle GBZ. Groundwater level data for the Upper, Middle, and Lower GBZs were plotted to produce a hydrograph (Figure 2) of groundwater elevations between January 2020 and February 2021. Although the hydrograph appears to have distinct groups of groundwater elevations within wells, the groupings are not split by formations in which they are screened, but instead are laterally grouped. Furthermore, contouring the Lower GBZ and Middle GBZ as a single zone results in contours that support the Lower and Middle GBZ as being a single Deep Zone (Figures 4-6).

Well data was compiled and put into the RockWare® RockWorks subsurface modeling software to produce graphic representations of the groundwater surface across the Site. Cross sections were produced for the monofill area (Figures 7-10), with well construction and groundwater level information plotted. A groundwater surface model (Figure 11) was also produced for the monofill area using available boring logs. The cross sections and groundwater surface model graphically support the independence of groundwater levels and the formations in which monitoring wells are screened in the monofill area. Groundwater levels were then used for the entire site including the Quarry Sump to produce a groundwater surface model showing the Lower GBZ and Middle GBZ wells as one Deep Zone. Figure 12 and 13 show the plan view of groundwater contours and the groundwater surface model as produced by RockWorks across the Site. A comment letter dated



February 3, 2021 from IDNR regarding the 2020 Annual Water Quality Report suggested that radial flow conditions may be present in the area of MW-4L. Based on this analysis it appears that groundwater flow across the site is radial, however flow is predominantly to the north and west towards the Quarry Sump.

# 3.7 Geochemical Data Evaluation

Time series plots were prepared for available major cations and anions including calcium, chloride, magnesium, potassium, sodium, and sulfate. Time series plots for chloride, potassium, sulfate, and sodium show obvious spatial variation in geochemistry with Lower GBZ well MW-4L plotting with Middle GBZ wells MW-4, MW-11, MW-14, and MW-18 (Appendix E). Furthermore, the remaining Lower GBZ and Middle GBZ wells plot together and show similar geochemistry (i.e. MW-16, MW-3, MW-3L, etc.).

# 3.8 Groundwater Monitoring System Observations and Recommendations

Based on review of groundwater potentiometric surface maps showing the Lower, Middle and Upper GBZ and the geochemical review, it appears that the Middle and Lower GBZ could be combined into one GBZ. Figures 6 through 13 support the comments from IDNR of radial flow existing at the Site. Further, geochemical comparison indicates that wells screened within the Middle and Lower GBZ are geochemically similar.

Although monitoring wells are screened at varying depths and stratigraphic units, it appears as though water levels are consistent and do not exist under confining conditions. In addition to similar groundwater levels, geochemical comparisons indicate that wells screened within the Middle and Lower GBZ are geochemically similar suggesting that they are monitoring the same waters.

Based on an analysis of the available data, Blackstone recommends that the Middle and Lower GBZ be treated as a single monitorable unit. The proposed Monitoring Network including gradient designations is shown on Table 1b.

# 4.0 GROUNDWATER SAMPLING PROCEDURE

The objective of groundwater sampling is to produce reproducible, representative, verifiable, and defensible groundwater chemical data. This section describes the specific tasks involved in sampling the groundwater monitoring system at the Landfill. Samples will be collected from the Landfill groundwater monitoring system by a field sampling technician fully trained in the required sampling procedures and protocols.



#### 4.1 Field Information Forms

To provide documentation of each monitoring event, a detailed sampling record will be maintained. An example field sampling record form is provided in Appendix B. Blackstone will also record sampling information on the IDNR Groundwater Sampling Forms 542-1322 or 542-1324, as required. This form will allow documentation of the following information, at a minimum:

- Identification of the well.
- Date, time, sampler identification.
- Static water level measurement.
- Total depth of each well.
- Well integrity (condition of the well pad, protective casing, well casing, well identification, and locks).
- Numerical field data.
- Date and time of sample collection.
- Field observations (well recharge rates, equipment malfunction, sample odor and characteristics).

#### 4.2 Decontamination and Equipment Preparation

All non-dedicated, sample-contacting equipment will be thoroughly decontaminated prior to use at the Site. Decontamination procedures will consist of the following steps:

- Wash with laboratory grade soap (Alconox).
- Rinse with distilled or deionized water.
- Air dry prior to use.

Wash and rinse fluids will be disposed of in an appropriate area segregated from the well.



Field sampling technicians who contact sampling equipment subsequent to decontamination will wear nitrile (or equivalent) gloves. Gloves will be replaced between each well or immediately if they become contaminated or torn. Measures will be taken to prevent surface soils from contacting sampling equipment.

# 4.3 Water Level Measurement

Static water level elevations provide information on the groundwater gradients, which in turn are used to predict the groundwater flow directions and velocities. Static groundwater levels will be measured prior to sampling activities each time the groundwater is sampled using a portable water level indicator with measurement accuracy of 0.01 foot. Groundwater elevations in wells which monitor the same solid waste disposal area shall be measured within a period of time short enough to avoid temporal variations in groundwater flow that could preclude accurate determination of groundwater flow direction. Water levels will be measured from least to most contaminated in order to limit potential cross-contamination. The following procedure will be used when measuring static water level elevations:

- Decontaminate the cable and probe of the water level indicator in accordance with the procedures specified in Section 4.2.
- Establish the measurement reference point (MRP), which is the top of the inner PVC casing.
- Lower the decontaminated probe into the well to the water surface until the meter gives an audible sound upon contact.
- Record the distance from the MRP to the water surface to the nearest 0.01 foot, and the date on the well sampling record.
- Decontaminate the probe and cable, as previously described, prior to measuring the next well.

Water levels will be compared with historic water levels whenever possible. If a significant difference in water levels from the previous sampling event is noted, the water level will be remeasured. If the remeasurement gives the same result, the inconsistency will be noted on the field form.

The water level measurements will be reported to the IDNR once a year in the Annual Water Quality Report (AWQR). Water level measurements will be provided on IDNR forms 542-1322 for the monitoring wells and IDNR form 542-1324 for the Quarry and Leachate Sumps.



#### 4.4 Well Inspection and Maintenance

Prior to performing sampling activities, each monitoring well will be inspected to assess its integrity. The condition of each well will be evaluated for physical damage that may have been caused by operation of Site equipment or vehicle traffic. The security of each well will also be assessed in order to determine the potential for outside contamination being introduced to the well. Maintenance and security requirements will be detailed on the field sampling forms.

#### 4.5 Sample Collection Procedures

The following sections describe sample collection procedures for groundwater and lysimeter samples. It should be noted that the mine stope, leachate, and sump samples will be collected as grab (no-purge) samples.

#### 4.5.1 Groundwater Samples

Groundwater samples will be collected using HydraSleeve® groundwater samplers. The HydraSleeve® samplers collect a whole water sample from within the well screen, without mixing fluid from other intervals and without purging. Groundwater samples will be collected with a disposable polyethylene bailer or pump if insufficient water is not present to deploy or other issue arises where a HydraSleeve® cannot be used. Care will be taken to avoid placing clean sampling equipment on the ground or a contaminated surface. Wells will be sampled from least to most impacted to reduce the potential for cross-contamination. Nitrile gloves will be worn during all sampling procedures. Sample bottles will be filled in the order of the volatilization sensitivity of the parameters as follows:

- 1. Metals
- 2. Major Cations and Anions
- 3. Sulfate and Chloride
- 4. Nitrate and Ammonia

A new sampler will be deployed in each well during the previous monitoring event. The sampler will be deployed in each well until it is approximately centered within the screened interval of the monitoring well. The sampler will be left in place, allowing time for the well to equilibrate prior to collection of the groundwater sample. The samplers will be retrieved from each well during the next regularly scheduled sampling event and new samplers will be deployed. The HydraSleeve®



Field Manual is included in Appendix D. The manual provides specific procedures for assembly, deployment, and sample collection.

The groundwater samples will be collected by extracting the HydraSleeve® from the wells. The HydraSleeve® is equipped with a one-way reed valve that is opened by the force of pulling the sampler upwards. The sampler will fill during the first 24- to 48-inches of upward pull and once the sampler is full, the reed valve closes, preventing mixing of non-representative fluid during sample recovery.

The sampler will be punctured with a disposable plastic tube and the appropriate laboratory supplied sample containers will be filled. Sample volume will be retained for field measurements of pH, specific conductivity, temperature, and turbidity. Field measurements will be collected using a calibrated multi-parameter probe. Per 567 IAC, specific conductance and pH analyses will be conducted in the field for all groundwater and leachate samples. The samples will be labeled and collected in appropriate containers with the appropriate sample preservative as described in subsequent sections.

# 4.5.2 Lysimeter Samples

Samples will be collected from the lysimeters using a disposable polyethylene bailer or pump. Care will be taken to avoid placing clean sampling equipment on the ground or a contaminated surface. Nitrile gloves will be worn during all sampling procedures. Sample bottles will be filled in the order of the volatilization sensitivity of the parameters as follows:

- 1. Metals
- 2. Major Cations and Anions
- 3. Sulfate and Chloride
- 4. Nitrate and Ammonia

In accordance with Permit Special Provision #4b, the lysimeters will not be purged prior to sampling because it appears that the lysimeters may be located above the water table and collecting leachate that has percolated through the liner. Because of the slow percolation rates through the liner, purging of these points may result in a dry point that will not recharge in a timely manner. Additionally, successful purging of the lysimeter to remove stagnant, unrepresentative water would require purging of all water from the lysimeter (retained within the lysimeter basin and the well casing). Hydrasleeve or other no-purge sampling devices are not recommended for



the lysimeters as they may not yield representative samples due to the lysimeter construction (i.e. with horizontal screens).

Sample volume will be retained for field measurements of pH, specific conductivity, temperature, and turbidity. Field measurements will be collected using a calibrated multi-parameter probe. Per 567 IAC, specific conductance and pH analyses will be conducted in the field for all lysimeter samples. The samples will be labeled and collected in appropriate containers with the appropriate sample preservative as described in subsequent sections.

# 4.6 Sample Labeling

A completed sample label will be affixed to each sample bottle indicating the sample number, date and time of collection, sampler's initials, and selected parameters.

# 4.7 Sample Preservation

Sample containers will be supplied by the laboratory for each sampling event. Each sample provided by the laboratory will be pre-preserved with the appropriate amount of preservative for the particular analysis. Alternatively, the laboratory may ship pre-measured amounts of preservative for addition to the sample in the field. Bottles will not be overfilled as this may cause loss of some of the sample preservative. Immediately after collection and labeling, the samples will be placed in a sample cooler with ice. Exposure of the samples to direct sunlight will be minimized as it can alter sample quality. The samples will then be transported to the laboratory in the sample cooler via overnight service. A sample temperature will be recorded when the sample container arrives at the laboratory to assure that the appropriate sample temperature was maintained during shipment. A summary of the appropriate sample preservation and holding times for each analytical method is shown on Table 3.

# 4.8 Chain-of-Custody Forms

Chain-of-custody procedures will allow for the possession and handling of samples to be tracked from the time of collection through laboratory analysis. A chain-of-custody form (COC) for each sample will be completed immediately following sample collection. The COC will be placed in the shipping container and accompany the samples from the time of collection through transportation to the laboratory. A copy of the COC will be maintained by the sampling personnel. An example of the COC is shown in Appendix C.



#### 4.9 Monitoring Well Redevelopment

Redevelopment of monitoring wells should occur when more than 25 percent of the screen length is occluded. If the screen is found to be 25 percent or more occluded, the following procedure will be used to remove fine-grained material from the well and filter pack near the screen:

- Decontaminate all down-hole equipment prior to beginning redevelopment.
- Obtain an initial water level measurement.
- Collect an initial sample of water and measure for field parameters including pH, specific conductivity, and temperature. Note the color, odor, and turbidity of the sample.
- If using a bailer to redevelop the well, lower the bailer to the bottom of the well and return it to the top in a manner to cause gentle surging in and out of the well. The bailer should be brought to the surface and the water and sediment emptied. Repeat this process until a minimum of five well volumes have been removed, field parameters have stabilized, and the well screen is cleared of sediment.
- If pumping and surging to redevelop the well, surging will be accomplished by lowering the pump into the saturated interval and repeatedly raising and lowering the pump. Following surging, the well should be pumped until at least five well volumes have been removed, field parameters have stabilized, and/or the well screen is cleared of sediment.
- If the monitoring well purges dry during redevelopment, water should be allowed to recover within a reasonable amount of time (i.e. within 8-hours). Following recovery, the development procedures should be repeated until five well volumes have been removed, field parameters have stabilized, and the well screen is cleared of sediment.

#### 5.0 GROUNDWATER ANALYSIS PROCEDURES

This section provides procedures for analysis of groundwater samples collected from the monitoring system at the Site. Analytical methodologies, as well as field and laboratory Quality Assurance/Quality Control (QA/QC) procedures are discussed in this section.

#### 5.1 Sample Frequency

Semi-annual groundwater sampling will be conducted during the months of March and September of each calendar year. Sampling events must be six months apart. New wells will be sampled quarterly until a minimum of eight quarters of valid data are collected.



# 5.2 Instrument Calibration

Equipment and instruments used in the field will be calibrated using calibration standards and method-specified calibration criteria according to manufacturer's specifications. Standards will be purchased as certified primary solutions from reputable, commercial lab suppliers. The results of field instrument calibration will be documented in the AWQR.

#### 5.3 Field Quality Assurance/Quality Control Samples

Field QA/QC samples collected during each regular sampling event at the Site will include:

• Duplicate Sample – A duplicate sample will be collected from one monitoring well during each sampling event. The sample will be collected by alternating filling a duplicate sample bottle and a regular sample bottle during sampling. The duplicate sample will be labeled as "Duplicate" on the Chain-of-Custody prior to sending to the laboratory for analysis.

#### 5.4 Laboratory QA/QC Samples

A record of the laboratory sample receipt, storage, and analysis procedures will be kept for each sample received. The analytical laboratory will prepare blanks and spikes to assure analysis quality in accordance with the laboratory's QA/QC Control Plan.

Method blanks are blank solutions which are treated as a sample for the analyte being measured, including all preparation procedures and are analyzed in the same manner as the environmental samples in order to assess analytical accuracy and the potential for sample contamination. These blanks are used to ensure that the solvents or chemicals used in sample treatment are not systematically biasing environmental sample results.

Matrix spikes are samples in which known concentrations of analytes expected to be in the sample are added. The percent recovery of any spiked analyte is taken as a measure of the bias of the analytical method caused by the sample matrix. Surrogate spikes are samples in which known concentrations of analytes not expected to be in the sample are added.

Any internal control problem associated with the submitted sample/analyte will be identified on the data qualifier report included with the analytical report.



# 5.5 Laboratory QA/QC Evaluation

The following sections describe the procedures that will be performed to evaluate the acceptability of the data received from the laboratory.

# 5.5.1 Detection Limits

In order to meet the sampling objectives, analytical detection limits must be low enough to support a conclusion that contaminants are not present at concentrations above levels that define a specified risk to human health or the environment.

The analytical laboratory uses the procedures described in 40 Code of Federal Regulations (CFR) 136 to determine method detection limits (MDLs). Method specific upper and lower precision and accuracy limits are developed each year from historical matrix spike and matrix spike duplicate data. The laboratory performing the analysis will be requested to maintain established Practical Quantitation Limits (PQLs) with +/- 25% of their medial value.

The reporting limits will be equal to, or lower than, the Iowa Statewide Standards (SWS) for the Protected Groundwater Sources. Should the analytical laboratory not be able to meet specified reporting limits for certain parameters (i.e. lithium), results may be quantified (j-flagged).

#### 5.5.2 Precision and Accuracy

Precision and accuracy measure the reproducibility of analytical results and the bias of a measurement method, respectively. Quality control limits for analytical precision and accuracy parameters are typically established by the laboratory in accordance with the specific analytical methods.

#### 5.5.2.1 Precision

Precision of the analytical results can be measured by comparing the analytical results of primary samples with those of duplicate samples. The variation in the results is a measure of precision. It can be evaluated in both field and laboratory duplicate samples.

Variation attributable to analysis is detected by observing the discrepancies between the laboratory matrix spike (MS) primary and matrix spike duplicate (MSD) samples and laboratory control sample (LCS) and laboratory control sample duplicate (LCSD), if provided. Precision between primary and duplicate samples can be determined by the relative percent difference (RPD) as indicated in the following equation:



# RPD = (PSR - DSR)/(PSR + DSR)/2 \* 100

Where:

RPD = relative percent difference between the primary sample value and the duplicate sample value PSR = primary sample results (detected concentration) DSR = duplicate sample results

Precision goals for laboratory analyses are method-specific, but typically less than 20 percent if not otherwise specified. Precision for field duplicates should be less than 50 percent.

# 5.5.2.2 Accuracy

The average laboratory spike recovery results are examined to assess the accuracy of the analytical results. Spikes may include reagent spikes (LCS), surrogate spikes, and matrix spikes. A reagent spike is a synthetic matrix (usually organic free water or sodium sulfate) to which a known concentration of all or some of the method analytes is added. A surrogate spike involves adding compounds that are chemically similar, but not identical to, the compounds in the sample being analyzed. The surrogate is added to all samples, including the original sample matrix, and to blanks and reagent spikes. For a matrix spike, known amounts of standard compounds identical to the compounds present in the sample of interest are added to an aliquot of the sample matrix.

Spike recovery is determined by submitting the spiked synthetic matrix or sample aliquot for the same laboratory analysis as the original sample. Spike recovery is calculated using the following equation:

Percent Recovery = (SSR - SR)/SA \* 100

Where:

SSR = spike sample results SR = unspiked sample results SA = spike concentration added to sample

The reagent spike is used to verify the method performance for each sample set. Acceptable accuracy ranges are identified by the laboratory in accordance with the analytical methods.



The surrogate spikes are typically added to all samples (except for those to be analyzed by gross non-chromatographic analytical methods). Surrogate results from blanks and reagent spikes are plotted by the laboratory to evaluate trends and variability with respect to corrective action.

Surrogate spike results for environmental samples are reviewed qualitatively in relationship to acceptance limits and results for blanks and reagent spikes to evaluate matrix effects and gross sample-processing errors.

The laboratory matrix spike is used to verify method performance by recovery of analytes in a particular matrix. Recovery reflects the bias from both the environmental sample matrix and normal method performance (as opposed to the reagent spike, which reflects the method performance only). Comparison with the reagent spike accuracy is used to assess whether the analytical process is in control (e.g., whether the matrix is biasing analyte recovery).

# 5.5.3 Representativeness

Representativeness expresses the degree to which sample data accurately and precisely represent site conditions. The determination of the representativeness of the data is performed by:

- Comparing analytical results of field duplicates to determine the spread in the analytical results.
- Examining the results of quality control blanks for evidence of contamination.

These involve qualitative reviews. Quality control blanks include trip blanks and laboratory method blanks. The quality control blanks are used to quantitatively qualify data.

# 5.5.4 Comparability

Comparability is the confidence with which one set of analytical data may be compared with another. Comparability is maintained by being aware of previous sampling and analysis at the Site and through the use of standard operating procedures and analytical methods and detection limits. To facilitate comparability of databases, data will be generated using widely accepted sampling standard operating procedures and analytical methods and will be reported in units consistent with those used by other agencies and organizations reporting analytical data.



# 6.0 GROUNDWATER ANALYSIS PROCEDURES

Monitoring will be conducted in accordance with the approved facility permits on a semi-annual basis during the months of March and September of each calendar year.

Background samples will be collected quarterly for a minimum of two years following installation of new wells. The purpose of background sampling is to establish a range of ambient concentrations of the groundwater system being monitored. Ideally, the background data set should contain enough data points to perform the selected statistical method and incorporate seasonality and/or temporal variability.

Samples will be collected for laboratory analysis at each of the specified monitoring points. The semi-annual and background monitoring parameter list includes the following parameters:

- Indicator parameters bicarbonate alkalinity, carbonate alkalinity, bromate, calcium, chloride, fluoride, nitrate, nitrite, phosphorus, total dissolved solids, and sulfate.
- Total metals aluminum, antimony, arsenic, barium, beryllium, boron, cadmium, chromium, cobalt, copper, lead, lithium, magnesium, manganese, molybdenum, nickel, potassium, selenium, silver, sodium, thallium, vanadium, and zinc.

The sample methods for the parameters are included in Table 3.

#### 6.3 Reporting Requirements

A comprehensive Annual Water Quality Report will be submitted in November of each year. The report will contain the field data, analytical data, and results of the statistical analysis. A copy of this report will be maintained on-site. This report will identify statistically significant increases (SSIs) or statistically significant decreases for parameters. The report will include the following information:

- Sampling purpose detection or assessment monitoring
- Copies of field notes, datasheets, and chain-of-custody documentation
- Significant deviations from the HSMP
- A discussion of the rate and direction of groundwater flow including piezometric surface maps and water level measurements
- Summary of laboratory analytical results
- Data validation
- A copy of the laboratory analytical results



- Summary of statistical results, statistical output, and identification of any statistically significant increases over background values
- Certification by an engineer registered in the State of Iowa

If an SSI of any monitored constituent is identified from the analytical results, confirmation resampling for those constituents will be conducted during the next scheduled semi-annual monitoring event unless otherwise directed by the IDNR.

# 7.0 GROUNDWATER STATISTICAL ANALYSIS PROCEDURES

This section outlines the statistical methodologies that may be used to evaluate whether a facility has negatively impacted groundwater quality. Statistical evaluation is employed to estimate typical behavior of groundwater data and manage uncertainty due to random/natural fluctuations in groundwater data. Despite sample fluctuations due to random variation, statistical analysis helps to determine if compliance concentrations are significantly higher, on average, than background groundwater concentrations and assists in separating natural fluctuations from increasing or decreasing patterns.

It is anticipated that the statistical approach for this facility will be multi-faceted and may use interand intrawell prediction limits for inorganic parameter compliance testing. Confidence intervals may also be constructed for select well-constituent pairs. Distributional analyses including outlier testing and time series plots will also be prepared for all wells to identify any apparent trends or excursions from normal ranges. Due to the complexities of this facility, specific statistical methods for the facility will be discussed and agreed upon by Continental and IDNR.

Statistical analysis will be completed using the Sanitas<sup>™</sup> statistical software, or equivalent. No statistical evaluations will be performed for non-detect results or those detected below the PQL. The historical database for statistical analysis will be updated following each monitoring event. The statistical background dataset will be updated in accordance with United States Environmental Protection Agency (USEPA) Unified Guidance.

# 7.3 Outlier Determination

Data will be examined for outliers, anomalies, and trends that might indicate a release. Outliers and anomalies are values that can occur due to sampling, laboratory, transcription errors, or other unknown factors. Significant trends can indicate a source of systematic error, or an actual contamination occurrence, and must be evaluated. The inclusion of outlying or anomalous values in the historical dataset used for statistical analysis could cause misinterpretation of the data and



results in an artificial increase in statistical limits. An artificial increase in statistical limits could increase the false negative rate (i.e. decrease the statistical sensitivity).

Statistical outliers will be determined using either Dixon's or Rosner's test, depending on the number of background observations.

If either Dixon's or Rosner's test identifies an observation as a statistical outlier, the measurement will not be treated as such until a specific reason for the abnormal value can be determined. Valid reasons might include contaminated sampling equipment, laboratory contamination of the sample, errors in transcription of the data values, etc. Based on this review, one of several actions may be taken:

- If an error in transcription, dilution, analytical procedure, etc. can be identified and the correct value recovered, the observation will be replaced by its corrected value and further statistical analysis done with the corrected value.
- If it can be shown that the observation is an error, but the correct value cannot be determined, the observation will be removed from the data set and further statistical analysis performed on the reduced data set. The removal of the observation and the reason for its removal will be documented in the report.
- If no error in the value can be documented, it will be assumed that the observation is a true but extreme value. In this case, it will not be altered or removed.

# 7.4 Interwell Prediction Limit Analysis

The interwell prediction limit analysis compares data collected from compliance (downgradient) monitoring wells with data collected from background (upgradient) monitoring wells. Data is used to calculate the interwell prediction limit and is used to determine if a single data point is statistically representative of a group of data points. If a data point exceeds the calculated interwell prediction limit, a statistically significant increase is noted.

Interwell prediction limit analysis will be prepared for monitoring wells screened within the individual GBZs. Pooled data from upgradient monitoring wells will be designated as background and downgradient wells will be designated as compliance wells.

Data distribution will be calculated using the Shapiro-Wilk test for normality. The Ladder of Powers will be applied for transformed data. If the data is determined to have normal or transformed normal distribution, a parametric prediction limit will be calculated. If the data is determined to have a non-normal distribution, a non-parametric prediction limit will be constructed.



Non-parametric prediction limits will be constructed for data sets containing 51-90% non-detect results. Interwell prediction limit analysis will be performed for the inorganic parameters detected in groundwater samples. Non-detect parameters will not be included in the interwell prediction limit analysis.

# 7.5 Intrawell Prediction Limit Analysis

Intrawell prediction limits compare concentrations of a constituent to historical concentrations (i.e. background) of that constituent within the same monitoring well. Significant upward changes in the concentration over time results in a statistical result above the prediction limit. As will be performed for the interwell prediction limits, data distribution will be calculated using the Shapiro-Wilk test for normality. The Ladder of Powers will be applied for transformed data. If the data is determined to have normal or transformed normal distribution, a parametric prediction limit will be calculated. If the data are determined to have a non-normal distribution, a non-parametric prediction limit will be constructed. Non-parametric prediction limits will be constructed for data sets containing 51-90% non-detect results.

Non-detect parameters will not be included in the intrawell prediction limit analysis.

# 7.6 Confidence Interval Analysis

Confidence intervals are constructed from sample data and are designed to contain the mean concentration of an analyte with a designated level of confidence. A minimum of four sample values are required for the construction of parametric confidence intervals and seven values are required for non-parametric confidence intervals. Because data can show either apparent or statistically significant trends, the number of constituents analyzed will be limited to the most recent eight sampling events.

For those well-constituent pairs screened that exceed the prediction limit and are confirmed SSIs, further evaluation using confidence intervals will be performed. Groundwater Protection Standards (GWPS) for parameters requiring confidence interval analysis will be proposed to IDNR for approval prior to use.

# 7.7 Data Distribution

Most statistical tests assume that the data comes from a normal distribution. The USEPA guidance recommends the Shapiro-Wilks Test to calculate normality of the data. Alternative procedures for evaluating groundwater contaminant distribution are available for use when data do not follow a normal distribution; these are termed "nonparametric" methods. Where normal



methods use the mean and standard deviation of the data for analysis, nonparametric methods deal with other descriptors of the data for analysis (e.g., minimum, maximum, median, etc.).

The Shapiro-Wilks Test will be used to calculate normality of the data. Based on the results of this test, the type of prediction interval will be calculated. Prediction limits based on a normal distribution will be calculated for parameters that are normally distributed; and "non-parametric" or distribution-free prediction limits will be calculated for parameters that are not normally distributed. For samples that show evidence of non-normality, a normalizing transformation using the Ladder of Powers will be explored. These transformations not only include the natural logarithm, but also other mathematical transformations such as the square root, the cube root, the square, etc. If none of these transformations creates an adequately normalized data set, a non-parametric limit will be calculated.

# 7.8 Treatment of Non-detects

The amount of data below the detection limits plays an important role in selecting the appropriate method. As a general guideline, if 50 percent or fewer of the values were "not detected," they will be replaced with the method detection limit divided by two. If more than 50 percent of the values are reported as not detected, a nonparametric method of analysis will be used.

If more than 90 percent of the background data are less than the MDL, a Poisson distribution-based prediction interval will be computed. The Poisson distribution is a probability distribution modeled for rare events. The Poisson probability of a detection observation is rare unless there is an impact. The sum of the Poisson counts across background samples is computed by adding the number of parts per billion (ppb) across all observations for the well. Prior to any calculation, non-detects are set to one-half the PQL and all trace values are evaluated as an average of the PQL. To test the upper prediction limit, the Poisson count of the sum of the next k observations from the well is compared to the 99 percent upper Poisson prediction limit. If this sum exceeds the prediction limit, there is significant evidence of an impact.

#### 7.9 Comparison of Groundwater Contaminant Concentration

Because the distribution of the data varies by constituent, both parametric and nonparametric forms of the Prediction Interval Method will be used for the statistical analysis. Prediction intervals are constructed to contain the next sample values from a population or distribution with a specified probability. An SSI is identified when the most recent reported sample value for a monitoring well is greater than its respective Upper Prediction Limit (UPL), calculated from historical data. Potential contamination is suggested, if one or more SSIs occur in monitoring wells identified as downgradient. When the historical data is not normally distributed and cannot be normalized



through transformation, the nonparametric UPL will be determined by the maximum historical value.

All SSIs will be reviewed for potentially anomalous data including analytical errors, transcription mistakes, laboratory variation in the PQL or MDL, etc. Outlier tests and time-series graphs will also be reviewed to identify potentially anomalous data.

# 7.10 Verification Resampling

Verification resampling is an approach used to help balance the false positive and false negative rates in groundwater monitoring. If the initial groundwater observation is below the Upper Prediction Limit, no verification resampling is necessary.

In the event of an initial exceedance above the UPL, verification resampling will be conducted, and the statistical exceedance will be verified (i.e. an SSI) if the resampled value also exceeds the UPL. The data used to verify the initial exceedance will be collected at the next scheduled semi-annual monitoring event.

# 7.11 Time Series Graphs

Time series plots depict concentration versus time of sample collection and are useful for identifying a variety of temporal patterns including trends over time, sampling events that may signal a contaminant release, measurement outliers resulting in anomalous 'spikes' due to field handling or analytical errors, and cyclical/seasonal fluctuations in the data. Time series graphs for parameters with observed SSIs will be prepared and reviewed for potentially anomalous data points and constituents which exhibit trends.

Time series graphs to illustrate trends for the inorganic parameters in all wells, presented by GBZ, will also be prepared, and reviewed for potentially anomalous data points and constituents which exhibit trends.

# 7.12 Trend Analysis

In addition to reviewing the time series graphs, the Mann-Kendall upward trend test and the Sen's test will be performed. These tests are non-parametric tests used for the detection of trend in a time series. These tests are widely used in environmental science because there are no distributional assumptions and missing data (i.e., non-detects) and irregularly spaced measurement periods are permitted.



The Mann-Kendall test can be performed at varied confidence intervals; however, a confidence interval of 95 percent will be selected. If an upward trend is identified from the results of the Mann-Kendall test, the Sen's test will be run since it is appropriate for a high percentage of non-detects and is not significantly affected by outliers.

The time series plots will be reviewed, along with the results of the trend analyses, and identified data trends will be evaluated.

# 7.13 Background

The most important quality of background data is that it reflects the historical conditions unaffected by the activities it is designed to be compared against. All detection monitoring tests involve comparison of compliance point data against background. If natural groundwater conditions have changed over time, background measurements from many years ago may not reflect current uncontaminated conditions. Similarly, recent background data obtained using improved analytical or field methods may not be comparable to older data and might have to be discarded in favor of more recent measurements in order to construct an appropriate comparison.

Per the USEPA Unified Guidance, a minimum of eight independent background observations will be collected from the monitoring wells before running statistical tests. Although this is still a small sample size by statistical standards, it will allow for minimally acceptable estimates of variability and evaluation of trend and goodness-of-fit.

Due to the need for sufficiently large sample sizes and the complex behavior of groundwater, background will be periodically reviewed and updated per the USEPA Unified Guidance. Because the Landfill will be conducting semi-annual groundwater sampling, and at least four to eight new measurements should be collected to enable such a test, background will be updated every two years. Outlier tests and Wilcoxon rank-sum comparisons will be conducted at each compliance well between existing intrawell background and the potential set of newer background. If a non-significant result is obtained, the newer compliance data will be added to the existing intrawell background sample. However, if a significant result occurs, the compliance measurements will be reviewed to determine whether a gradual trend or other change has occurred.

# 7.14 Review of Existing Background

It is understood that potential issues may exist with the current background dataset due to historically used sampling procedures and/or the inclusion of trending data and outliers. A background database was provided to Blackstone that included data collected from March 2018 through September 2020 (six total datapoints). Blackstone will evaluate the existing database for



outliers, data trends, and consistency once additional datapoints have been collected for comparison. The results of this analysis will be submitted under separate cover.

#### 8.0 LIMITATIONS

This report was prepared in accordance with that level of skill and care ordinarily exercised by other members of Blackstone's profession practicing in the same locality and under similar conditions when the services were provided. No warranties, express or implied, are intended or made.

#### 9.0 REFERENCES

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- 2. Day, J., Late Middle and Early Upper Devonian Brachiopod Fauns of Southeastern Iowa and Northwestern Illinois, Illinois State University, 1994.
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- 4. Terracon Consultants, Inc., 2020 Annual Water Quality Report, Continental Cement Company Cement Kiln Dust Monofill, Buffalo, Iowa, December 21, 2020.
- 5. Hickerson W., Anderson R., Paleozoic Stratigraphy of the Quad-Cities Region East-Central Iowa, Northwestern Illinois, Geological Society of Iowa, April 24, 1994.
- 6. Komex International LTD., Hydrogeological Workplan, Cement Kiln Dust Management Area, LaFarge Davenport Plant, Alberta, Canada, July 2, 1996.

TABLES

**CONTINENTAL CEMENT COMPANY** 

# Table 1a BLACKSTONE ENVIRONMENTAL ENVIRONMENTAL Existing Monitoring Well and Piezometer Network Network

Continental Cement Landfill Permit Number 82-SDP-16-97P

Well ID	Location (Easting / Northing)	TOC Elevation	Total Depth	Approximate Groundwater Elevation	Screen Length (ft)	Gradient
		Upper GBZ	Z Monitori	ng Wells		
1B	2408909 / 546267.4	617.759	574.51	594.44	20	Upgradient
2A	2409895 / 545676.1	589.596	524.98	560.98	20	Downgradient
		Middle GB2	Z Monitori	ing Wells		
1A	2408901 / 546267.5	617.272	474.43	482.73	20	Sidegradient
3	2410005 / 545114	569.372	468.07	501.57	20	Upgradient
4	2408798 / 545106.5	490.901	456.38	484.19	NA	Downgradient
5	2408744 / 545496.4	490.488	463.20	486.37	10	Sidegradient
11	2409216 / 544852	533.597	423.25	472.73	20	Downgradient
12	2408546 / 545902.2	526.758	448.86	474.79	20	Downgradient
13	2409208 / 544442.7	564.989	465.26	505.99	40	Upgradient
14	2408613 / 544786.9	488.497	456.39	473.98	20	Downgradient
15	2407821 / 543883.2	565.03	429.68	497.64	20	Upgradient
16	2408010 / 545084.8	483.558	417.30	471.64	20	Downgradient
18	2408823 / 545092.4	490.733	423.35	481.88	20	Downgradient
		Silurian GB	Z Monitor	ing Wells		
3L	2410007 / 545144.4	570.355	417.69	474.18	10	Upgradient
4L	2408806 / 545112.6	490.527	429.23	481.71	10	Downgradient
7	2409278 / 547324.6	598.23	412.83	469.56	13.5	Downgradient
16L	2408015 / 545093.8	483.22	367.39	471.07	20	Downgradient
19	2409193 / 546682.8	615.295	399.55	470.06	20	Downgradient
		Stope N	<i>Monitoring</i>	ı Well		
2CR	2409765 / 545875.7	592.563	486.12			
		Sump M	lonitoring	Wells		
Leachate- Sump	2408957 / 545743.8	536.522				
Quarry- Sump	2407834 / 544450.5	485.636	443.42	449.74		
		Leachate	Monitorin	g Points		
MW-9	2409452 / 545411.2	596.29	498.49	Dry		
MW-10	2409664 / 545430.8	594.155	495.79	495.79		
UL-1	2409014 / 545798.2	553.785	544.38	Dry		
LL-1	2409020 / 545789.2	553.39	528.79	532.49		
UL-2	2408874 / 545928	542.305	535.15	537.44		
LL-2	2408869 / 545936	540.732	529.83	530.60		
UL-3	2408805 / 546029.2	543.105	535.69	536.69		
LL-3	2408810 / 546021.1	541.198	530.47	Dry		

All TD and groundwater elevation are based off the most recent Jan, 2021 field activites or as-builts

# Table 1bBLACKSTONE<br/>ENVIRONMENTALProposed Monitoring Well and Piezometer Network

Continental Cement Landfill Permit Number 82-SDP-16-97P

	Location			Approximate	Screen	
Well ID	(Easting / Northing)	TOC Elevation	Total Depth	Groundwater Elevation	Length (ft)	Gradient
		Shallow GB	SZ Monitor	ring Wells		
1B	2408909 / 546267.4	617.759	43.249	594.44	20	Upgradient
2A	2409895 / 545676.1	589.596	64.616	560.98	20	Downgradient
		Deep GBZ	. Monitorir	ng Wells		
1A	2408901 / 546267.5	617.272	142.842	482.73	20	Downgradient
3	2410005 / 545114	569.372	101.302	501.57	20	Sidegradient
4	2408798 / 545106.5	490.901	34.521	484.19	NA	Downgradient
5	2408744 / 545496.4	490.488	27.29	486.37	10	Downgradient
11	2409216 / 544852	533.597	110.347	472.73	20	Downgradient
12	2408546 / 545902.2	526.758	77.898	474.79	20	Downgradient
13	2409208 / 544442.7	564.989	99.729	505.99	40	Upgradient
14	2408613 / 544786.9	488.497	32.107	473.98	20	Downgradient
15	2407821 / 543883.2	565.03	135.35	497.64	20	Upgradient
16	2408010 / 545084.8	483.558	66.26	471.64	20	Downgradient
18	2408823 / 545092.4	490.733	67.383	481.88	20	Downgradient
3L	2410007 / 545144.4	570.355	152.67	474.18	10	Sidegradient
4L	2408806 / 545112.6	490.527	61.297	481.71	10	Downgradient
7	2409278 / 547324.6	598.23	185.4	469.56	13.5	Upgradient
16L	2408015 / 545093.8	483.22	115.83	471.07	20	Downgradient
19	2409193 / 546682.8	615.295	215.745	470.06	20	Downgradient
		Stope I	Monitoring	Well		
2CR	2409765 / 545875.7	592.563	486.12			
		Sump M	lonitoring	Wells		
Leachate- Sump	2408957 / 545743.8	536.522				
Quarry- Sump	2407834 / 544450.5	485.636	443.42	449.74		
		Leachate	Monitorin	g Points		
MW-9	2409452 / 545411.2	596.29	498.49	Dry		
MW-10	2409664 / 545430.8	594.155	495.79	495.79		
UL-1	2409014 / 545798.2	553.785	544.38	Dry		
LL-1	2409020 / 545789.2	553.39	528.79	532.49		
UL-2	2408874 / 545928	542.305	535.15	537.44		
LL-2	2408869 / 545936	540.732	529.83	530.60		
UL-3	2408805 / 546029.2	543.105	535.69	536.69		
LL-3	2408810 / 546021.1	541.198	530.47	Dry		

All TD and groundwater elevation are based off the most recent Jan, 2021 field activites or as-builts \* - Unknown if well is still in place Blank cells are unknown

## Table 2 Monthly Static Waterlevel Measurements Continental Cement Landfill

Permit Number 82-SDP-16-97P

Monitoring						[	Date					
Point ID	1/9/2020	2/11/2020	3/16/2020	4/7/2020	5/12/2020	6/9/2020	7/14/2020	8/11/2020	9/4/2020	10/13/2020	1/28/2021	2/22/2021
MW-1A	483.01	482.77	483.71	483.87	483.07	482.67	482.58	481.32	481.37	480.57	481.81	482.73
MW-3		470.27	473.45	470.95	468.54						495.05	501.57
MW-4	484.37	484.78	485.1	485.6	484.8	485.33	484.6	483.9	483.4	483.8	483.93	484.19
MW-5	486.68	487.05	487.5	486.92	486.49	487.39	487.34	483.32	481.59	485.29	486.71	486.37
MW-11	470.82	471.36	474.01	470.97	468.37	468.21	467.23	465.11	465.56	464.21	465.6	472.73
MW-12	474.98	472.86	476.04	474.86	475.05	475.05	474.43	473.26	471.86	473.31	474.14	474.79
MW-13	508.14		514.79	509.9	507.79	507.79	508.59	505.89	505.99	505.99	NM	NM
MW-14	474	474.15	474.66	474.65	473.54	473.95	473.71	472.2	472.3	472.5	473.11	473.98
MW-15	498.38	498.23	508.98	500.73	498.66	497.82	498.22	495.53	495.48	495.13	496.12	497.64
MW-16	471.2	471.16	471.56	472.11	471.16	471.36	470.72	469.19	468.36	469.16	470.57	471.64
MW-18	480.67	480.57	481.84	481.52	480.28	480.74	479.89	478.93	478.73	478.68	479.95	481.88
MW-3L	469.21	470.05	473.21	470.83	468.45	467.31	467.29	464.46	464.26	463.01	467.66	474.18
MW-4L	480.53	480.68	481.8	481.48	480.25	480.58	479.75	478.74	478.68	478.58	480.28	481.71
MW-7	469.28	468.08	469.71	469.59	466.98	466.98	466.63	463.18	463.58	462.73	466.16	469.56
MW-16L	465.87	466.71	469.37	465.52	461.67	462.82	461.9	458.97	459.09	458.72	462.66	471.07
MW-19	469.13	468.52	470.78	469.65	468.43	466.9	466.79	464.53	465.3	463.1	466.12	470.06
MW-1B	594.27	594.44	594.68	594.76	595.33	594.61	594.17	588.83	588.36	589.16	594.47	594.44
MW-2A	560.86	560.48	561.05	561.43	561.04	561.25	560.36	560.36	560.1	560.6	561.02	560.98
MW-2CR	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM
Q-Sump	453.74	453.72	455.44	453.75	453.21	453.31	453.64	447.07	447.07	455.08	455.19	449.74
Leachate Mon	itoring Point										-	
MW-9	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry
MW-10	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	495.89	495.94
UL-1	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry	545.07
LL-1	531.52	530.69	Dry	Dry	531.27	531.77	531.64	531.14	530.89	531.69	532.49	532.91
UL-2	536.34	536.99	537.09	536.08	NM	NM	NM	Dry	Dry	NM	537.44	537.47
LL-2	530.48	530.44	530.45	531.7	NM	NM	NM	530.53	Dry	NM	530.6	530.78
UL-3	Dry	535.85	536.13	535.99	NM	NM	536.34	Dry	Dry	537.81	536.69	536.52
LL-3	Dry	Dry	Dry	531.10	NM	NM	Dry	Dry	Dry	Dry	Dry	Dry

NM - Not Monitored

msl - mean sea level



Table 3



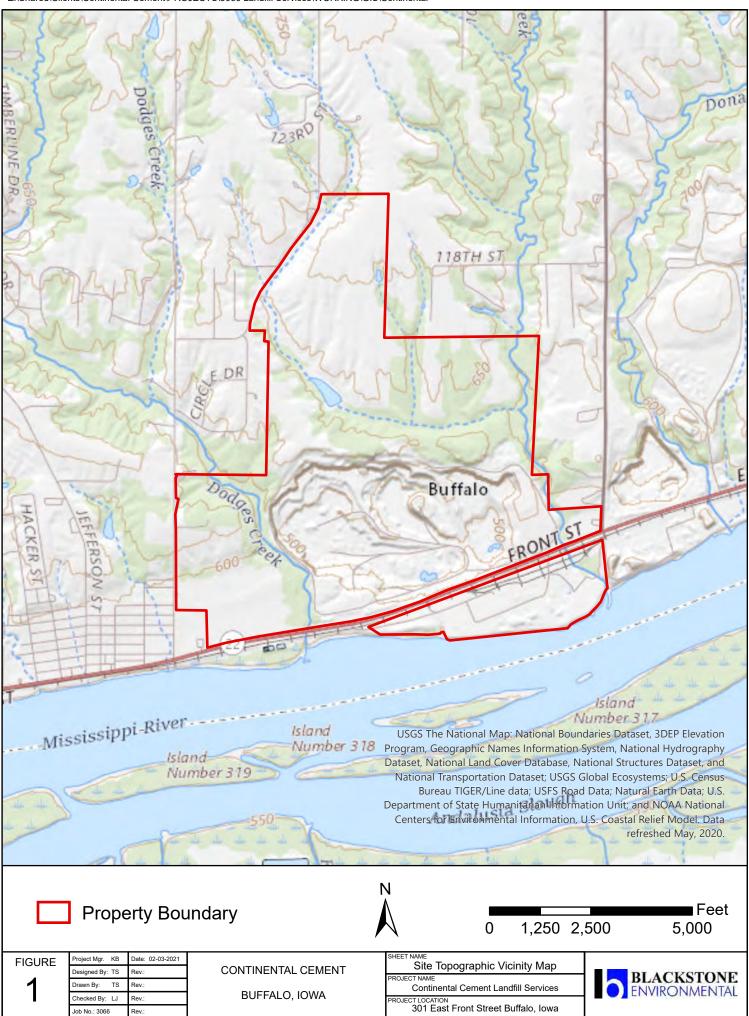
## Sample Method, Collection, Preservation, and Holding Time

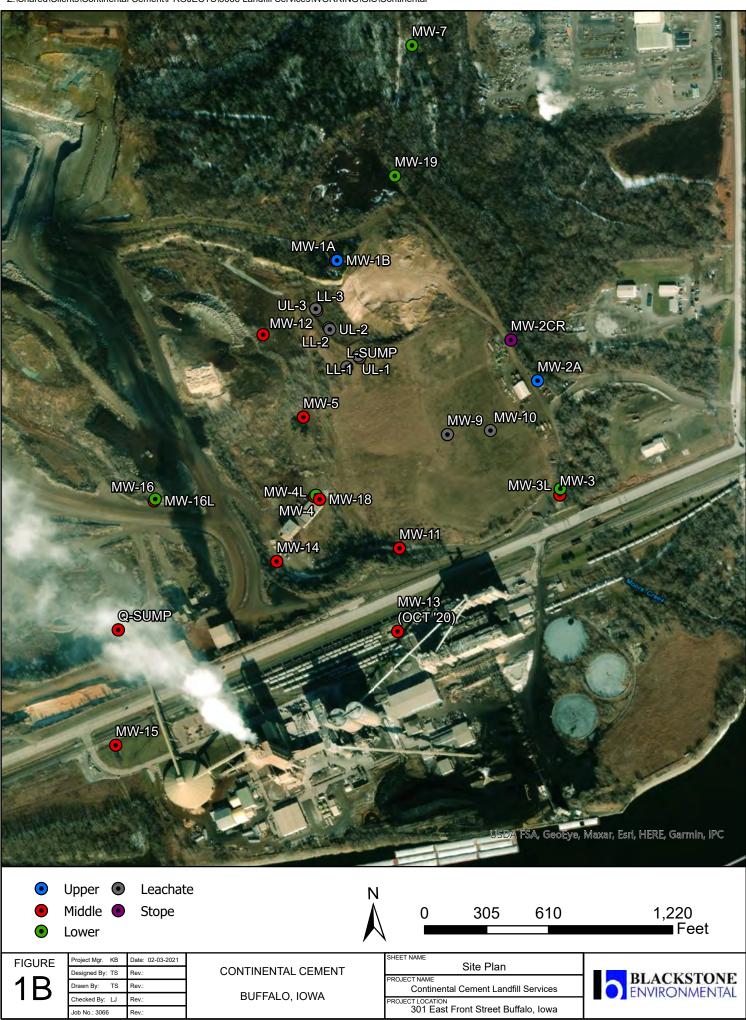
Continental Cement Landfill Permit Number 82-SDP-16-97P

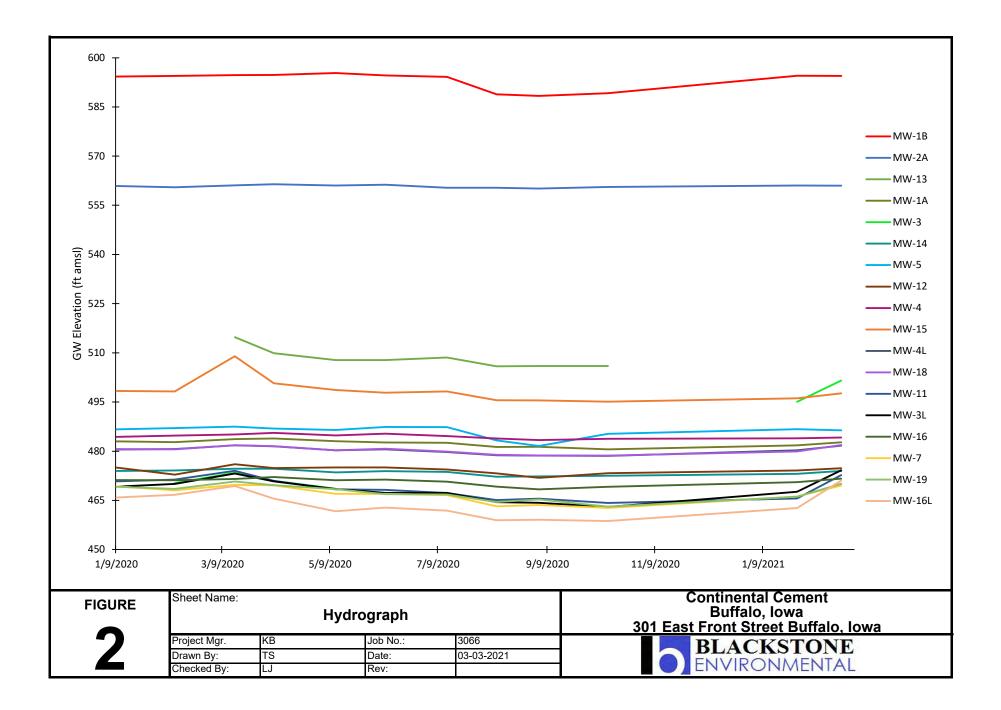
Analysis	Method	Containers	Preservatives	Holding Times
Total Metals	EPA Method 6010B	500 mL plastic	HNO3 pH<2; Cool 4 degrees Celsius	6 Months
Chloride	SM4500	125 mL plastic	Cool 4 degrees Celsius	28 Days
Total Dissolved Solids	SM 2540	500 mL plastic	Cool 4 degrees Celsius	28 Days
Sulfate	9056	125 mL plastic	Cool 4 degrees Celsius	28 Days
Nitrate/Nitrite	SM 4500	125 mL plastic	Cool 4 degrees Celsius	48 Hours
Phosphorous	EPA 365.1	125 mL plastic	H2SO4 pH<2; Cool 4 degrees Celsius	28 Days

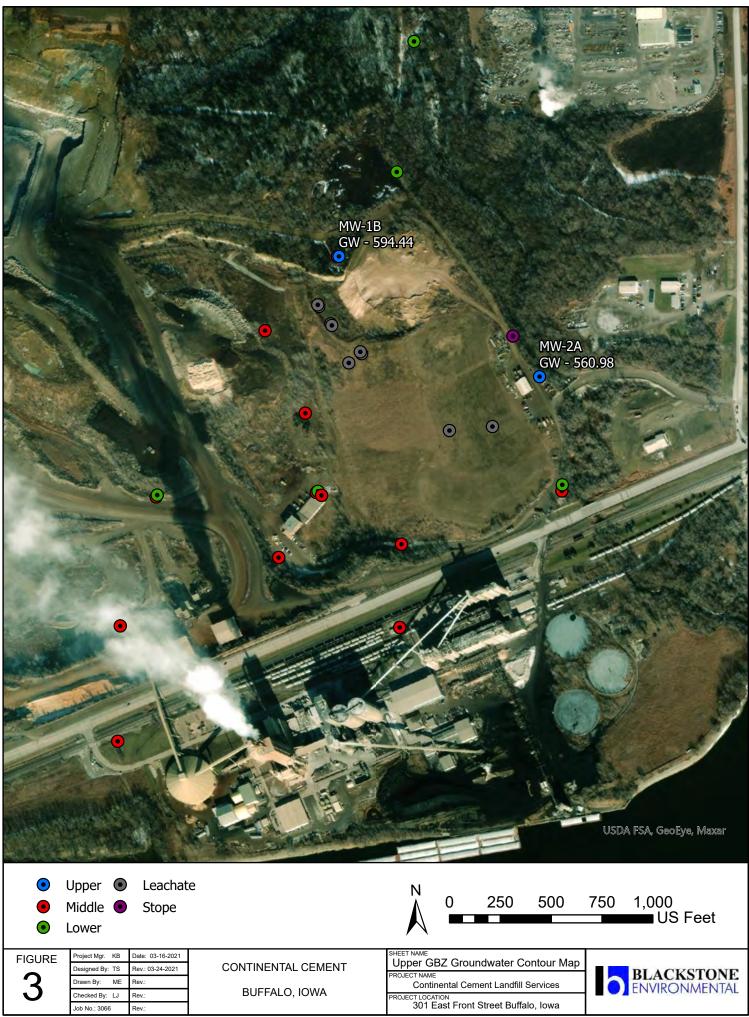
**FIGURES** 

**CONTINENTAL CEMENT COMPANY** 

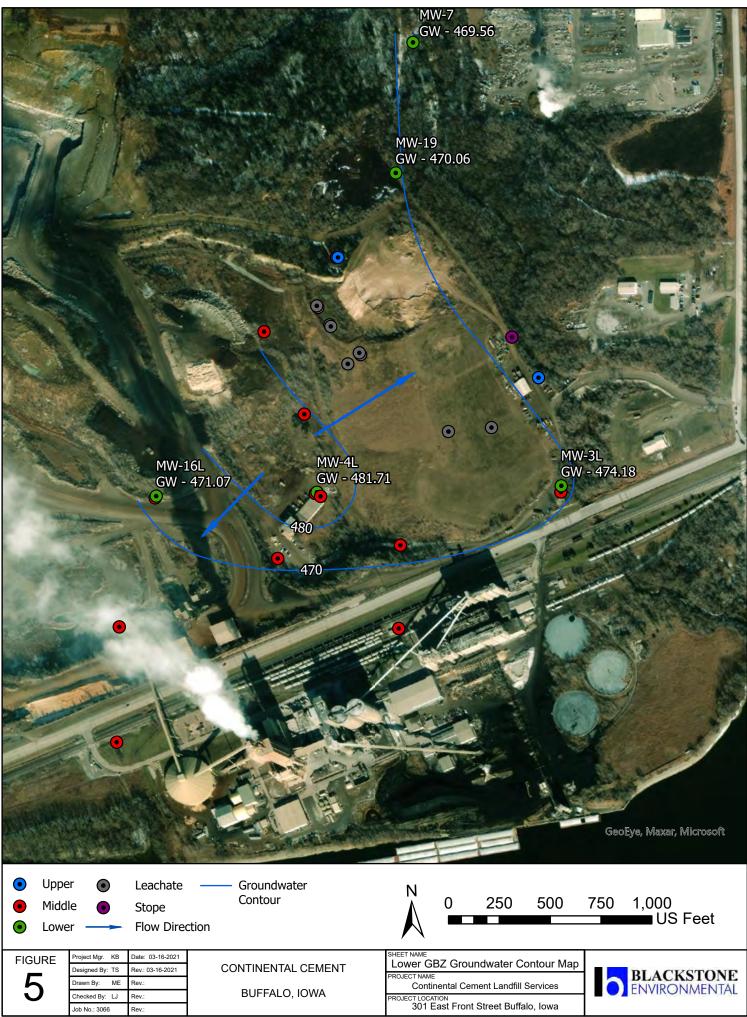




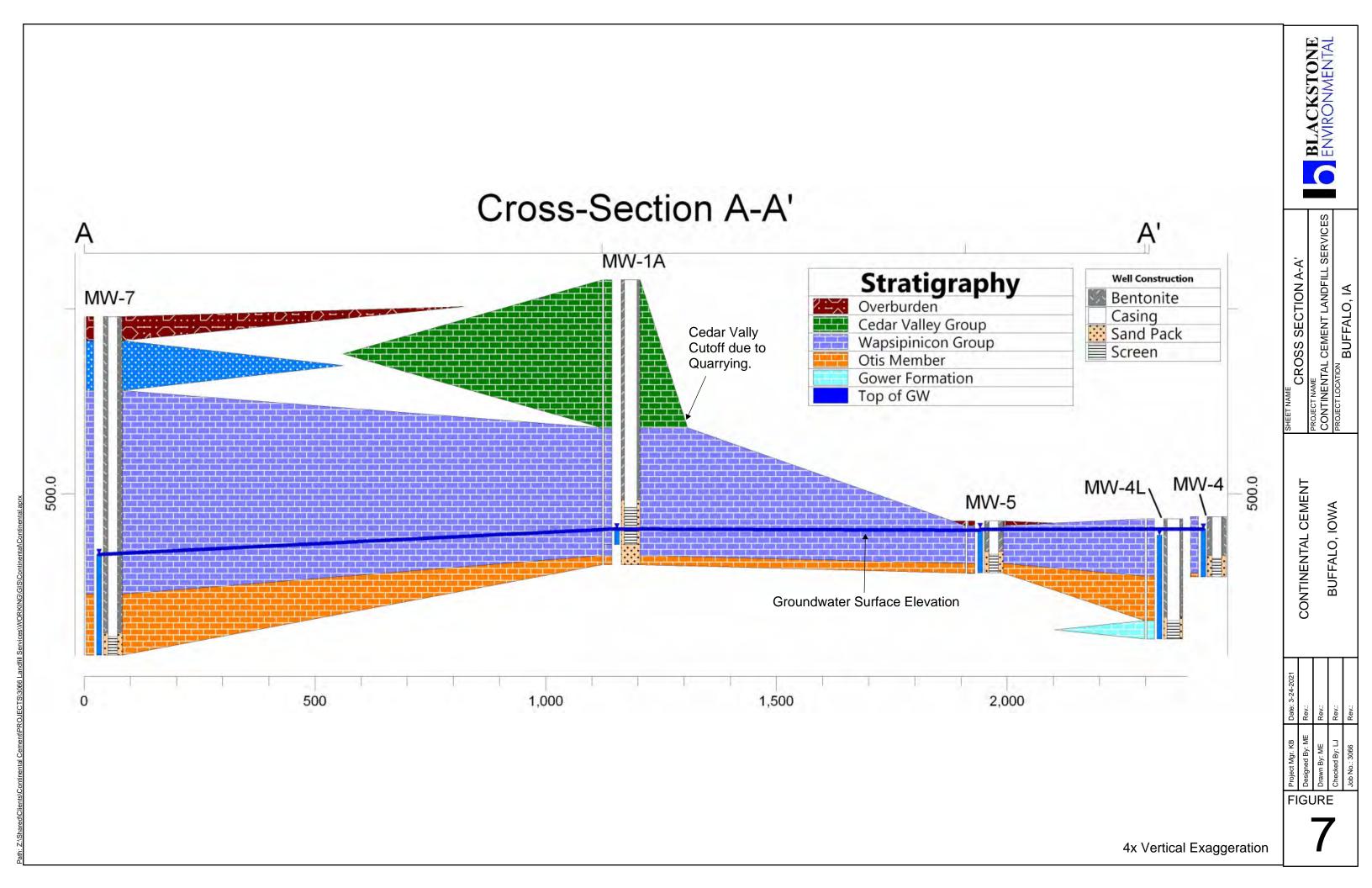


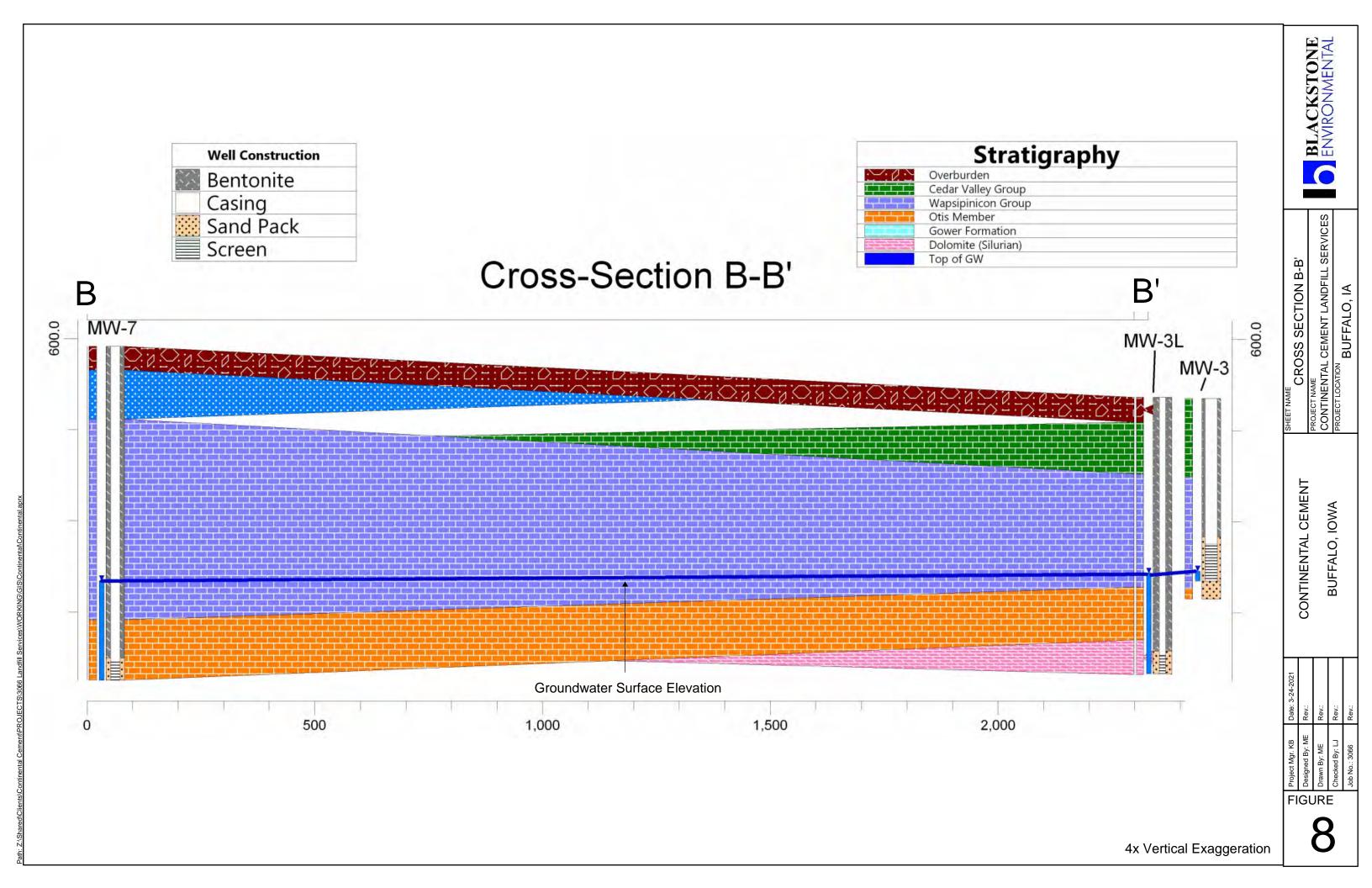


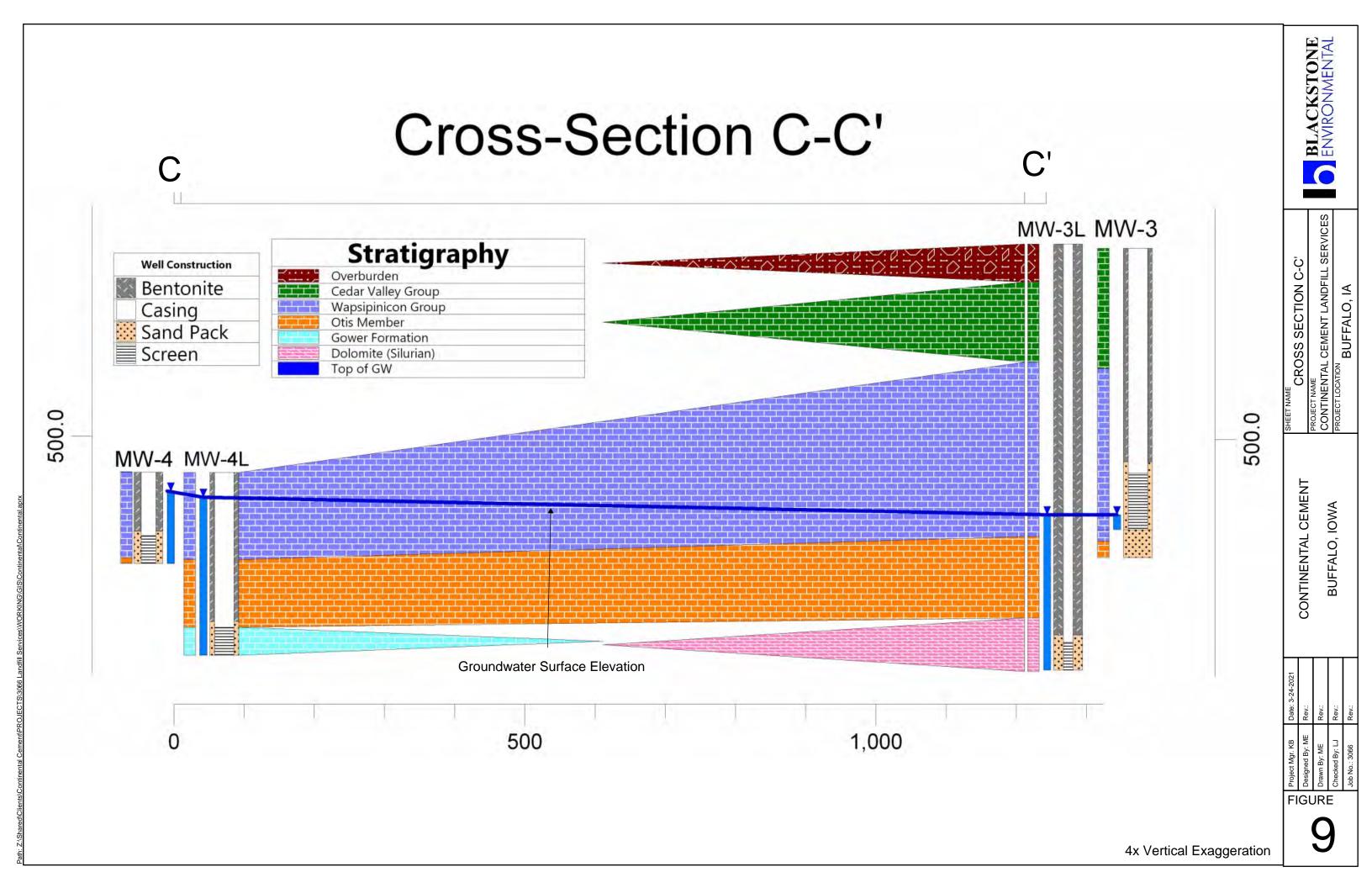




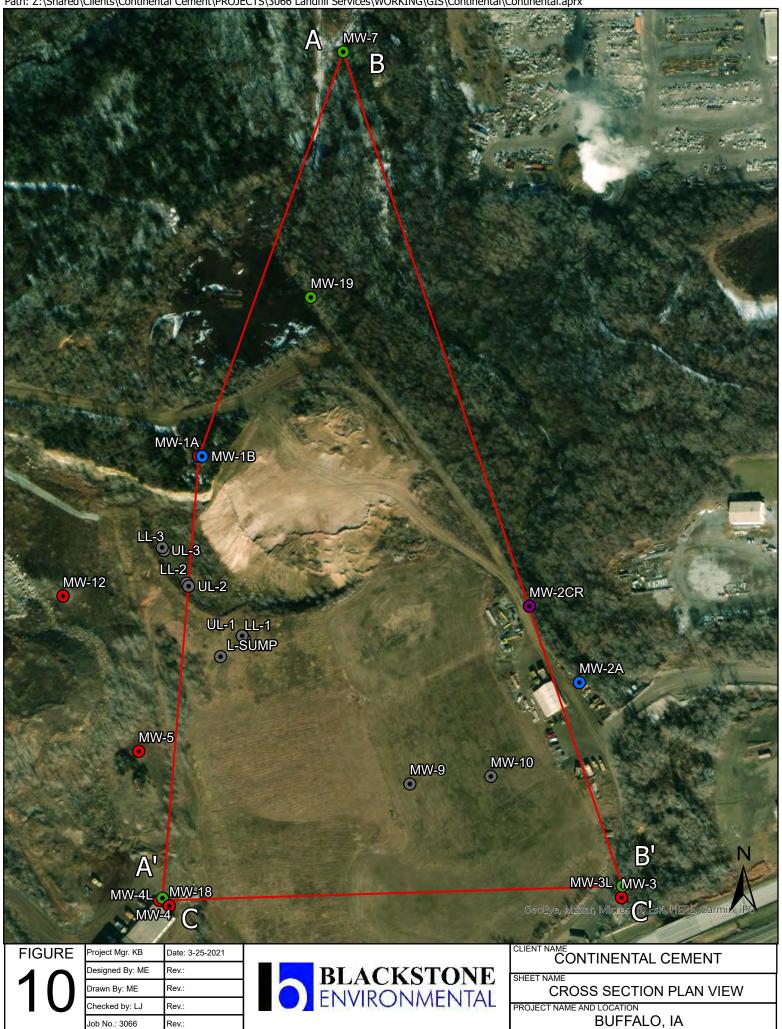


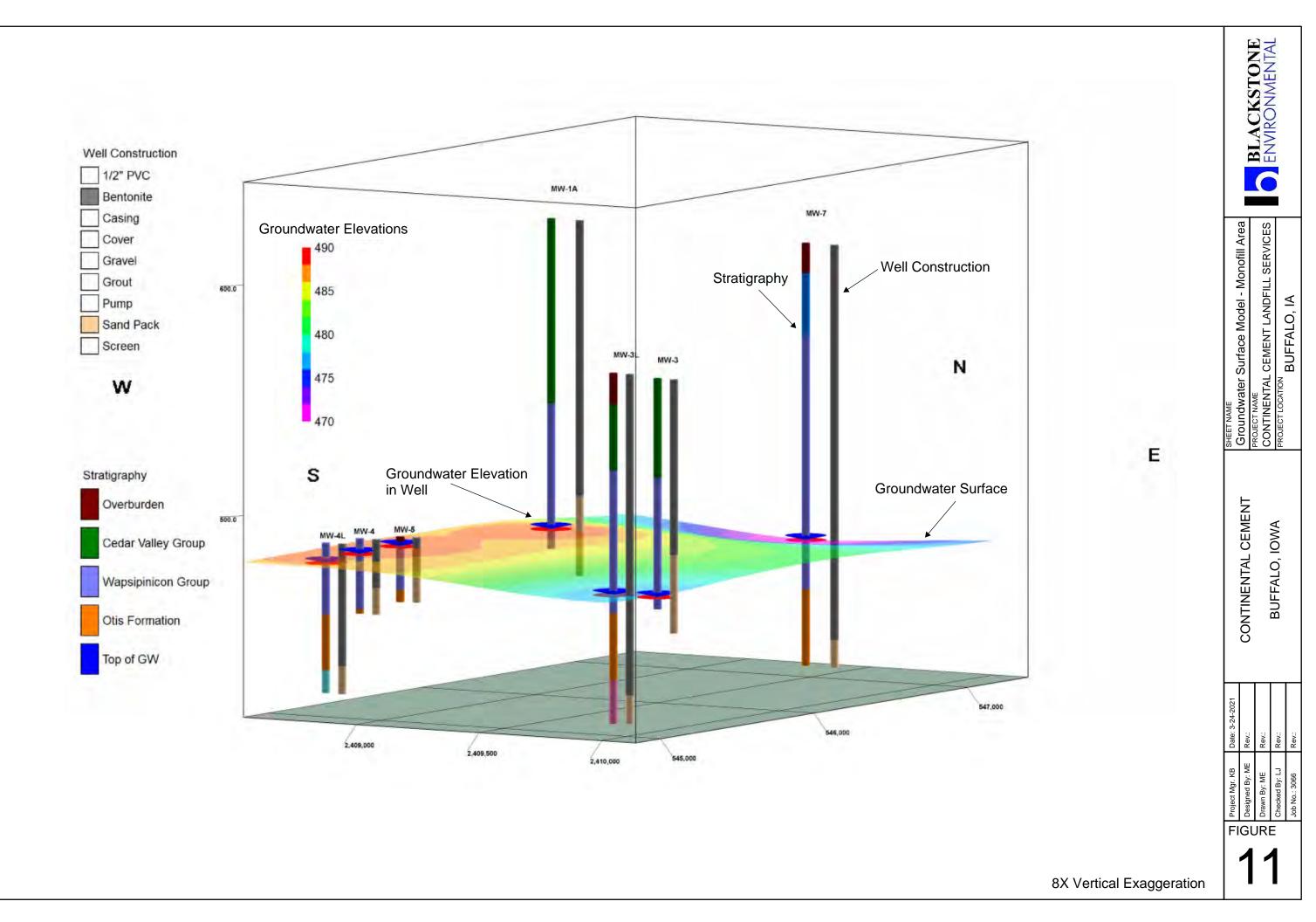




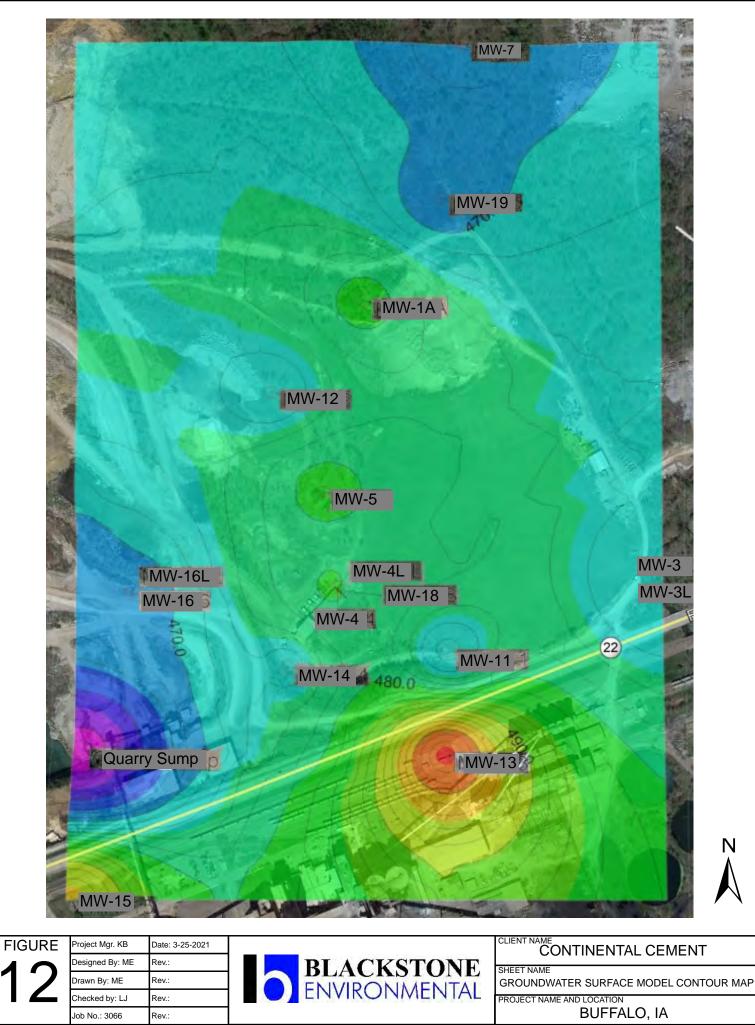


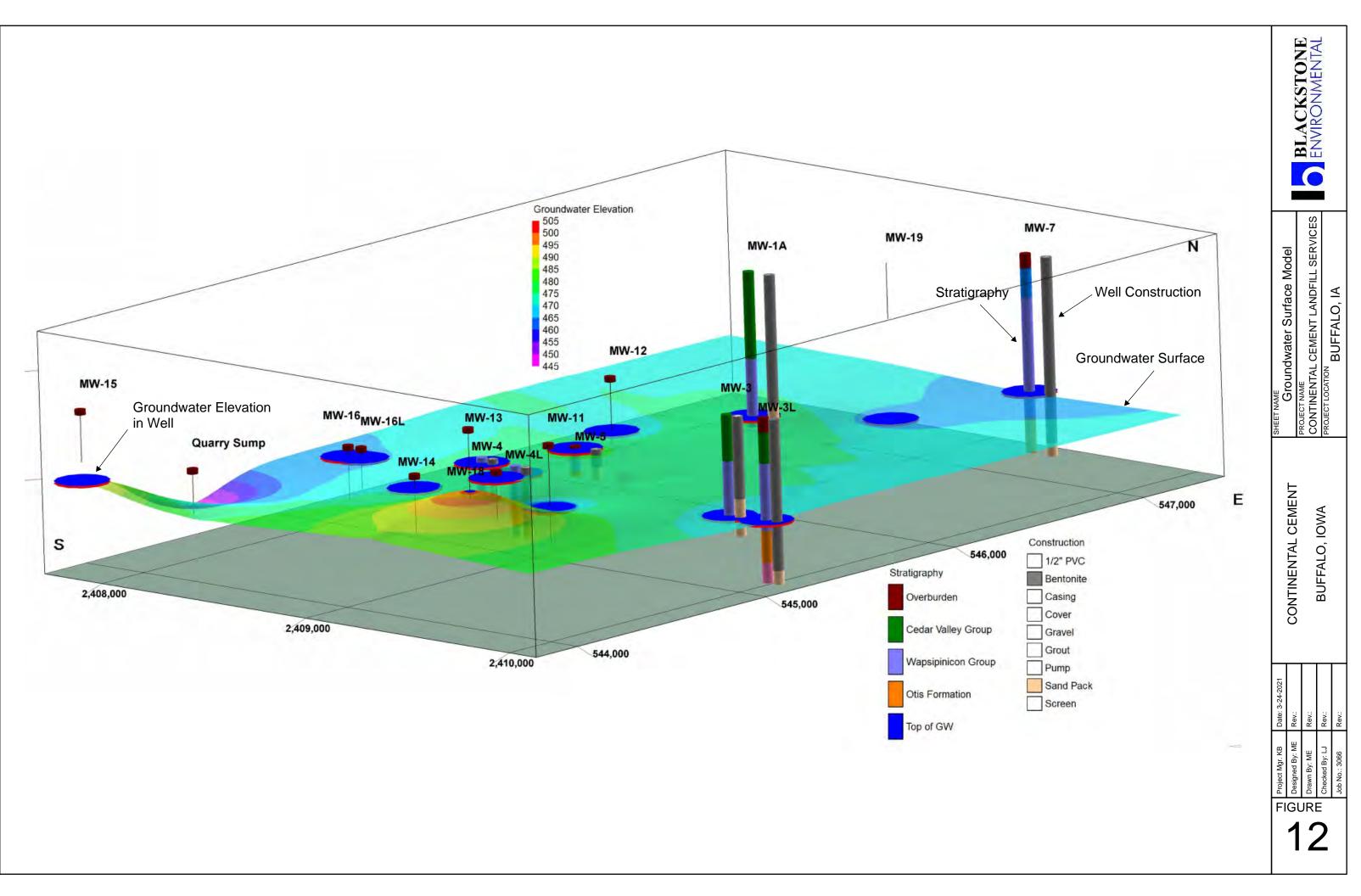
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## **APPENDIX A**

CONTINENTAL CEMENT COMPANY Boring Logs and Well Construction Diagrams

(WL-OI) Page 1 of 5

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

HOLE DESIGNATION: MW1A-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WC CRA SUPERVISOR: D. SHEILD

DEPTH fl. BG	DESCRIPTION OF STRATA	ELEV. fl. AHSL	MONITOR	ਲਵ	i ee	ae ≻		. M
	GROUND SURFACE REFERENCE POINT (Top of Riser)	615.50 616.95	*	BEDROCK	RUN NUMBER	RECOVERY	RODX	HATER RETURN X
2.5	LIMESTONE (CEDAR VALLEY GROUP), dolomitized, sandy, hard, vuggy, fossilized, reddish tan, andelusia member		BENTONITE GROUT			æ		
-5.0			BENTONITE				8	
-7.5	in the second se						8 <sup>6</sup>	393
-10.0	9 2	<u>.</u>			1	85	5	13
2.5			3. 0					
15.0		•	BOREHOLE			£ 8	2	2
-17.5	<ul> <li>calcarenite, medium to fine grained, grey to tan, fossiliferous, stratified and interbedded with calcilutite, silty to muddy, cou falls member</li> </ul>		3" Ø BOREHOLE J" STEEL CASING SET Ø I7II BGS					
-20.0			SET 0 1711 BGS					
-22.5	4 <sub>2</sub>					-		2.5
-25.0			2" PVC PIPE		2	95	-	
-27.5			PIPE			5J	-	
-30.0								,
.5	ē.						93	27
	- interbedded argillaceous calcites						6	÷
<u>لا</u>	OTES: MEASURING POINT ELEVATIONS MAY CHANGE WATER FOUND ♀ STATIC WATER LEVEL	E: REFER '	TO CURRENT ELEVATION TA	BLE	2	95	17	4 5 7 8 8

(WL-01) Page 2 of 5

1

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

HOLE DESIGNATION: MW1A-95 DATE COMPLETED: FEBRUARY I, 1995 DRILLING METHOD: WC CRA SUPERVISOR: D. SHEILD

IL BIS     DESCRIPTION OF STRATA     IT. AMSL     INSTALLATION     VOID USE	untossikiterous beds, vuggy calcite replacements, various bugs of orau and	2		BEOR	NUMBIN	COR	ROD	ATE
distinctly stratified ross and undrossifierous and ten, rapid member and solon member     Image: Constraint of the second member and solon member       -40.0       -40.0       -42.5       -45.0       -47.5       -50.0       -55.0       -55.0       -56.0       -57.5       -60.0       -57.5       -60.0       -61.0       -62.5       -55.0       -55.0       -56.0       -57.5       -60.0       -57.5       -60.0       -57.5       -60.0       -57.5       -60.0       -57.5       -60.0       -57.5       -60.0       -61.0       -7.5       -62.5       -65.0	untossikiterous beds, vuggy calcite replacements, various bugs of orau and						1	1 72
-42.5 -45.0 -47.5 -50.0 -52.5 -55.0 -57.5 -60.0 -62.5 66.0	6.5 C.5			22	2	8	2 6	
-42.5 -45.0 -47.5 -50.0 -52.5 -55.0 -57.5 -60.0 -62.5 66.0			BENTONITE				3	
62.5 65.0								
62.5 65.0		12						
62.5 65.0								
62.5 65.0		÷	3" 0	1		-		1
62.5 65.0			BOREHOLE		3	95	17	
62.5 65.0					56			
62.5								
62.5 65.0			2" PVC			•		
			PIPE					
67.5								
								11000
NOTES:		MEASURING POINT ELEVATIONS MAY CHANG WATER FOUND V STATIC WATER LEVEL	MEASURING POINT ELEVATIONS MAY CHANGE: REFER WATER FOUND & STATIC WATER LEVEL #	MEASURING POINT ELEVATIONS MAY CHANGE: REFER TO CURRENT ELEVATION TA	MEASURING POINT ELEVATIONS MAY CHANGE: REFER TO CURRENT ELEVATION TADIE	MEASURING POINT ELEVATIONS MAY CHANGE: REFER TO CURRENT ELEVATION TADLE	MEASURING POINT ELEVATIONS MAY CHANGE: REFER TO CURRENT ELEVATION TADLE	MEASURING POINT ELEVATIONS MAY CHANGE: REFER TO CURRENT ELEVATION TAGES

(WL-01) Page 3 of 5

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

HOLE DESIGNATION: MWIA-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WC CRA SUPERVISOR: D. SHEILD

.

DEPTH 11. BGS	DESCRIPTION OF STRATA	ELEV. fl. AMSL	MONITOR INSTALLATION	VAL	~ #	E RY X	 	× Ez
			•	BEDROCK INTERVAL	RUN NUMBER	RECOVERY	ROD	HATER RETURN X
-72.5			BENTONITE GROUT			α	•	
-75.0			BENTONIT		3	95	17	
-77.5							80	
-80.0	LIMESTONE (WAPSIPINICON GROUP), massive, microspar to intraclastic	535.50			_			Ś
-82.5	stratified beds, brecciated and fractured fossiliferous with pyrite and calcite replacements of fossils and infilling of fractures and breccia matrix, hardened beds are stybility gravita, daymonort		3" 0 BOREHOLE					
-85.0	member	3						3
-87.5			3" Ø BOREHOLE				्र स	
-90.0			BOREHOLE			5		1
-92.5					4	95	10	
-95.0							-	
-97.5			2" PVC PIPE		1			
-100.0								
1025			2.2.2.2 2.2.2.2			2	13	
-102.5				en de		5		
6	IDTES: MEASURING POINT ELEVATIONS MAY CHANG WATER FOUND V STATIC WATER LEVEL	E: REFER	TO CURRENT ELEVATION TA	<u> </u>				10 D

(WL-01) Page 4 of 5

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

.

HOLE DESIGNATION: MW1A-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WC CRA SUPERVISOR: D. SHEILD

DEPTH fl. BGS	DESCRIPTION OF STRATA	ELEV. ft. AMSL	MONITOR INSTALLATION	BEDROCK	RUN NUMBER	CORE RECOVERY X	×	RN X
: 10	•		•	BEDI	N N	RECOV	ROO	NATER RETURN X
-107.5			GROUT	E			(8) 2 <sup>9</sup>	
-110.0	•		BENTONIT GROUT 3" Ø BOREHOLE					
-112.5								1
-115.0					4	82	10	5
-117.5			2" PVC	)) }		90	8	
120.0		2 . J					20 12	
-122.5	<ul> <li>highly fractured weathered and flaggy on upper contact stratified interbedded arenitic, petroliferous and prominently stylolitic, some shaley beds white to gray</li> </ul>		SAND PACK					
-125.0	to lan, some beds are more crystaline toward the lower contact, spring grove member							
-127.5						•		
-130.0					5	95	ः 12	-
-132.5			WELL SCREEN					
135.0								1
-137.5	<ul> <li>dotomitic, brecciated and fractured bedded, argillaceous to arenitic</li> </ul>						8	2
	limestone, some fossils, quartz filling fractures				6	95	64	00 50

(WL-01) Page 5 of 5

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

#### HOLE DESIGNATION: MW1A-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WC CRA SUPERVISOR: D. SHEILD

DEPTH fl. BGS	DESCRIPTION OF STRATA	ELEV. IL AMSL	MONITOR INSTALLATION	ਨਿੱਖ	æ	×		5
			•	BEDROCK	RUN NUMBER	RECOVERY	Ra0 x	MATER
-142.5	distictly stratified lower contact with sandy, gray and tan beds, kenwood member	5	WELL SCREEN	8	Ċ.	0		
-145.0			5AND		6	95	64	, 8
-147.5			PACK			~	33	83
-150.0	LIMESTONE (OTIS FORMATION), finely bedded and argillaceous breccialed, vuggy and fractured with calcite filling vugs and fractured, bluish gray to tan	466,58	3"Ø BOREHOLE					385
j-152.5	13 	5			7	95 	20	
-155.0	END OF HOLE @ 153.9/1 BGS	- 461.58	SCREEN DETAILS Screened interval	ł				
-157.5			I23 to I43(t BGS Length: 2011 Diameter: 2" Slot Size: #10 Material: PVC Sand Pack;					22
-160.0			19 to 153,91t BGS Material: #30 Flint				S.	9
-162.5					•			
-165.0			×			3	3	-
-167.5								÷
-170.0								92
172.5	€							2
6	8) (5							

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5

## STRATIGRAPHIC AND INSTRUMENTATION LOG (BEDROCK)

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA (WL-O2) Page 1 of 2 HOLE DESIGNATION: MW18-95 DATE COMPLETED: FEBRUARY 21, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD

	GROUPD Store to -	IL ANSL	INSTALL		Įõ.∜	SE	R E E E E	×	<b>S</b>
	GROUND SURFACE REFERENCE POINT (Top of Riser)	815.49 818.51	• <b>1</b> =7		BEDROCK INTERVAL	RUN NUMBER	CORE RECOVERY 3	ROD	NATER RETURN X
2.5	LIMESTONE (CEDAR VALLEY GROUP), dolomitized, sandy, hard, vuggy, fossilized, reddish tan, andelusia member		N N N N N N N N N N N N N N N N N N N	•					
.0				- BENTONITI GROUT		•		-	
.5			1.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2						
0.0				- 5" Ø BOREHOLE					1.14
2.5									
5.0		-		2" PVC PIPE		-			
.5	<ul> <li>interbedded calcilutite and fossiliterous beds, silty to muddy, cou falls member</li> </ul>								
0.0									
2.5				SAND					
5.0				PACK				-	•
7.5				WELL					
0.0				SCREEN					
2.5									
NO	TES: MEASURING POINT ELEVATIONS MAY CHANG WATER FOUND Q STATIC WATER LEVEL	E: REFER		EVATION T					

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

#### HOLE DESIGNATION: MW18-95 DATE COMPLETED: FEBRUARY 21, 1995 DRILLING METHOD: WR CRA SUPERVISOR: O. SHEILD

DEPTH fl. BGS	DESCRIPTION OF STRATA	ELEV. fl. AMSL	MONITOR INSTALLATION	X YK	28	R RY X	×	×
			F	BEDROCK INTERVAL	RUN NUMBER	RECOVERY	Rao x	NATER RETURN X
-37.5	- interbedded argillaceous calcilutite, fossiliferous, wilh calcite filled vugs, gray and tan, rapid member		WELL SCREEN SCREEN SAND PACK				105	- 2 - 2
-40.0	END OF HOLE @ 40.0ft 8GS	575.49	SCREEN DETAILS					
-42.5			Screened interval: 20 to 4011 BGS Length: 2011 Diameter: 2" Slot Size: #10 Materiat: PVC					8 8
-45.0	~		Sand Pack: 16 to 41ft BGS Material: #30 Flint	23			- 18	525 125
47.5			an a				×	82
-50.0				8				
-52.5	·	C.					*	22
-55.0							i X	
-57.5	b	5	φ.			2	5	
-60.0							8	, <sup>1</sup> 2
-62.5								
-65.0	×		· · ·					192
37.5	·			~			а 1911	5.00
	NOTES: MEASURING POINT ELEVATIONS MAY CHAN WATER FOUND ¥ STATIC WATER LEVE	GE: REFEI	R TO CURRENT ELEVATION	ABLE			ði C	

(WL-02) Page 2 of 2

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

#### HOLE DESIGNATION: MW2A-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WC 12.1

CRA SUPERVISOR: D. SHEILD

DEPTH ELEV. DESCRIPTION OF STRATA HONITOR **fL BGS** ж BEDROCK INTERVAL **IL AHSL** INSTALLATION 24 RUN NUMBER CORE RECOVERY RETURN æ **0**02 GROUND SURFACE 587\_37 REFERENCE POINT (Top of Riser) zí, 588.22 ţ SM-SAND (FILL), some gravel, little sill, fine to medium grained, brown, moist .... 1 ľŻ ·2.5 : BENTONITI -5.0 2 GROUT -7.5 5" Ø -10.0 BOREHOLE SC/SM-SAND (FILL), silty, some clay, 577.37 trace gravel, fine to medium grained, brown, moist 12.5 1.1.1. ÷ ... - 14 -15.0 1 2" PVC PIPE -17.5 SM-SAND (FILL), some sill, little gravel, 569.87 fine to medium grained, brown, moist -20.0 -22.5 -25.0 LIMESTONE (CEDAR VALLEY GROUP). 562.37 3" STEEL interbedded calcilutite and arenilic, CASING fossiliferous, very fine to coarse grained, SET @ 25/1 BGS slightly stylolitic and fractured with -27.5 traces of calcite and pyrite filling fractures, gray and tan, rapid and solon member 3. 0 -30.0 BOREHOLE -32.5 SAND 2 PACK ; MEASURING POINT ELEVATIONS MAY CHANGE; REFER TO CURRENT ELEVATION TABLE NOTES: WATER FOUND ¥ ÷ انع ب STATIC WATER LEVEL

(WL-03) Page I of 4

(WL-03) Page 2 of 4

PROJECT NAME: LAFARGE PROJECT NUMBER: 8031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

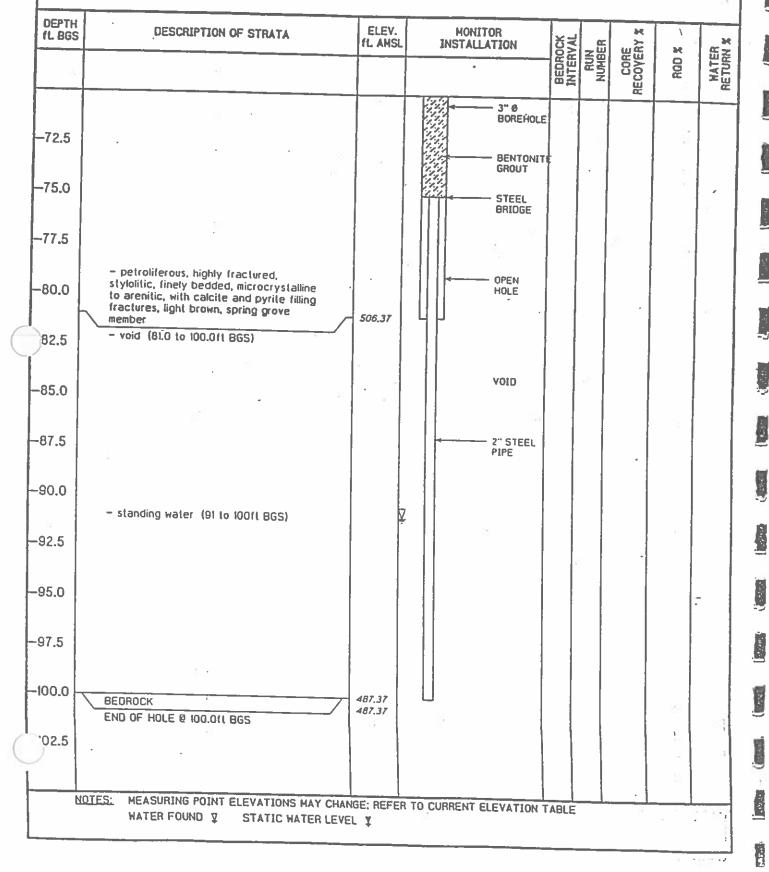
#### HOLE DESIGNATION: MW2A-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WC CRA SUPERVISOR: D. SHEILD

DEPTH fl. 865	DESCRIPTION OF STRATA	ELEV. fl. AMSL	HONITOR INSTALLATION	NAL VAL	N BER	RE ERY X		ž X X
	12. 		đ	BEDROCK INTERVAL	RUN NUMBER	RECOVERY	RGD <b>X</b>	HATER RETURN X
-37.5	15 +0 - 10 <b>X</b>							
-40.0			SAND				3	
-42.5	LIMESTONE (WAPSIPINICON GROUP), argillaceous to microspar, compact crystaline, interbedded and fossiliterous, abundant stylolites with vugs and abundant fractures, locally brecciated	546.37						
-45.0	with pyrite and calcite healing fractures and voids, gray to light brown, davenport member				<b>e</b> :		1	
47.5					43	ماينة من ال	12	
-50.0		· T	WELL					
-52.5		.1				ŝ		
-55.0							- <sup>-10</sup>	
-57.5						<u>,</u>	93	
-60.0			3" Ø BOREHOLE					
-62.5	×-				85			
-65.0					R		22	14
67.5			BENTONIT	25			œ.	1017
	NOTES: MEASURING POINT ELEVATIONS MAY CHAN	NGE: REE	R TO CURRENT ELEVATION	TADI				
	WATER FOUND ¥ STATIC WATER LEVE	EL ¥	TO COMENT ELEVATION	1 AUL	=			

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

#### HOLE DESIGNATION: MW2A-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WC CRA SUPERVISOR: D. SHEILD

(WL-03) Page 3 of 4



"ROJECT NAME: LAFARGE ROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

#### HOLE DESIGNATION: MW2A-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WC CRA SUPERVISOR: D. SHEILD

fL BGS	DESCRIPTION OF ST		ELEV. IL AMSL	MONITOR INSTALLATION	BEDROCK INTERVAL	RUN NUMBER	CORE RECOVERY X	R00 X	MATER RETURN X
			- 23	ж.	a.r	ž	RECI	, <del>CC</del>	×₩
-107.5	÷	्र • मेरे य	8 1 1	SCREEN DETAILS Screened Interval: 34.6 to 64.61t BGS Length: 301t Diameter: 2" Slot Size: #10 Naterial: PVC					
-110.0		17		Sand Pack: 30 to 671t BGS Naterial: #30 Flint					
8									- 6
-112.5								8.°	2
-115.0	92		• ®				s.		
								2	8
J.5									70
120.0			•				20		
122.5				24					
125.0		а. 192							-
127.5		2			~			3	
130.0									
132.5	*		-				ľ		
135.0								3	
.5	Υ.	ā.						ł	ł

(WL-03) Page 4 of 4

(WL-04) Page 1 of 4

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

HOLE DESIGNATION: MW2B-95 DATE COMPLETED: FEBRUARY 21, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD

fL BGS	DESCRIPTION OF STRATA	ELEV. ft. AHSL	MONITOR INSTALLATION	VAL	Z W W	ERY X	અ ં	er.
	GROUND SURFACE REFERENCE POINT (Top of Riser)	587.21 589.61	·	BEDROCK INTERVAL	RUN NUMBER	RECOVERY	Râo	MATER
	SM-SAND (FILL), some gravel, fine to medium grained, brown, moist					0	-	
2.5	ч <sup>а</sup> .	×					00 13	
5.0		12	BENTONITI GROUT				10	
7.5							84.5 1	
10.0			S" Ø BOREHOLE	<b>1</b> 0			Ÿ.	<u></u>
	SC/SM-SAND (FILL), silly, some clay, trace gravel, fine to medium grained, brown, moist	577.21		0			36.14	
12.5	~						-	
15.0		830	Z PVC PIPE					
17.5	SM-SAND (FILL), some silt, little gravel, line to medium grained, brown, moist	569.71	BENTONITI GROUT S" 8 BOREHOLE Z 2" PVC PIPE					
20.0								
22.5								
25.0								
27.5	LIMESTONE (CEDAR VALLEY GROUP), interbedded calcilutite and arenilic,	560.21	J" STEEL CASING SET @ 2711 BGS					
30.0	fossiliferous, very fine to coarse grained, slightly stylolitic and fractured with traces of calcite and pyrite filling	e.						
32.5	fractures, gray and tan, rapid and solon member	:	BOREHOLE					Ł
J2.J	·		SAND PACK					S. i -
L	DIES: MEASURING POINT ELEVATIONS MAY CHAI WATER FOUND X STATIC WATER LEVE	NGE: REFE	TO CURRENT ELEVATION			!	8	•••••••••••••••••••••••••••••••••••••••

(WL-04) Page 2 of 4

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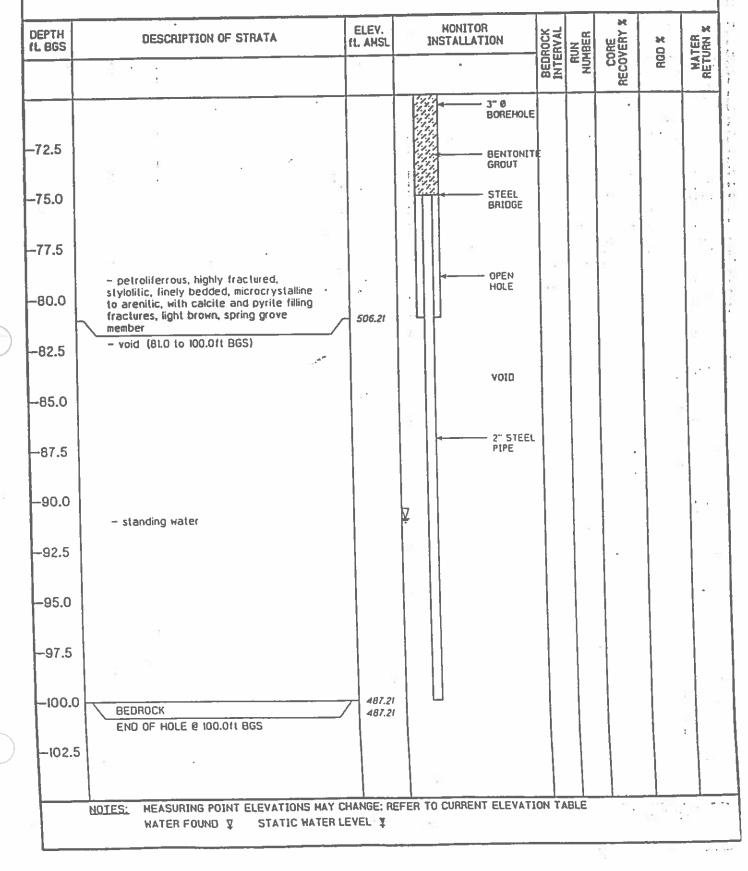
PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

#### HOLE DESIGNATION: MW2B-95 DATE COMPLETED: FEBRUARY 21, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD

DEPTH	DESCRIPTION OF STRATA	ELEV. fl. AMSL	MONITOR INSTALLATION	BEDROCK	RUN NUMBER	CORE RECOVERY X	ROD X	TER IBN K
		- 22	۰ 	INTE	S N N	RECO	8 B 6	WATER
37.5	a . G	20 44			8 - R			
40.0	X 8	:0	SAND			* ///		а "А
42.5	LIMESTONE (WAPSIPINICON GROUP), argillaceous to microspar, compact crystaline, interbedded and fossiliterous, abundant stylolites with vugs and abundant fractures, locally brecciated	- 546.21					T -	
45.0	wilh pyrite and calcite healing fractures and voids, gray to light brown, davenport member						2	
47.5		21				ي. 1999 م.)		22
50.0			WELL SCREEN	÷00				
52.5								
55.0							÷	
57.5						3	i di	
·60.0			3" Ø BOREHOLE				2	-8
-62.5							$\times$	
-65.0						13	a <sup>2</sup>	
-67.5	¥ 		BENTONIT GROUT	TE.			4	

(WL-04) Page 3 of 4

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA HOLE DESIGNATION: MW2B-95 DATE COMPLETED: FEBRUARY 21, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD



PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

## HOLE DESIGNATION: MW2B-95 DATE COMPLETED: FEBRUARY 21, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD

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#2 5 N 55 N

DEPTH fl. Bgs	DESCRIPTION OF STRATA	ELEV. ft. AMSL	HONITOR INSTALLATION				_6	× ×		
			22	BEDROCK INTERVAL	RUN NUMBER	RECOVERY	Ran	HATER		
-107.5	:		SCREEN DETAILS Screened Interval:					20		
-110.0	2. 42. Sa		Material: PVC Sand Pack: 32 to 6711 BGS Material: #30 Flint			1	2 2	1989		
-112.5							8 2	É		
-115.0	5						<u>s</u> (			
7.5				-						
-120.0				59						
122.5										
125.0										
127.5			a							
130.0	2					15		56		
32.5			5							
135.0							3	20 20		
.5	· .		3				1			
<u> </u>	TTES: MEASURING POINT ELEVATIONS MAY CHANG WATER FOUND ¥ STATIC WATER LEVEL	E: REFER ¥	TO CURRENT ELEVATION T	ABLE				1		

(HL-04) Page 4 of 4

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PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

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HOLE DESIGNATION: MW2C-95	
DATE COMPLETED: FEBRUARY 23, 1995	
DRILLING METHOD: WR	
CRA SUPERVISOR: D. SHEILD	

DEPTI fL BG	DESCRIPTION OF STRATA	ELEV. fl. AHSL	I	MONITOR INSTALLATION	VAL VAL	- 6	¥.		×
	GROUND SURFACE REFERENCE POINT (Top of Riser)	592.33 589.71			BEDROCK	RUN NUMBER	RECOVERY :	ROD X	MATER RETURN X
	SM-SAND (FILL), some sill and gravel, fine to medium grained, brown, moist						<u>ac</u>		
-2.5									
-5.0	a 6. Maria			BENTONITE PELLET SEAL					3
-7.5									
-10.0		20		BENTONITE PELLET SEAL SEAL SEAL SEAL SEAL SEAL SEAL SEAL				32 	i i
-12.5					14 14	-	-	2	
-15.0	· · · · ·								
-17.5				J" STEEL CASING				;	
-20.0									<u>.</u>
-22.5	LIMESTONE (CEDAR VALLEY GROUP), interbedded calcilulite and arenitic,	569.83		J" STEEL CASING					2
-25.0	fossiliferous, very fine to coarse grained, slightly stylolitic and fractured with traces of calcile and pyrite filling fractures, gray and tan, rapid and solon member			SET 0 22.811 BGS					
-27.5									
-30.0			-	3" Ø BOREHOLE				ور. ب	• %
-32.5	53 . Li	-3							
	NOTES: MEASURING POINT ELEVATIONS MAY CHANG WATER FOUND V STATIC WATER LEVEL	SE: REFER		RRENT ELEVATION TA					5 10 mp - 10 - 10 17 17 18 18 19 19 19 19 19 19 19 19 19 19 19 19 19

(WL-05) Page 1 of 3

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PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

### HOLE DESIGNATION: MW2C-95 DATE COMPLETED: FEBRUARY 23, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD

(WL-05) Page 2 of 3

DEPTH fl. BGS	DESCRIPTION OF STRATA	ELEV. fl. AMSL	MONITOR INSTALLATION	상 북	A RE	RY X	i. M	× Sz	2
			•	BEDROCK	RUN NUHBER	CORE RECOVERY	ROD X	HATER RETURN X	
37.5		~				85 •	55 5		
-40.0		2	3" 0				4		
-42.5	LIMESTONE (WAPSIPINICON GROUP), argillaceous to microspar, compact crystaline, interbedded and fossiliferous, abundant stylolites with vugs and	551,33 	BOREHOLE				5		
-45.0	abundant fractures, locally brecciated with pyrite and calcite healing fractures and voids, gray to light brown, davenport member		4			<u>ت</u>			
7.5	Δ.						₽ <sup>2</sup>		
-50.0		e <sup>lle</sup> a				-	-		
52.5							3		
-55.0 -57.5								*	
-60.0						2	£ _		
-62.5		1						=	
-65.0									
.5	2. X								
	NOTES: MEASURING POINT ELEVATIONS MAY CHAN WATER FOUND V STATIC WATER LEVEL	GE: REFER	TO CURRENT ELEVATION TA	BLE		7	10	1	

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

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	(WL-05) age 3 of 3
HOLE DESIGNATION: MW2C-95	¥8
DATE COMPLETED: FEBRUARY 23, 1995	Nashkar M
DRILLING METHOD: WR	
CRA SUPERVISOR: D. SHEILD	

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DEPTH ft. BGS	DESCRIPTION OF STRATA	ELEV. fl. AHSI		BEDROCK	RUN NUMBER	CORE RECOVERY X	R00 X	TER JRN X
	8		·	BEC	- NUN	RECOC	B B	MATER RETURN
-72.5	· · · · · ·	20 54				-		5253 12
-75.0	0 · · · · · · · · · · · · · · · · · · ·		3" Ø BOREHOLE			•	() 1	, 8
-77.5	~			8	: 			
-80.0	<ul> <li>petroliferous, highly fractured, stylolitic, finely bedded, microcrystalline to arenitic, with calcite and pyrite filling fractures, light brown, spring grove member</li> </ul>	•••		9 23 23	Sire:	7		•
-82.5	~ void (83.0 to 103.01t BGS)	509.33					е Д	<u>.</u>
-85.0		а 					1 X 14	
-87.5			V01D			,	24 14. 12	
-90.0								
-92.5		÷				3	,	
-95.0	- slanding water		2					
-97.5								8
-100.0							S	-
j <sup>102.5</sup>	BEDROCK END OF HOLE @ 103,511, BGS	488.83 488.83	<i></i>					
	NOTES: MEASURING POINT ELEVATIONS MAY CHAN WATER FOUND ¥ STATIC WATER LEVE	IGE; REFE L 및 문	R TO CURRENT ELEVATION T	ABLE		5 7		a san ta

(WL-06) Page 1 of 4

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

#### HOLE DESIGNATION: MW3-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD

OEPTH ft. BGS	DESCRIPTION OF STRATA	ELEV.	MONITOR	OCK	N BER	ie RY X	20 20	N. N.
	GROUND SURFACE REFERENCE POINT (Top of Riser)	587.09 589.17	•	BEDROCK INTERVAL	RUN NUMBER	CORE RECOVERY	Rad	HATER RETURN X
-2.5	LIMESTONE (CEDAR VALLEY GROUP), interbedded calcareous muds, silts and sandstones, very fine to fine grained, abundant fossils, corals, bivalves, some calcite replacement, trace of pyrite along fractures, beds range from 0.04 to 11.8" in thickness, trace of stylolites,		BENTONITI PELLET SEAL 4" Ø BOREHOLE 3" STEEL CASING 3" 0 BOREHOLE					
-5.0	some soft sediment brecciation, gray tones, rapid member						ж 2	
-7.5			3" STEEL CASING			24		1. 13
-10.0							2	4 - 22 - 2
-12.5	Ч •				•			
-15.0							10	4 P
-17.5								4
-20.0			3" Ø BOREHOLE		1	100	55	
-22.5						-		
-25.0	<ul> <li>very finely bedded, very fine calculites, from mudstone to wackestone fabric, more massively bedded, slightly</li> </ul>							
-27.5	fossiliferous, brecciated with pyrite and calcite filling fractures, solon member				2	100	55	
-30.0	· · · ·		2" PVC PIPE					
.32.5	<ul> <li>sandy, very fine to coarse grained, calculite, some shaley partings interspersed, trace of fossils, corals, brachiopods, crinoids and trilobites,</li> </ul>				2	100	i 55 .	
	NOTES: MEASURING POINT ELEVATIONS MAY CHA WATER FOUND ¥ STATIC WATER LEV		ER TO CURRENT ELEVATION	TABL	E			1

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

HOLE DESIGNATION: MW3-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD

(HL~06) Page 2 of 4

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fL BGS	DESCRIPTION OF STRATA	ELEV. fl. AHSL	I INS	OCK	N E B C	ERY X	×		
			0.*/)	•	BEDROCK INTERVAL	RUN NUMBER	CORE RECOVERY	RaD	NATER
-37.5	slightly fractured and brecciated with pyrite and calcite filling fractures and voids, vuggy, pyrite replacement of fossils, undulating bottom, gray and tan, solon member			•			ес С	1	Corrections
-40.0				BENTONIT PELLET SEAL		. 3	100.	55	2 <sup>3</sup>
-42.5									8
-45.0	LIMESTONE (WAPSIPINICON GROUP), interbedded sublithographic to brecciated beds, little fossils, some domal stromatolites in sandy to muddy beds, breccia fragments in upper portion range from 0.04 to 2.0", slightly	524.26							
-47.5	fractured with prominent stylolites, pyrite and calcite filling fractures, with some disseminated pyrite, colors are highly variable in individual beds of gray and tan to pink, davenport member		-					5	2
50.0				3" 0					
-52.5				BOREHOLE					
55.0									
57.5		20		121		4	100	55	
60.0									- )e
62.5				PIPE				8	
65.0		с 5							
67.5							i.	1	andigan (m. 1914
				INT ELEVATION 1					and an and an

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

#### Page 3 of 4 HOLE DESIGNATION: MW3-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD

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**DEPTH** DESCRIPTION OF STRATA ELEV. fL BGS MONITOR 24 BEDROCK ft. AMSL CORE RECOVERY INSTALLATION RUN NUHBER 38 NATER RETURN 5 æ Bon -72.5 BENTONIT PELLET 4 SEAL 100 55 , -75.0 - petroliferous and prominently flaggy or weathered in upper contact, highly stylolilic, finely bedded, with mudstone to -77.5 very fine sandstone, lower portion is highly brecciated and highly fractured and vuggy with abundant calcite, trace 2" PVC of pyrile, tan to tan gray, spring grove PIPE -80.0 Member J2.5 ... -85.0 5 100 33 SAND PACK -87.5 3" Ø -90.0 BOREHOLE -92.5 dolomitic, highly brecciated and fractured, some fossils, sandy, bedded, vuggy with quartz and a trace of pyrite filling vugs, breccia fragments from 0.04 to 3.2", with rounded to angular WELL -95.0 SCREEN fragments, gray to white with brown sandy beds, kenwood member -97.5 6 100 55 -100.0 2.5 LIMESTONE (OTIS FORMATION), finely 462.92 MEASURING POINT ELEVATIONS MAY CHANGE: REFER TO CURRENT ELEVATION TABLE NOTES: 100 10 WATER FOUND V STATIC WATER LEVEL Y

(HL-08)

(WL-08) Page 4 of 4

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

HOLE DESIGNATION: MW3-95 DATE COMPLETED: FEBRUARY 1, 1995 DRILLING METHOD: WR CRA SUPERVISOR: D. SHEILD

fil. BGS	DESCRIPTION OF STRATA	ELEV. fl. ANSL	HONITOR INSTALLATION	BEDROCK INTERVAL	RUN NUMBER	RE /ERY X	× 0	NATER
	100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100		•	BED	R R	RECOVERY	RaO	TAH A
-107.5	bedded, medium to very fine grained, sublithographic, trace of fossils, brachiopods, massively brecciated with prominent stylolites, some shaley beds, vuggy with abundant calcite, light bluish grey to dark grey to pink	24	SAND PACK		7	100	10	
-110.0 -	END OF HOLE @ 110.011 BGS	457.09	BOREHOLE		_			
-112.5	د. آن ا		SCREEN DETAILS Screened intervat: B0 to 1001t BGS Length: 201t Diameter: 2" Stot Size: #10 Material: PVC				10 M	
-115.0			Sand Pack: 76 to IIOtt BGS Material: #30 Flint					
-117.5			2 -	÷			*	
-120.0	2	3. 					- 23	
-122.5		-				•		
-125.0	50 50						20 30	
-127.5		1.1	3			•	2	
-130.0						2	1	
-132.5								
-135.0							η.	
-137.5	IES: MEASURING POINT ELEVATIONS MAY CHANG	40 20 11				-	N	1.1.1

			INTERNATIONAL LTD	OFFICE RE	EPORT	ON	IS	ITI	E INVEST	IGAT	ION		SHE	et . 1	OF 6,			
	BC	DNTRACT NO DRING NO DRTHING		reuster rt, Iowo				BORING	Date: N Tor:: L	Nov. 20, 1996 Lafarge/GSI 567.66 fta.sl. (Gr.)								
	/     	NPLE TYPES A AUGER SAMP H NASH SAMPL R ROCK CORE C CRREL BARR	е о с р д V	SHELBY TUBE THEIN WALL OPEN THEIN WALL PISTON STATIC WATER LEVEL		SAMPL	01 F/	isturi Vir 100			TEST INFORMATION PEXETROPETER kg/co2							
┢	_	3 SPLIT SPOD	¥¥	DYNAMEC WATER LEVEL		MPLES	_	ist I			Δ SPT BLOUS/0,3n							
	DEPTH (Ft)	SMBOL	DESCRIPTI	ON	11PE	CONDITION	NUMBCR	INTER LEVEL	PIEZONETER CONSTRUCTION DETAILS		2	0	30		<u>50</u>			
	0 -		SILTY SAND FILL: loos medium brown.	e, moist,		8	MU	NN				O CK-UP	50		id linit 90			
	3	35	SILT AND SAND: trace of gravel, medium stiff, n organic-rich (former to horizon).	noist, black							8" TE WI	Surfa 1Porar Th 6"	NDE H NILY STEE	DLE Casid _ Pipe				
	9		SAND AND SILT: little dark brown.	gravel, loose,		-	w.											
-1	12		GRAVEL AND SAND: Toose Timestone Fragments.	e, dry, rounded														
- 1	5		LIMESTONE (CEDAR VALLE) orgillaceous to arenace bedded, hard, dry, nedi	ous inter-		i I I					- 6"	BOREH	CLE					
- 1	.0										- 2"	SCH 4	PV.	C PIPE				
											. Ben Cem	TONETH ENT GI	- 0UT	PORTLA	0			
														_				

	ŀ	COMEX IN	ITERNATIONAL LTD OFFICE REP	ORT	ÓN	S	SITE	INVESTI			SHF	FT Z	OF 6
	BO	ONTRACT NO ORING NO ORTHING	4283 COMPILED BY M. Brek MW3L LOCATION Davenport, EASTING	ster	_		_	BORING DA CONTRACTO ELEVATION	ATE: Nov DR: Lof	. 20,	1996		
		NPLE TYPES A AUGER BAMPLE H HASH SAMPLE R ROCK CORE C CRREL BARREL S SPLIT SPOON	T SHELBY TUBE D THEN WALL OPEN P THEN WALL PISTON STATIC HATER LEVEL TOTMATEC WATER LEVEL		SAMPL	01 F/	NDITI ISTURE AIR DOD DST			ETROMET	ER kg/ci	MAT]	.ON
	iudoo 30	DBLLS SCIIL/RC	DESCRIPTION	TTPE on	NOLLEON	RUMBER	INTER LEVEL	PIEZONETER CONSTRUCTION DETAILS	LD X plestic i	init –	0.3n 30 R CONTEN	<u>η</u> 10 Π ± Ιigui	- <u>50</u> ., 50 d'iimit X
$\bigcirc$	- 30 - 33 - 36 - 39		LIMESTONE (CEDAR VALLEY GROUP) as above, with trace black medium sand sized grains, little fossils lcarrals), light grey.		2	2	3			5" 80	EHOLE		90
	- 45		LIMESTONE (WAPSIPINICON GROUP) arenaceous, dark grey	1							-	C PIPE	
	- 51 - 54		Limestone, argiliaceous, trace Fassils, light tan								ETE - GFOUT		
L	60 E												

k		EX IN	TERNATIONAL LTD. OFFICE REPO	ORT	ON	5	SITE	INVEST	[GAT	101		SI	EET	3 n	F 6
BC	)RING )RTHI	NGay	4283 COMPILED BY: М. Вген MW3L LOCATION Davenport, EASTING	ster				BORING DE CONTRACTO ELEVATION	ate: N Dr: L	DV .		1996			
	i liash 7 rock 7 crrei	r sample I sample	T SHELBY TUBE O THEN HALL OPEN P THEN HALL PISTON STATIC HATER LEVEL W DYNAMIC HATER LEVEL		SAMPL	C Fi Gi	NOITI Isture Air 000 0st				_	NFO		TIO	N
HLLDO	Smeol		DESCRIPTION	-	PLES		INTER LEVEL	PIEZDHETER CONSTRUCTION DETAILS	-i0	1	20 1045/0 20 14	30 Conte	3 	 0	<u>50</u>
-60 -63 -66 -69 -72 -75		SOTL/ROCK 70.0	LIMESTONE: as above, trace black sond groins, pyritic, no fissils, buff to medium tan. Limestone, argillaceous to arenaceous, infrequent black shale beds, medium to light brown.	34/1	CONCI	HUNBLY	INTER			2"	SCH			PE	
- 81 - 84 - 87 - 87						(Np 199				CE					

BI		NO I	1283 1W3L	EASTING	И. Brewst enport, I	040				EL	RING D/ INTRACT( EVATIO	]R⊧ L	ov. 2 afari	20, 1 ge/GS	996 I		_	
	a auge II IIASH R Rock C Crre	ir sample	אד 0 אד ק צוצ עד	ELBY TUBE IN HALL OPEN IN HALL PISTON ATIC HATER LEVEL NATIC HATER LEVEL				DI FA	sture Ir 00			• f	ENETR	IN OMETER 2	kg/ci		TIC	)N
HLGO -90	81180L	5011_/ROCK	DESCRIPTIO	N			CONDITION	NUMBER	INTER LEVEL	CONSTR	DHETER NUCTION AILS	Δ	2 2 2	dhs/o. D Hater t	3n 30	, 4 пх іі	0, quid	ii
93			LIMESTONE: as above, lin buff, iron oxide (possib coatings.	iht tan ta y sidersite)														
96		<u>95 Q</u>	LIMESTONE (KENWOOD MEMBE argillaceous to arenaceou same fossils, light to da	ıs, dolomitic.					-				- 6"	BORE	HELE		-	
99					- - - -													
102		_104 0.											-2"	SCH 4		- pr		
105			LIMESTONE (OTIS FORMATION orgillaceous, trace fossi grey. At 105 Ft. groundw estimated flow 5 to 10 gp	ls, dark ater				1	<b>▼</b> 05,0									
108													BEN	TOMET ENT G	E -	POR	LAND	
111																		_
14																		
117																		-

	I	Komi	EX IN	TERNATIONAL LTD.	OFFICE REP	ORT	ON	S	ITI	E INVE	ST	[GAT	ION	1		SHEET	. 5	OF 6
	B	ORING		HW3L LOCI	PILED BY: M. Bres ATION Dovenport, TING:	uster				BORI CONT	NG D	ate n Dr l	lov.	20,	199	_		
		li uash R Rock C Crre	r sample Sample Core L Barrel	t shelby ti O thon kali P thon kali V statie k	L OPEN L PISTON WATER LEVEL		SAMPLI ×××	DI F/	NDITI ISTURI AIR IOD						INF (		ATI	0N
		S SPLI	t spoon	T DINAME	WATER LEVEL				JST				ļ_	2	, 1	Э	, 4	Ļ,
	-			DESCRIPTION					Ę	PIEZONE		10 Δ		rone/ So	10.3n . 30	)	40	50
	HLLGO	SmB0.		DESCUTLITON			CONDETTON	NUMBER	NATER LEVEL	DETAIL		y plati			r con	TENT 1	<u>.</u>	
	-120	╘╌┥	SOIL/ROC			11PE	CON CON	HUH	UNT			10		30	50	)	liquic 70	1111111 90
				LIMESTONE (OTIS FORMATION): as above.									+6'	BO	EHO	.E		
	-123															_		76
													2"	SCI	1 40	PVC	PIPE	
	-126												<u> </u> 			+		
	-129												-		$\downarrow$	_		
)												Í	DE	UTO				
											才		CE	MEN	GFO	- PUI UT	RLAN	
	-132		133-0									_			_			
				DOLOMITE (SILURIAN) argillad	eous,													
	-135			trace arenaceous, chinodern ar corral fassils, thin black sho	id iles, i							<u>135 0</u>						
		<u>NN</u>		soft, fissile								<u>_L3D_U</u>			+	+	╞╼╎	+
													- PE	.TO	ITE	PELLE	s	
	-138											Í						
											0 0 0 0							+
											0 0 0	_	SA			NO 3 Sand		
	- 141										0 2					שמאמ		
											0 6	141 5				1		
											0 4)							
	-144										0							
											0							
		<u> </u>									о с		N0 SCR	O   C IEEI	)10*	SLOT		
1	147	<u>H</u>									0 0							
	121.121	<u>1</u> <u>1</u> <u>1</u>																
		HH									0							
l	-150-6	<u> </u>																

(

				TERNATIONAL LTD OFFICE	REPOF	RT -	ON	1 8		E INVEST	TGA	TT	חח		SH		Б		5
	BI NI	ORINE DRTH1	ING	4283 COMPILED BY: M. MW3L LOCATION Daveny EASTING	Brewst	er				BORTNG	Date: Tor:	No	v. 21	0. 1	996		. P	<u> </u>	
		a auge II IIasi R Rock C Crre	TYPES ER Sample H Sample K Core El Barrel IT Spoon	T SHELBY TUBE B THEN WALL OPEN P THEN WALL PISTON V STATEC WATER LEVEL TOTWATEC WATER LEVEL		1		0) F/	NDITI ISTURI NIR NIR DOD			_		TETER	IFOF	<b>n</b> 2		ис 	
	HL 20	Sm <b>BOL</b>	SUIL/ROOK	DESCRIPTION	TYDE	-	PLES	NUMBER	UNTER LEVEL	PIEZONETER Construction Details	) <u>1</u> - X - X	) tic	NA Tiùil	TER I	3n	π x .	10 , 10 , iquid	50	Ţ
i	100	ТИНИИ		DOLOMITE (SILURIAN) as above.				ž	3		-15		30 - Sane - No. - Scree	_	50 CX 10° 9		1 1	90	
	-153			TOTAL DEPTH = 152.0 Ft.									-		<b>=</b>				=
	- 156																		
	159																		
-	162			NOTES Estimated gu flaw @ 2 gpm Lags based on cuttings from downhole air percussion hanmer. Cuttings									-	-		-			-
	165			were predominantly dust with rock chips to 1/4".													+		_
	168																_		
	171																		
- 1	74											-							
																	+		
	77						2			-					_	_			-
L	30 L																		

(WL-07) Page 1 of 1

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PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

## HOLE DESIGNATION: MW4-95 DATE COMPLETED: FEBRUARY 25, 1995 DRILLING METHOD: NX CORE CRA SUPERVISOR: C. AHRENS

fl. BGS	DESCRIPTION OF STRATA	ELEV.		MONIT( INSTALLA		Y AL	- E	R RY X		œ
	GROUND SURFACE REFERENCE POINT (Top of Riser)	489.43 491.83	====	 	•	BEDROCK	RUN NUMBER	CORE RECOVERY	Rac	MATER
	LIMESTONE (WAPSIPINICON GROUP), extremely fine grained, massive, fractured, light beige, spring grove		1212		BENTONIT	2			3	
-2.5	member		N.X.X.		5" Ø BOREHOLE 3" STEEL			80	4	
5.0	2 A				CASING SET © 3tt BGS				E.	
7.5	-						2	90	ः -	
	0									35
10.0	9	·					3	53	-	
2.5					2.		4	96	-	
5.0	– very fine grained, massive, rare stylolites, light brown to light gray				4" Ø BOREHOLE					
15.0	- extremely fine grained, contorted to								34	
17.5	wavy bedding planes I" thick, very light brown to light gray						5	100	-	
20.0	<ul> <li>very line grained, breccia, light gray</li> <li>extremely fine to very fine grained</li> <li>beds, 2" thick, very light brown to very</li> <li>light gray</li> </ul>								i,	
22.5	<ul> <li>dolomitic, very fine to microfine, wavy to contorted beds 3" thick, argillaceous to slightly argillaceous, occasional bed of green-gray argillite, very light gray to gray, kenwood member</li> </ul>					_			·	С. 20
25.0								29		- 10
27.5							6	98	-	
30.0	- 3" chert nodule (@ 30.31t BGS)	450.00		1.0	3					
2.5 -	to 0.75" laminations, 0.25" calcite nodules, gray to dark brown, kenwood	458.93								,
ł.	LIMESTONE (OTIS FORMATION), massive, microfine, very light brown END OF HOLE @ 32.511 BGS	490.83	_	,						

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

HOLE DESIGNATION: MW4L-95 DATE COMPLETED: MAY 5, 1995 DRILLING METHOD: 6" AND 3" WET ROTARY CRA SUPERVISOR: C. AHRENS

DEPTH fl. BGS	DESCRIPTION OF STRATA	ELEV. fl. AMSL	HONITOR INSTALLATION	BEDROCK INTERVAL	RUN NUMBER	RE ERY <b>X</b>		E
	GROUND SURFACE REFERENCE POINT (Top of Riser)	489.48 491.49	· ·		NUR	RECOVERY	ROD	MATER
	LIMESTONE (WAPSIPINICON GROUP), spring grove member					2	20	-
-2.5	f a f ja				Ì	5	.8 5	
87.		5						2) 23
-5.0			х х с с с с с с с				83	
		1	BOREHOLE					
7.5								
10.0		× .						
10.0								
12.5			6" Ø BOREHOLE 3" STEEL CASING SET Ø i211 BGS			2	<u></u>	÷
			CASING SET 2 1211 865	.0	1		- 20	
5.0				°				
							$\sim$	
7.5								
20.0								
22.5	DOLOSTONE (WAPSIPINICON GROUP), kenwood member	468.46	BOREHOLE					
22.0						<b>1</b> 2		
25.0								
27.5	2		BENTONITE					200 Million
	R							13
30.0							1 20. j	
	LIMESTONE (OTIS FORMATION)	458.46		8				-
32.5	· .			~		65	8	
							ŝ	-
NO	IES: MEASURING POINT ELEVATIONS MAY CHA WATER FOUND V STATIC HATER LEV	NGE: REFER	TO CURRENT ELEVATION	TABLE	13			

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(HL-09) Page I of 3

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

### HOLE DESIGNATION: MW4L-95 DATE COMPLETED: MAY 5, 1995 DRILLING METHOD: 6" AND 3" WET ROTARY ' CRA SUPERVISOR: C. AHRENS

(WL-Og) Page 2 of 3

Depth IL Bgs	DESCRIPTION OF STRATA	ELEV. II. ANSL	MONITOR INSTALLATION XX BE COOKER WILL NUMBER NOMBE
37.5	G.		
10.0			BENTONITE GROUT
12.5			
5.0			
.5		- 25	3" Ø BOREHOLE
0.0	12	· e	
2.5			
5.0 -	LIMESTONE (BLANDING FORMATION)	434.46	
7.5			SAND PACK
0.0	¥		
2.5	·		SCREEN
5.0 -	END OF HOLE @ 65.011 BGS	424.46	
2			
NO	IES: MEASURING POINT ELEVATIONS MAY CHAN WATER FOUND V STATIC WATER LEVE	GE: REFER	TO CURRENT ELEVATION TABLE

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

### HOLE DESIGNATION: MW4L-95 DATE COMPLETED: MAY 5, 1995 DRILLING METHOD: 6" AND 3" WET ROTARY CRA SUPERVISOR: C. AHRENS

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(HL-09) Page 3 of 3

DEPTH fl. 8GS	DESCRIPTION OF STRATA	ELEV. ft. AMSL	HONITOR INSTALLATION	RVAL	N BER		<b>x</b> *	er av x
			•	BEDROCK	RUN NUMBER	RECOVERY	ROD	HATER RETURN X
-72.5			SCREEN DETAILS Screened Interval: * 55 to 651t BGS Length: 101t Diameter: 2* Slot Size: #10 Haterial: PVC Sand Pack:					
-75.0			53 to 651t BGS Material: Sand		3			
-77.5	.a.							
-80.0	6	5	ŝ				3 (4	$\phi_{r_2}$ .
-82.5		2	-10 <i>4</i>				:	
-85.0			а в <sup>6</sup>					2
-87.5						•		
90.0	19							
92.5								
95.0								ંગ
97.5	са 00							2
-100.0							F .	
102.5	· · · * *						212 	

PROJECT NAME: LAFARGE PROJECT NUMBER: 6031 CLIENT: LAFARGE CORPORATION LOCATION: DAVENPORT, IOWA

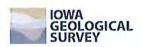
HOLE DESIGNATION: MW5-95 DATE COMPLETED: FEBRUARY 24, 1995 DRILLING METHOD: NX CORE CRA SUPERVISOR: C. AHRENS

(HL-08) Page 1 of 1

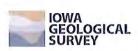
DEPTH ft. BGS	DESCRIPTION OF STRATA	ELEV. ft. AHSL		HONITOR INSTALLATION	X I	- <b>E</b>	R X X		×
	GROUND SURFACE REFERENCE POINT (Top of Riser)	485.28 488.03	=		BEDROCK INTERVAL	RUN NUMBER	CORE RECOVERY	RoD	WATER Return X
-2.5		482.60		BENTONITI GROUT 5" Ø BOREHOLE				9. R.	
-5.0	LIMESTONE (WAPSIPINICON GROUP), very fine grained, fractured, abundant stylolites, becoming dolomitized with depth, very light brown, spring grove member		E.	SET @ 311 BGS					
-7.5	<ul> <li>fine grained, massive, minor fractures filled with calcite, very light brown to very light gray</li> </ul>						100	-	
10.0	<ul> <li>very fine grained, wavy beds up to</li> <li>0.5" lhick</li> <li>extremely fine grained, brecciated,</li> <li>part argiilite filled, very light brown</li> </ul>								
2.5	- dolomitic, microcrystalline to fine grained, wavy to swirled beds 4" thick, light brownish gray, kenwood member			4" 0			na a ¶ana		
-15.0	- dolomitic, very fine to microcrystalline, wavy to swirled beds 2" Thick, slightly argilaceous to argillaceous, becomes	8	3	BOREHOLE		2	100	-	
-17.5	more dolomilic with depth, light gray to brownish gray - 1" chert nodule (@ 18.33/1 BGS)			<b>a</b>					
-20.0		S.				3	100		
-22.5	- 3" chert nodule (@ 22.66/1 BGS) LIMESTONE (OTIS FORMATION), massive,	462.34							
-25.0	microcrystalline, mottled very light brown and light gray								
-27.5						4	100	-	
	END OF HOLE @ 28.311 BGS	457.01	L	80	2				
-30.0							,	8	
2.5	ч • • •								
	DIES: MEASURING POINT ELEVATIONS MAY CHAN			2.32			~		
ĊŰ	DIES: MEASURING POINT ELEVATIONS MAY CHAN WATER FOUND ¥ STATIC WATER LEVE	GE: REFER	TO CU	RRENT ELEVATION TA	BLE	<u></u>		<u> </u>	
Ť					_		. <u> </u>		



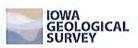
BOR	TRACT NO INS NO. THING:	4161 COMPILED BY: S. Ross MN7 LOCATION Davenpart, EASTING:	Ісыа				CON	ING DA Itracto Vation	2 6	eote	chni	col S	ervi	ces I I Igr	Inc.
AHRC	LE TYPES AUBER SAMPLE WASH SAMPLE ROOK COAL CRREL BARREL SPLIT SPOON	T SALER TUBE O TREN HALL OPEN P DEEN HALL PISTON IZ STATIC HATER LEVEL I OTHATER LEVEL		SAMPL SAMPL		STURS IR 00						in kg/			N
1111	234	DESCRIPTION	si Si	CONDITION 4	NUMBER	TRAD HOLD	PIEZO ODVSTRU DETA		Δ 10 x		1045/1 20			10	50 90
0	1.0	TOPSOIL: block organic rich silt, obundant rootlets, danp							1					PR	
		OLAY AND SELT: reddish brown, soft, low plasticity, trace sand, damp.		-											
0									-	-6	-1/2	DTA	. 301	RCHOL	ε.
20	13.0	Het.													
.0		SANJSIONE: grey, soft, nedium to coarse grained, thin black shale beds, fossil fragments, damp (Pennsylvanian)							14.0		. 01	. 80	re hou		
3.0	1 0000 to 2000 to 2									R	DI ISER	. FV PIFE	C, SI	C8 40	
				-						BG	DTIN TUCR	ate	- 21	HENT	
70															
0.0	9         Size Jaj           80         Size Jaj														



CONTRACT BORING N NORTHING	0.: MN7 LC	MPILED BY: S. Ros ICATION: Daverport ISTING:	, Іоно	Ø			BORTHG CONTRAC ELEVATI	IR	Geo	. 14-16 atechnic ar. 596	ol Ser	vices	Inc. pr)
SHIPLE THP A AUGER : U UASH S R ROOX O	SATPLE O THEN I	TUBE IALL OFEN IALL PESTON C NATOR LEVEL	s	AFL				-		ST IN		1.1.1.	ON
C CRAEL 5 SPL17	O WEL	IC WHER LEVEL	54	FLE	LO	ST	PIEZOPETES	+	A GP	2 BLOLE/0	3 3h		1
KITH R	DESCRIPTION		TIPE	CONDITION	KUMBCR	INTER LEVEL	CONSTRUCTION DETAILS		10	20	20 READE OD	40 1G 700	<u>50</u>
-39.	SAWJSTON€: os above												
	<u>40 0.</u> LIMESTONE: light grey to soft to medium hordness, a thin black shale beds, fos IDevonian - Ropid & Solon	rgilloceous, sil freamente.								4" 01/	. EORE		
										-2"  DI, RISER	n. ryc, pife	SCH	40
										BENTO	ALTE -	22HEN	



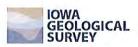
ONTRACT NO.: 4161 Oring Ho.: May Orthing:			· .			BORING DA CONTRACTO ELEVATION	R: Ge	: 14-18 otechnic pr. 596	cal Serv		
AMPLE TYPES A AUGEA SAMPLE	T SHELBY TURE 0 THEN WALL OPEN		SAPL		STURE	- A ( )	TE	ST IN	NFORM	ATIC	N
N WASH SAMPLE R ROCK CORE	P THEN HALL PISTON		IJ	FA			0 PE	KETFICHETC	R kg/ca2		
C CRAEL BARREL S SPLIT SPOON	STATIC WATER LEVEL		. "	10			100	, 2		4	
11			ANFLES	5	H	PIEZOHETER	V S	T BLOLE/O	),3n		
STIBOL	DESCRIPTION		CONDITION	5	TRACTI KELAN	CONSTRUCTION DETAILS	10 X	20 0.Y.M	30 . READING	44	50 X
SUIL/ROOK		TYPE	8	NUMBER	TUN		100	300	500	200	900
	LIMESTONE as above.										
田											
9.0年											
FI ·											
두											
2日											
田							IT				
臣			14								
5.00											
臣	,				1		-			1	
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1.0 = = =											
				1							
田	- •						H			-	
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臣			1					+		-	
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							4			-	
28日				1							
E											
6. 臣										_	
		1									
日											
,,臣					}						



NORTHING	4161 147	CCHPILED BY: S. R LCCATJON: Davenpa EASTING:	rt, Іска				CONT	NG DA RACTO ATION	TE: De R: Ge : ap	atect	mical	Serv	ices I ist (gr	inc.
SAMPLE TIPES A MUSER SAMPLE N MASH SAMPLE R HODX CORE C CRREL ENRREL S SPLIT SPOON	0 91 22	HELBT TLEE HDN WALL DEEN NEN WALL PESTON BTATEC MATER LEVEL DINNIC WATER LEVEL		SAMPLE	DI FA 60 L0	STURS UR DO			• 0 A	OKETRO	RETER K	9/ca2	IATIC	N
	DESCRIPTIO	ΩN	TTPE .	FLES	NUMBOR	TENCI NOLUT	PIEZONE CONSTRUC DETAIL	TION	χ 100 70	. a	Y.A. F	n or	10 700	5
	LINESIONE: es above LINESIONE: light tan, no fossil fragments (0 nember)	hord, orgillocœus, evonion - Doverport				∑ \$¥12.				2" RI		RVC.		



808	RING N RINE N		1161 1W7			LED BY: 9 ION: Doven NG:		на			α	ORING DA INTRACTO LEVATION	R: G	cotec	hni	6, 199 cal Se 5.8 ft.	vices	Inc. (gr)	
AURC	AUGER S MAGER S MASI SA ROCK CC CREL ( SPLIT S	SAAPLE AMPLE ORE BARREL			T SHELBY THE O THEN WALL P THEN WALL STATIC HA TOTANGLE W	open Piston Ier Leyel		SW	×,	CONDIT DISTUR FAIR 6000 LOST			TI	EST	I	NFOR	MATI		
DEPTH R.	STABOL	XIIL/ROX	D	ESCRIPT	ION			SANFA		IMTER LEVEL	PIE CONST DE	ZONET (R Ruction IAILS	ο 10 x		D D		40 NG 700	<u>. 50</u> 90	
132		137.0	LIMESTONE	as above.										2" RI	DI) SER	RVC, PIFE TTE-CE	SCH ·		
138 [4].1 [44,			LIMESTONE:	dolonitic.	ry hard, , few fos: n Kenwood	sil fragmen	5, t5					50505	145.		OI	N EORI	HOLE		
-156 -159		150.0	very hard, frognents,	argillace	оця, Ген Г орргох. С	1.1 gal/nin					0×0×00×0×0×0×0×0×0×0×0×0×0×0×0×0×0×0×0			BE	ift	ИТИ БІ			
-162											0.00.00	50 d0 00	162.	O BI	ENTO Lift	NITE G	RDUT		



80	NTRACT NO.: 4161 Ring Ko.: Mw7 Rthing:	DDHPILED BY: S. Ross LOCATICN: Davenport, EASTING:				•	BORING DA CONTRACTO ELEVATION	R: Ge	otechn	16, 199 ical Se 96.8 ft	essive	Inc. gr)
8	FLE TOPES AVIER SMALE WASH SAVPLE ROCK CORE CRIEL BAREL SPLIT SPCCM	T SHELDT TUDE O THEM WALL OPEN P THEM WALL PESTON SZ STATEG MATER LEVEL SK DINAME MATER LEVEL		SAVEL	] DIS	STURB IR ID			ENETADIE	ENFOF		ON
COTH AL.	Strifta.	DESCRIPTION	11K	CONDELEON	NUTEER	WIER LEVEL	PIEZONETER CONSTRUCTION CETAILS	Δ s 10 x	PT BLOUS 20	2, , /0.3n . 30 .A. READ	40 146	<u>با</u>
-180		grey to light brown, thin beds, very hord, argAlaceous, dalonitic, black thin shale layers, no fosså fragments, producing vater approx. 5 gal/nin (Silurian)						100	R[3Ef - 1/4* 5 - 10/2 0 - 4" D - 2" D 0.01	500 IA. FVC PIFE DIA P DIA P IA FVC	E_TOUT SAND	16
-186 -189 -196	0	IAL DEPTH = 183.0 FJ.										
-195	δD							$\left  \right $				+

CO BO NO	NTRAC RING I RTHIN(	VG: EASTING	M. Brewster				8	ORING DA	TE	Nov	20 19	996	1	ur
A µ R	NASH S ROCK C	R SAMPLE 0 THEN WALL OPEN SAMPLE 0 THEN WALL OPEN				DNDIT) ISTUR AIR 000							1ATI	101
S		I SPOON I DINNICC WATER LEVEL				051				1	2	. 3		4
DEPTH (Ft)	SMB0.	DESCRIPTION	-	CONDITION	Τ	INTER LEVE	CONST	ZOMETER Ruction Tails	ťò	SPT BL	DHS/0.3	30 10NTENT	40 X	<u> </u>
0		SILTY CLAY: trace roots, cool,	11.62	COND	NUMBER	RATE			plest 10	c'   ini 	t ) 	€ 50 + +	liqui 70	d 11
		iron oxide staining.								STI	Х-ЦР	= 0.38	f	
3		4.0											•	
6		FILL: CKD silty texture, little gravel, accasional boulder, laose, dry, light grey-brown.												
											_		_	
									_					
	20-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-				-	-			-	-6"	BOREHI			
	20-0-													
										- 2" !	SCH 4(	PVC	ΡΙΡξ	
222														
16									+-					
	1010								_	L BENT Ceme	ONITE NT GR	- P0 OUT	RTLAN	ן מ ן
- V	N													
<u>vokor</u>												_		
NONON	>=			ŀ										

CC   BC	Intra	ict no.⊜ 42 Eno.÷ mi	283 48	IONAL LTC	com Loc/	PILED BY	CE REP M. Brei Javenport,	Ister					NVESTI BORING D CONTRACTI ELEVATIO	ate: OR:	: No	v	20,	1996	EET	. 2	OF
	i uash R Rock C Crre	r Sample			T SHELBY TH O THEN WALL P THEN WALL V STATIC W DINAMIC	l open L piston Witer level			SAMPL	D) Fi	NDITI ISTUR NIR NOD IST	ION .				NE TR	II Omete	R kg/	ce2	۹TI	:ON 
HLLGO - 30 -	Sm80.	SUIL/ROCK		DESCRIP	TION			TYPE	CONDITION	NUMBER	UNTER LEVEL	008	EZOMETER STRUCTION ETAILS	X.		T BL 2	ous/o D Hater 1	3n 30	ENTX	40 Liquii 70	a' i i
- 33			FILL	as above.										34		6" 2" BE	BOR SCH	HOLI 40 I	e PVC H - POI		
36	000000																				
39	000000						i							39				+			
42	0000000														_	NO		_		I SA	
45	000															NUE		10-	5_01	SCR	EEN
48	0000000										9 9 1 1			48							
51			TOTAL D	EPTH = 49.0 F	t.											_					
54			returns ILafarg encount investi	ft drilling, р with air-roto e quorry rig) ered within th gation — Expec approx 50 ft	iry hainmer No grau he depth al ited base i	ndwater F															
50																					

		_		TERNATIONAL LTD. OFFICE F	REPORT	ON	SI	ITE	INVESTI	GATIO	N	SHEE	T .1	OF 1
	B	ORING		4283 COMPILED BY M. MM9 LOCATION Davenp EASTING	Brenster		_	_	BORING DA CONTRACTO ELEVATION	TE Nov R: Geo	20, 1 technic	.996	VICes	20.0
		h hash r rock c crre	types Er Sample I Sample Core 2. Darret, T Spoon	T SHELBY TUBE O THON WALL OPEN P THON WALL PISTON V STATIC WATER LEVEL V DYNAMOL WATER LEVEL		SAMPLI		D			TROMETER	IFORM kg/ca2		N
	DEPTH (FL)	SMBQ.		DESCRIPTION		AMPLES	- 		PIEZOMETER INSTRUCTION DETAILS	1 	elohs/0 20 Hater (	30 CONTENT		
	- 3		<u>2011_/ROC</u>	SAND TOPSDIL: trace clay, silt, gravel, slightly moist, roots, crange-brown.	1172	CON					30 STICK-UI	⊕ 50 P = 2.02 BOREHDI	1 1	90 90
			50_	SILTY CLAY: medium stiff, moist, low plasticity, grey-brown.										
	- 6		6.5	SILT: little clay, trace sand, coal, very stiff, dry, medium brown: CEMENT KILN DUST (CKD): silty, very	_							+	+	
)	- 12		13.0	stiff, dry, light grey to ton, crumbles easily. Some moisture								TE PVC		
	- 15										MENT G			
	- 21													
2	- 24 - 27		25 D	CKD very hard, dry										
	30													

$\bigcirc$	CC 80	INTRA	NCT NO.: 4 5 NO.: M	ERNATIONAL LTD 283 W9	COMPILED BY	CE REP M. Brew lavenport,	ster				BORING DA	ATE Nov IR Geot	20,	1996		S DF 4
$\bigcirc$	SA I I I	HPLE A AUGE A HASE R ROCE C CRRE	TYPES ER Sample 4 Sample 4 Core 2. Garrel 1. Garrel 17 Spoon		EASTING: T SHELBT TUBE O THEN HALL OPEN P THEN HALL PISTON Z STATIC HATER LEVEL E OTHATIC HATER LEVEL			SAMPL	E CONOI DISTI FAIR 6000 LOST		ELEVATIO	TES PENE	TROHETE	iR kg/ci		ION
	HL-30	Smeor	SOIL/ROCK	DESCRIPT				MPLES	NUMBER LATER 1 EVEN	P COP	PIEZONETER NSTRUCTION DETAILS	∆ SPT ⊥D X plostic li	20		<u>, 10</u>	50 50 110 11011
	- 33			CEMENT KILN DUST (CKI stiff, dry, light gre crumbles easily.	l) silty, very y to tan,				-				3-1/4'	BURE	IDLE	
	- 36	-														
$\bigcirc$	- 39															
	-42		43_0	Hard, cement-like lay	er .							B	Εντοια	TE -	PORTL <i>I</i>	IND
	- 45		45_0	Solid, nodularized CK tan, almost white.	D, light								EMENT	68001		
	-48					1			4 1 1 1							
	- 51								1							
	- 54															
	-57															
	60															

CO BO NO	ntra RIN5 RTHI	ct no No Ng		Н. Вген	ster				BORING D CONTRACT ELEVATIO	ate: Or:	Nov	20.	1996		
A H R C	i Hash Rock Crrei	IYPES R SAMPLE SAMPLE CORE L BARREL T SPOON	T SHELBY TUBE O THEN HALL OPEN P THEN HALL PISTON V STATIC HATER LEVEL V DYNATIC HATER LEVEL			SAMPL XX	01 F/	NDITI ISTUR VIR VIR VID DOD DST		•	TES PENE	ROMET	ER kg/	íce2	ATION
HLG0 69-	SmBQ.	SOIL/ROCI			11PE 12	CONDITION	NUMBER	INTER LEVEL	PIEZONETER CONSTRUCTION DETAILS	, j	SPT (	20		ENT X	10 iquid li 70
- 63			CEMENT KILN DUST (CKD) as above.								8	-1/4	BCR	EHDL	
66		70										SCI		PVC F	
72		10	Аз above, CKD varies From tan to near white, loose, dry	, , ,								NTO: Men	ITE - Grou	- POR JT	TLAND
75						-									
78						8						3.4			
81										81 5		'f" P	ELTON	ITE	
94										83 9 85 4		3	TUSCA	TINE	SAND
97												0	020*	S_OT	SCREEN

(

			EX IN	TERNATIONAL LTD	OFFICE REF	PORT	- ON	I SI	ITE	E INVEST	IGA	TTC			SHEET	4	05	4
)	BI	ORTHE		MW9 LOC	1PILED BY: M. Bre CATION: Dovenport, STING:	wster				BORING I CONTRAC ELEVATIO	DATE : TOR :	Nov	20	1996	;			
		a auge N Nasi R Roch C Crre	TYPES ER Sample H Sample K Core El Barrel, IT Spoon		LL OPEN		SAMPL XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX		sturs Ir 10				TROME	ENFI		ATI	ON	
	HL 00	SmBOL.	\$011_/R02	DESCRIPTION		11PE	CONDITION		UNTUR LEVEL	PIEZONETER Construction Details		) , tic'i	BLOUS 20 HAT	30 R CON	TENT X	Liquis	dili	
	- 93			CEMENT KILN DUST (CKD) as a	bove.			-	-				KD3	ST BOF MUSE	REHOLI CATION	e sai	0	
	- 96			TOTAL DEPTH = 95.0 Ft.							95	0						=
	- 99																	
	- 102																	_
	105			NOTES Hole drilled to 95 ft. using 6 sten auger. No moisture was encountered within the depth o exploration. Base of CKD pile estimated at 100 ft. depth.	of .													
	111																	-
i-	114													_		_		_
	117									1								
			<u>.</u> .															

	KOM	EX INTERNATIO	NAL LTD OFFICE RE	PORT	0	V 8	SIT	E TNVF	STT	GAT				ECT	1	OF .9.
S N	ORING		COMPILED BY: G. Ki LOCATION Davenpar EASTING:	mler				BORI CONT	NG DA	nte: C Ne: L	)ec. .afar	19, oe/6	1996 ST	.I. (		<u>ur 30</u>
	a aug II liasi R Roci C Crre	TYPES ER GANPLE H SANPLE K CORE EL BARREL ET SPOON	T SHELBY TUBE 0 THEN WALL OPEN P THEN WALL PISTON \[2] STATIC WATER LEVEL		SAMP	0             	DNOIT. ISTUR AIR 000	ION		Т	EST	_	١FO	RMA	_	 DN
DEPTH (Ft)	BMBOL		DESCRIPTION	S	AMPLE	_	120 TRAD	PIEZONE	TEON			2 0,2,2,0 0,2,0		3	<u> </u>	<u> </u>
- 0 -	1 3	SOIL/ROCK		TTPE	CONDITION	NUMBER	WATER L	DETAIL	8					X TH: i	iquid	
- 3		Cement Ki	LN DUST :			-				3.0	-21	U ICK-I	JP =	2.16		00
- 6							18									
9																
- 12							-			•	- 8-1	/4 [				
- 15																_
- 18											- 2" (			C PI		
- 21																
- 24						*										
27												N G	FOUT	PORTL	_n/\U	

-	10X	EX INTERNATI	DNAL LTD OFFICE I	REPOR	T O	N S	SIT	E INVEST	IGATI		SH	FT 2	NF 4
	BORIN	ACT NO. : 4283 16 NO. : MW10 ING : TYPES	COMPILED BY G LOCATION Daven EASTING	Kinler				BURTHOR	iate: De 'Or: Lo	ec. 19	1996 GST		
	A AUG II HAS R ROC C CRR	TIPES ER BANPLE H SAMPLE X CORE EL BARREL IT SPOON	t shelby tube 0 then wall open p then wall piston \$\sigma\$ static water level \$\sigma\$ dtwayic water level		x		ISTUR AIR 000 05T		TE	EST I	INFOF	RMATI	
- 30		SOIL/ROCK	DESCRIPTION	TYPE	CONDITION	KUMBER	NATER LEVEL	PIEZONETER CONSTRUCTION DETAILS	∆ S 10 X plostic	PT BLOHS/ 20 HATE Hait	10.3n 30 R CONTEN (+)	. 10 T X ilqui	<u>50</u> d'ilinit
- 33		CEMENT K	ILN DUST				2		01	30	50		90
- 36			6										
- 39							:						
- 42													
- 45						-	-			8-1/4	BUREHD	LE	
-48													
- 51										2" SCH	40 PVC	PIPE	
- 54													
- 57										ENTONIT Enent (	TE - PO Srout		
. 60				4 4 4									

	RING NO. MWLO RTHING		COMPILED BY: G. LOCATION: Dovens EASTING:	iort, Iow	٥			BORIN Contr Eleva	g di Acti Tion	NE: DR: N:	Lafa 590:	19, rge/( 72 ft	1995 SI .a.s	ाः न	Gr)	
A H R	PLE TYPES AUGER SAMPLE MASH SAMPLE ROCK CORE CRREL BARREL	I	t Shelby Tube 0 Then Hall Open P Then Hall Peston 2 Static Nater Level	Q	×.		andit Distur Air	JON			TES	TI		RMA		NI IN
s	SPLIT SPOON		Z DYNAMIC NATER LEVEL				000 097				1	2	_	2		
HLLGOD	SWBOL	DESCRIPT	ION		CONDITION	Τ	NATER LEVEL	PIEZOPETE CONSTRUCTION DETAILS	DH	0t		1.045/ 20		- <u>-</u>	0_,	5
60 +	SUIL/ROCK			1.PE	CONDI	NUMBER	UNTER			y bicst Of	ic I li	janici jit 30	€ CUNIE ⊕ 50		quid 0	lin 9
	CEMEN	i kiln dust											Ī			
63		¥										1/4	BERE	HDLE		-
56											-2"	904	40 P1			+
9																
s											BE	ntola 1ent	TE - Grout	PORTI	AND	
5	108															-
										75 0						
			35								PE.	.TO/U	te pe	LE S		
									2. 1.							
					-		2			3.0						
							0				NO : NO	3 ML 0 02	ISCATI 20° S	NE SI		

	K	COM	EX IN	TERNATIONAL LTD. OFFICE REP	ORT	OI	N S	SIT	E INVEST	IGA		N		SHEET	4	ÛF	4
	BC NO	IRENE		4283     COMPILED BY: G. Kim       MW10     LOCATION: Davenport,       EASTING:	ler				BORING D Contract Elevatio	ate: Or	Dec. Lafa	19, rae/	199 GST	6	(Gr)		1.00
	4 14 15 15 15 15 15 15 15 15 15 15 15 15 15	AUGE I Hasi I Roci Crre	TYPES ER SAMPLE H SAMPLE CORE EL BARREL ET SPOON	T SHELBT TUBE O THEN WALL OPEN P THEN WALL PESTON 32 STATEC WATER LEVEL ST DTRATEC WATER LEVEL	-	ļ,	- - - - - - - - - - - - - - - - - - -	DNDIT: ISTUR AIR 000 0ST	ION			ТI	INF	ORM	ATI	_	
- I	HLLCOD	SmBQ.	SOIL/ROC	DESCRIPTION	11PE 8	CONDELLON		멾	PIEZONETER CONSTRUCTION DETAILS	∆ 10 X	_	1045/ 20	, <u>3</u> R CON	) TENT 1	40		0
	90		COLLYNCE	CEMENT KILN DUST:	12	3	12	VII		10	N	30 ) 3		CATEN	E SAN	Ð	
-	93											). () 	020	' S.O	TISCR	EEN	
	ŧ			Total Depth = 93.0 r												•	
	96																
       	99			NOTES: Hole drilled and logged by GSI personnel.									+				_
-1	02																_
-1(	05								-	_							
-10	18								•								
- 11	11																
- 11	4								-								
1	7																
L 12																	

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# TÀLE 1 PIEZOMETER INSTALLATION DETAILS, DATUM / GROUNDWATER SURFACE ELEVATIONS AND HYDRAULIC CONDUCTIVITIES

PIEZOMETER	DATUM ELEVATION (top of PVC) (ft)	STICKUP (PVC) (ft)	TOTAL DEPTH OF PIEZOMETER (ft bgs)	DEPTH INTERVAL OF SAND PACK (ft bgs)	DATE (d-m-y)	DEPTH TO WATER (ft btoc)	GROUNDWATER SURFACE ELEVATION (ft asi)	HYDRAULIC CONDUCTIVITY (ft/s)	LITHOLOGY OF COMPLETION ZONE
MWIA	616.95	1.45	143.0	119.0 - 153.9	2-Mar-95 5-May-95 18-Dec-95 24-Nov-96	129.85 126.09 131.40 130.91	487.10 490.86 485.55 486.04	NT	Limestone (Devonian-Spring/Grove and Kenwood Members, and Otis Formation)
MWIB	618.51	3.02	40.0	16.0 - 41.0	2-Mar-95 5-May-95 18-Dec-95 24-Nov-96	40.70 27.72 30.50 30.28	577.81 590.79 588.01 588.23	NT	Limestone (Devonian - Cou Falls and Rapid members)
MW2A	588.22	0.85	64.0	30.0 - 67.0	5-May-95 18-Dec-95 23-Nov-96	29.33 36.96 35.56	561.07 553.44 552.66	NT	Limestone (Devonian - Rapid, Solon, and Davenport members)
MW2B	589.61	2.40	65.0	32.0 - 67.0	5-May-95 18-Dec-95 23-Nov-96	38.20 40.28 41.20	552.21 550.13 548.41	NT	Limestone (Devonian - Rapid, Solon, and Davenport members)
MW2C	592.33	2.62	100,4*	22.8 - 103.5*	23-Nov-96	100.23	492.10		Limestone (Devonian - Rapid, Solon, Davenport and Spring Grove members)
MW3	569.17	2.08	100.0	76.0 - 110.0	2-Mar-95 5-May-95 19-Dec-95 27-Nov-96	86.91 71.10 86.30 86.45	482.26 498.07 482.87 482.72	1.8 x 10 <sup>-6</sup>	Limestone (Devonian Spring Grove and Kenwood members, and Otis Formation)
MW3L	570,16	2.50	152.0	138 - 151.7	27-Nov-96	88.36	481.80	> 3.0 x 10 <sup>-4</sup>	Limestone (Silurian - Blanding Formation)
MW4	491.83	2.40	32.5*	3.0 - 32.5*	2-Mar-95 5-May-95 18-Dec-95 24-Nov-96	10.65 10.10 10.73 10.63	481.18 481.73 481.10 481.20	1.3 x 10 <sup>-4</sup>	Limestone (Devonian Spring Grove and Kenwood members, and Otis Formation)

96-4283

TÀLLE 1 PIEZOMETER INSTALLATION DETAILS, DATUM / GROUNDWATER SURFACE ELEVATIONS AND HYDRAULIC CONDUCTIVITIES

PIEZOMETER	DATUM	STICKUP	TOTAL	DEPTH	DATE	DEPTH	GROUNDWATER	HYDRAULIC	LITHOLOGY
	ELEVATION	(PVC)	DEPTH OF	INTERVAL OF		то	SURFACE	CONDUCTIVITY	OF COMPLETION ZONE
	(top of PVC)		PIEZOMETER	SAND PACK		WATER	ELEVATION		
ļ	(ft)	(ft)	(ft hgs)	(ft bgs)	(d-m-y)	(ft btoc)	(ft asl)	(ft/s)	
MW4L	491.49	2.03	65.0	53.0 - 65.0	5-May-95 18-Dec-95 24-Nov-96	9.67 10.32 10.08	481.82 481.17	> 3,0 x 10 <sup>-4</sup>	Limestone (Silurian - Blanding Formation)
MW5	488.03	2.77	28.3	3.0 - 28.3*	2-Mar-95 5-May-95 18-Dec-95 24-Nov-96	2.98 2.58 3.58 3.53	481.41 485.05 485.45 484.45 484.50	NT	Limestone (Devonian - Spring Grove, Kenwood members and Otis Formation
MW6	565.27	2.62	148.0	133.0 - 148.0	18-Dec-95 23-Nov-96	75.40 76.49	489.87 488.78	>3 x 10 <sup>-4</sup>	Limestone (Silurian - Blanding Formation)
MW7	598.84	3.14	183,0	169.5 - 183.0	19-Dcc-95 23-Nov-96	121.95 120.43	476.89 478.41	>3 x 10 <sup>-4</sup>	Limestone (Silurian - Blanding Formation)
MW8	542.53	0.33	49.0	39.0 - 49.0	23-Nov-96	DRY	-	NT	CKD fill
MW9	595.20	2,02	95.0	83.9 - 95.0	23-Nov-96	DRY	~	NT	CKD fill
MWIO	592.88	2.16	93_0	81.0 -93.0	23-Nov-96	DRY	<u>ی</u>	NT	CKD fill

#### Notes:

1. ftbgs- denotes feet below ground surface

2. ftbtoc- denotes feet below top of 2" PVC collar

3. \* - denotes open borehole completion

4. NT- denotes not tested

196-4283

## **APPENDIX B**

CONTINENTAL CEMENT COMPANY Example Field Forms

#### CONTINENTAL CEMENT GROUNDWATER SAMPLING LOG

Site Name: Continental Cement CKD Monofil

Date: \_\_\_\_\_

Weather Conditions: \_\_\_\_\_

Purging/Sampling Device: Hydrasleeves

Samplers: \_\_\_\_\_

Analytical Parameters: \_\_\_\_\_

Sample Location	Sample Time	Water Level (ft btoc)	Total Depth (ft btoc)	Temperature (Degrees C)	рН	Conductivity (uS/cm)	Sample Appearance	Sample Odor	Comments
MW-1B									
MW-2A									
MW-1A									
MW-3									
MW-4									
MW-5									
MW-11									
MW-12									
MW-13									
MW-14									
MW-15									
MW-16									

Field Observations/Comments:



#### CONTINENTAL CEMENT GROUNDWATER SAMPLING LOG

Site Name: Continental Cement CKD Monofil	Date:
Weather Conditions:	Purging/Sampling Device: <u>Hydrasleeves</u>

Samplers: \_\_\_\_\_

Analytical Parameters: \_\_\_\_\_

Sample Location	Sample Time	Water Level (ft btoc)	Total Depth (ft btoc)	Temperature (Degrees C)	рН	Conductivity (uS/cm)	Sample Appearance	Sample Odor	Comments
MW-18									
MW-3L									
MW-4L									
MW-7									
MW-16L									
MW-19									
Q-Sump									
MW-2CR									

Field Observations/Comments:



#### CONTINENTAL CEMENT MONITORING POINT SAMPLING LOG

Site Name: Continental Cement CKD Monofil

Date:

Weather Conditions: \_\_\_\_\_

Purging/Sampling Device:\_\_\_\_\_

Samplers: \_\_\_\_\_

Analytical Parameters: \_\_\_\_\_

Sample Location	Sample Time	Water Level (ft btoc)	Total Depth (ft btoc)	Temperature (Degrees C)	рН	Conductivity (uS/cm)	Sample Appearance	Sample Odor	Volume purged & Final Water Level	
MW-9										
MW-10										
UL-1										
LL-1										
L-Sump										
UL-2										
LL-2										
UL-3										
LL-3										

Field Observations/Comments:



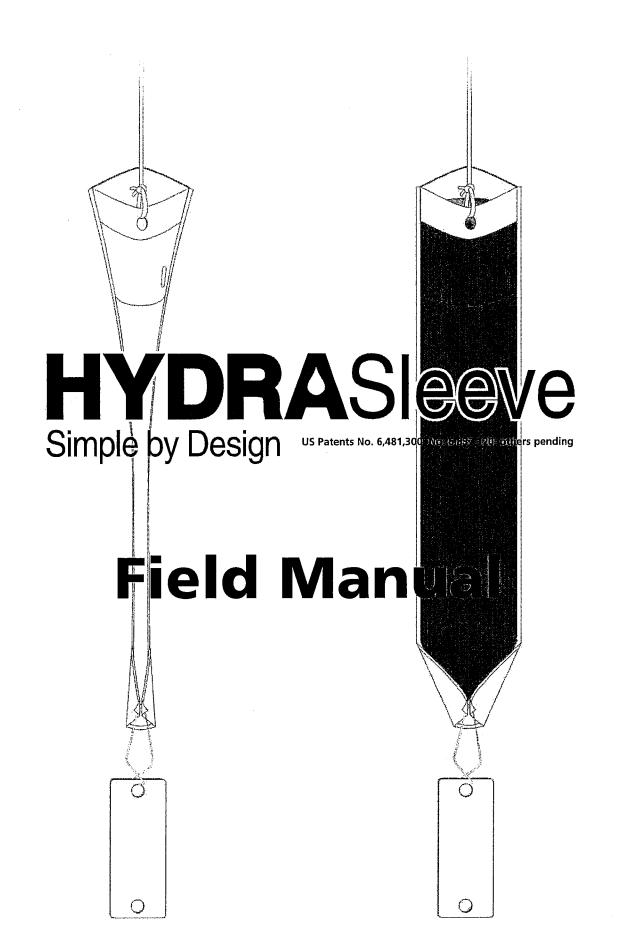
## **APPENDIX C**

CONTINENTAL CEMENT COMPANY Example Chain of Custody

Pace Analytical *		ample via this	-CUSTODY Analytical Request Document chain of custody constitutes acknowledgment and acceptance of the Pace Terms and								LAB USE ONLY- Affix Workorder/Login Label Here or List Pace Workorder Number or MTJL Log-in Number Here									
				ound at: https://info.pacelabs.com/hubfs/pas-standard-terms.pdf stody is a LEGAL DOCUMENT - Complete all relevant fields																
Company:		Chain-oi-C	Billing Information:																	
Address:										ALL BOLD OUTLINED AREAS are for LAB USE ONLY										
												Con	ntainer	<sup>-</sup> Prese	rvative	Туре	**			Lab Project Manager:
Report To:			Email To:							** Pre	servativ	e Types	s: (1) n	itric acio	d, (2) su	lfuric a	cid, (3)	hydro	chloric	acid, (4) sodium hydroxide, (5) zinc acetate,
Сору То:			Site Collection Info/Address:							(6) methanol, (7) sodium bisulfate, (8) sodium thiosulfate, (9) hexane, (A) ascorbic acid, (B) ammonium sulfate,										
										(C) ammonium hydroxide, (D) TSP, (U) Unpreserved, (O) Other							Lab Profile/Line:			
Customer Project Name/Number:			State: County/City: Time Zone Collected: / [ ]PT [ ]MT [ ]CT [ ]ET										Analy	/585					Lab Fione/Line. Lab Sample Receipt Checklist: Custody Seals Present/Intact Y N NA	
Phone:	Site/Facility ID	#:	. ,			e Monitori		1		1										Custody Signatures Present Y N NA
Email:					[] Yes	[ ]No	-													Collector Signature Present Y N NA
Collected By (print):	Purchase Orde	er # :			DW PWS I	D #:			1											Bottles Intact Y N NA Correct Bottles Y N NA
	Quote #:				DW Location Code:														Sufficient Volume Y N NA	
Collected By (signature):	Turnaround Da	ate Require	ed:		Immediately Packed on Ice:     (5)       [] Yes     [] No       Field Eiltered (if applicable):     (5)													Samples Received on Ice Y N NA		
						[ ] No			las											VOA - Headspace Acceptable Y N NA USDA Regulated Soils Y N NA
Sample Disposal:	Rush: (Expedi							or G											Samples in Holding Time Y N NA	
<ul> <li>] Dispose as appropriate</li> <li>[ ] Return</li> </ul>	[] Same D		ext Day		[]Yes []No															Residual Chlorine Present Y N NA Cl Strips:
[ ] Archive:	[]2 Day [								ic (F											Sample pH Acceptable Y N NA
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* Matrix Codes (Insert in Matrix bo	x below): Drinki	ng Water (I	(DW), Ground Water (GW), Wastewater (WW),																	Sulfide Present Y N NA Lead Acetate Strips:
Product (P), Soil/Solid (SL), Oil (O	L), Wipe (WP), Ai	r (AR), Tiss	ue (TS), Bio	assay (B), \	/apor (V), O	ther (OT)			Type:											
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## **APPENDIX D**

CONTINENTAL CEMENT COMPANY HydraSleeve Field Manual

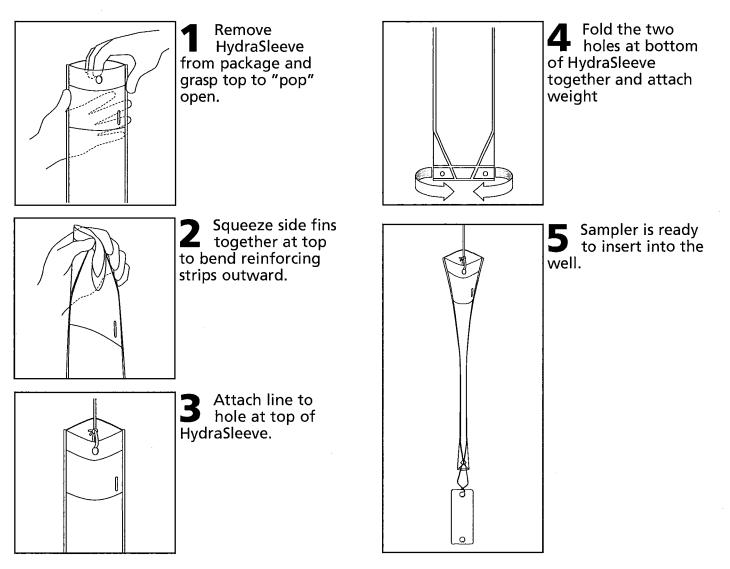


# Introduction

The HydraSleeve groundwater sampler can be used to collect a representative sample for most physical and chemical parameters without purging the well. It collects a whole water sample from a user-defined interval (typically within the well screen), without mixing fluid from other intervals. One or more HydraSleeves are placed within the screened interval of the monitoring well, and a period of time is allocated for the well to re-equilibrate. Hours to months later, the sealed HydraSleeve can be activated for sample collection. When activated, HydraSleeve collects a sample with no drawdown and minimal agitation or displacement of the water column. Once the sampler is full, the one-way reed valve collapses, preventing mixing of extraneous, non-representative fluid during recovery.

# Assembly

Assembling the HydraSleeve is simple, and can be done by one person in the field, taking only a minute or two.



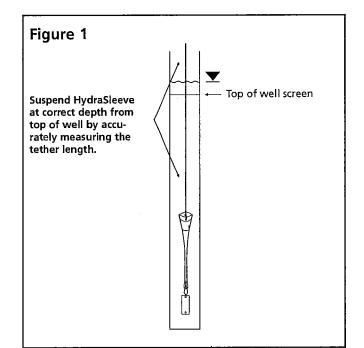
# Placing the HydraSleeve(s)

To collect a representative groundwater sample without purging, the well must be allowed time to re-equilibrate after placement of the sampler. When any device is lowered into a well, some mixing of the water column occurs. The diameter of the device and its shape greatly affect the degree of mixing. The flat cross-section of the empty HydraSleeve minimizes the disturbance to the water column as the sampler is lowered into position, reducing the time needed for the well to return to equilibrium.

There are three basic methods for holding a HydraSleeve in position as the well equilibrates.

**TOP DOWN DEPLOYMENT (Figure 1)** Measure the correct amount of suspension line needed to "hang" the top of the HydraSleeve(s) at the desired sampling depth (in most cases, this will be at the bottom of the sampling zone). The upper end of the tether can be connected to the well cap to suspend the HydraSleeve at the correct depth until activated for sampling.

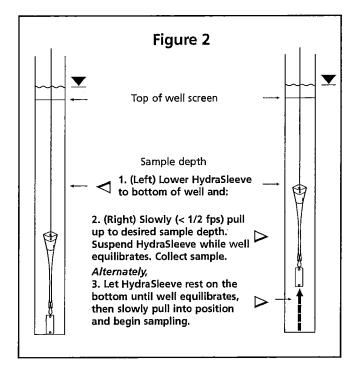
Note: For deep settings, it may be difficult to accurately measure long segments of suspension line in the field. Factory prepared, custom suspension line and attachment points can be provided.



#### **BOTTOM DEPLOYMENT (Figure 2)**

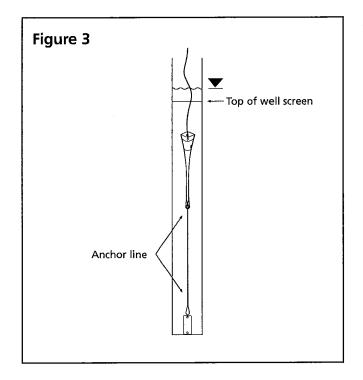
Sound the well to determine the exact depth. Lower the weighted HydraSleeve into the well and let it touch the bottom. <u>Very slowly</u> (less than 1/2 foot per second) raise the sampler to the point where the check valve is at the depth the sample is to be collected. Attach the suspension line to the top of the well to suspend it at this depth. (It is often easier to measure a few feet from the bottom of the well up to the sample point, than it is to measure many feet from the top of the well down.)

Alternately, the sampler can be left on the bottom until the well re-equilibrates. For sampling, it can be very slowly pulled (< 1/2 fps) to sampling depth, then activated (see "Sample Collection," p. 6) to collect the sample, and retrieved to the surface.



#### **BOTTOM ANCHOR (Figure 3)**

Determine the exact depth of the well. Calculate the distance from the bottom of the well to the desired sampling depth. Attach an appropriate length anchor line between the weight and the bottom of the sampler and lower the assembly until the weight rests on the bottom of the well, allowing the top of the sampler to float at the correct sampling depth.

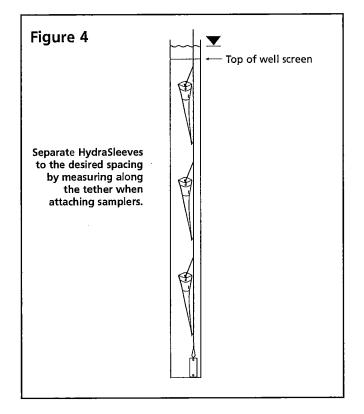


# **Multiple Interval Deployment**

There are two basic methods for placing multiple HydraSleeves in a well to collect samples from different levels simultaneously.

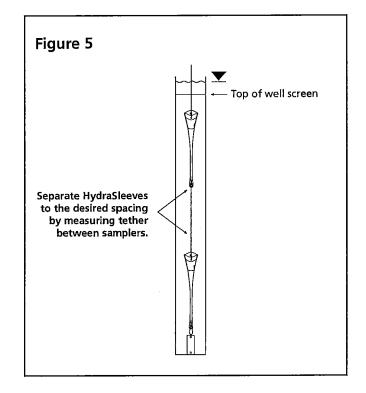
#### ATTACHED TO A SINGLE TETHER (Figure 4)

To use 3 or more samplers simultaneously, we recommend attaching them all to a tether for support to prevent the sampling string from pulling apart. The weight is attached to a single length of suspension line and allowed to rest on the bottom of the well. The top and bottom of each HydraSleeve are attached to the tether at the desired sample intervals. Cable tie or stainless steel clips (supplied) work well for attaching the HydraSleeves to the line. Simply push one end of the clip between strands of the rope at the desired point before attaching the clip to the HydraSleeve.



#### ATTACHED END TO END (Figure 5)

To place 2 or 3 stacked HydraSleeves for vertical profiling, use one of the methods described above to locate the bottom sampler. Attach the bottom of the top sampler to the top of the following HydraSleeve(s) with a carefully measured length of suspension cable. Connect the weight to the bottom sampler. Note: if many HydraSleeves are attached to a tether, more weight may be required than with a single sampler.



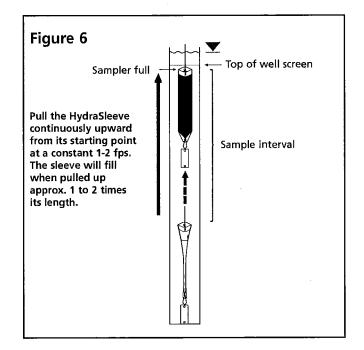
# **Sample Collection**

The HydraSleeve must move upward at a rate of one foot per second or faster (about the speed a bailer is usually pulled upward) for water to pass through the check valve into the sample sleeve. The total upward distance the check valve must travel to fill the sample sleeve is about 1 to 2 times the length of the sampler. For example, a 24-inch HydraSleeve needs a total upward movement of 24 to no more than 48 inches to fill. The upward motion can be accomplished using one long continuous pull, several short strokes, or any combination that moves the check valve the required distance in the open position. A special technique is used for sampling low-yield wells.

#### **CONTINUOUS PULL (Figure 6)**

Pull the HydraSleeve continuously upward from its starting point at a constant 1 to 2 feet per second until full. This method usually provides the least turbid samples and is analogous to coring the water column from the bottom up.

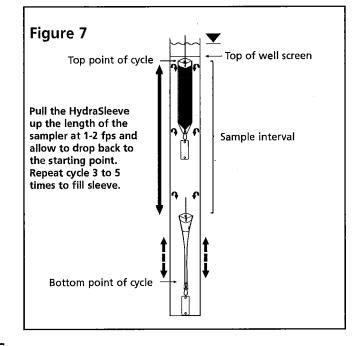
Note: When using this method, the screen interval should be long enough so the sampler fills before exiting the top of the screen.



#### SHORT STROKES (Figure 7)

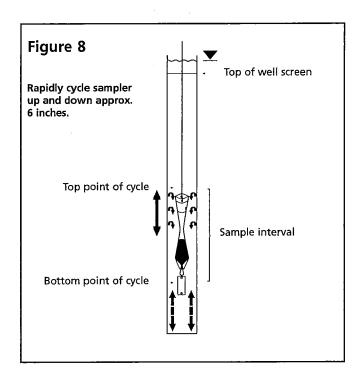
Pull the sampler upward at about 1 to 2 feet per second for the length of the sampler and let it drop back to the starting point. Repeat the cycle 3 to 5 times.

This method provides a shorter sampling interval than the continuous pull method (above), and usually reduces the turbidity levels of the sample below that of numerous rapid, short cycles (below). The sample comes from between the top of the cycle and the bottom of the sampler at its lowest point.



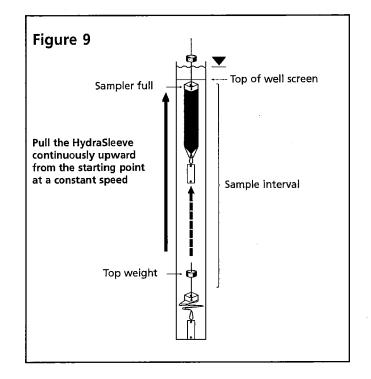
#### **RAPID, SHORT CYCLES (Figure 8)**

Cycle the HydraSleeve up and down using rapid, short strokes (6-inch cycle at a minimum of 1 cycle per second) 5 to 8 times. This method provides the shortest sampling interval. Dye studies have shown that when using this method the sample flows into the check valve from along the length of the sampler and immediately above the check valve. The sample interval is from the bottom the sampler at its lowest point in the cycle to the top of the check valve at the peak of the cycle.



#### SAMPLING LOW-YIELD WELLS (Figure 9)

HydraSleeve provides the <u>best available</u> <u>technology</u> for sampling low yield wells. When pulled upward after the well re-equilibrates, the HydraSleeve will collect a water core from the top of the sampler to about its own length above that point. The sample is collected with no drawdown in the well and minimal sample agitation. An optional top weight can be attached to compress the sampler in the bottom of the well if needed for an extremely short water column. With a top weight, the check valve is pushed down to within a foot of the bottom of the well.



# Sample Discharge

The best way to remove a sample from the HydraSleeve with the least amount of aeration and agitation is with the short plastic discharge tube (included).



First, squeeze the full sampler just below the top to expel water resting above the flexible check valve. (Photo 1, top left)

Then, push the pointed discharge tube through the outer polyethylene sleeve about 3-4 inches below the white reinforcing strips. (Photo 2, middle left)

Discharge the sample into the desired container. (Photo 3, bottom left)

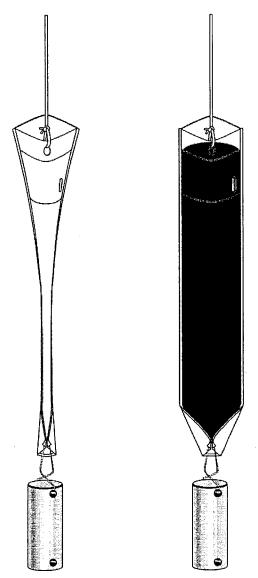
Raising and lowering the bottom of the sampler or pinching the sample sleeve just below the discharge tube will control the flow of the sample. The sample sleeve can also be squeezed, forcing fluid up through the discharge tube, similar to squeezing a tube of toothpaste. With a little practice, and using a flat surface to set the sample containers on, HydraSleeve sampling becomes a one-person operation.



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# HYDRASleeve Simple by Design US Patent No. 6,481,300; No. 6,837,120 others pending

Standard Operating Procedure: Sampling Ground Water with a HydraSleeve



This Guide should be used in addition to field manuals appropriate to sampling device (i.e., HydraSleeve or Super Sleeve).

Find the appropriate field manual on the HydraSleeve website at http://www.hydrasleeve.com.

For more information about the HydraSleeve, or if you have questions, contact: GeoInsight, 2007 Glass Road, Las Cruces, NM 88005, 1-800-996-2225, info@hydrasleeve.com.

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## **Table of Contents**

Introduction1
Applications of the HydraSleeve1
Description of the HydraSleeve
Selecting the HydraSleeve Size to Meet Site-Specific Sampling Objectives
HydraSleeve Deployment
Information Required Before Deploying a HydraSleeve5
HydraSleeve Placement
Procedures for Sampling with the HydraSleeve
Measurement of Field Indicator Parameters11
Alternate Deployment Strategies11
Post-Sampling Activities
References

#### Introduction

The HydraSleeve is classified as a no-purge (passive) grab sampling device, meaning that it is used to collect ground-water samples directly from the screened interval of a well without having to purge the well prior to sample collection. When it is used as described in this Standard Operating Procedure (SOP), the HydraSleeve causes no drawdown in the well (until the sample is withdrawn from the water column) and only minimal disturbance of the water column, because it has a very thin cross section and it displaces very little water (<100 ml) during deployment in the well. The HydraSleeve collects a sample from within the screen only, and it excludes water from any other part of the water column in the well through the use of a self-sealing check valve at the top of the sampler. It is a single-use (disposable) sampler that is not intended for reuse, so there are no decontamination requirements for the sampler itself.

The use of no-purge sampling as a means of collecting representative ground-water samples depends on the natural movement of ground water (under ambient hydraulic head) from the formation adjacent to the well screen through the screen. Robin and Gillham (1987) demonstrated the existence of a dynamic equilibrium between the water in a formation and the water in a well screen installed in that formation, which results in formation-quality water being available in the well screen for sampling at all times. No-purge sampling devices like the HydraSleeve collect this formation-quality water as the sample, under undisturbed (non-pumping) natural flow conditions. Samples collected in this manner generally provide more conservative (i.e., higher concentration) values than samples collected using well-volume purging, and values equivalent to samples collected using low-flow purging and sampling (Parsons, 2005).

#### **Applications of the HydraSleeve**

The HydraSleeve can be used to collect representative samples of ground water for all analytes (volatile organic compounds [VOCs], semi-volatile organic compounds [SVOCs], common metals, trace metals, major cations and anions, dissolved gases, total dissolved solids, radionuclides, pesticides, PCBs, explosive compounds, and all other analytical parameters). Designs are available to collect samples from wells from 1" inside diameter and larger. The HydraSleeve can collect samples from wells of any yield, but it is especially well-suited to collecting samples from low-yield wells, where other sampling methods can't be used reliably because their use results in dewatering of the well screen and alteration of sample chemistry (McAlary and Barker, 1987).

The HydraSleeve can collect samples from wells of any depth, and it can be used for singleevent sampling or long-term ground-water monitoring programs. Because of its thin cross section and flexible construction, it can be used in narrow, constricted or damaged wells where rigid sampling devices may not fit. Using multiple HydraSleeves deployed in series along a single suspension line or tether, it is also possible to conduct in-well vertical profiling in wells in which contaminant concentrations are thought to be stratified.

As with all groundwater sampling devices, HydraSleeves should not be used to collect groundwater samples from wells in which separate (non-aqueous) phase hydrocarbons (i.e., gasoline, diesel fuel or jet fuel) are present because of the possibility of incorporating some of the separate-phase hydrocarbon into the sample.

#### Description of the HydraSleeve

The HydraSleeve (Figure 1) consists of the following basic components:

- A suspension line or tether (A.), attached to the spring clip or directly to the top of the sleeve to deploy the device into and recover the device from the well. Tethers with depth indicators marked in 1-foot intervals are available from the manufacturer.
- A long, flexible, 4-mil thick lay-flat polyethylene sample sleeve (C.) sealed at the bottom (this is the sample chamber), which comes in different sizes, as discussed below with a self-sealing reed-type flexible polyethylene check valve built into the top of the sleeve (B.) to prevent water from entering or exiting the sampler except during sample acquisition.
- A reusable stainless-steel weight with clip (D.), which is attached to the bottom of the sleeve to carry it down the well to its intended depth in the water column. Bottom weights available from the manufacturer are 0.75" OD and are available in three sizes: 5 oz. (2.5" long); 8 oz. (4" long); and 16 oz. (8" long). In lieu of a bottom weight, an optional top weight may be attached to the top of the HydraSleeve to carry it to depth and to compress it at the bottom of the well (not shown in Figure 1);
- A discharge tube that is used to puncture the HydraSleeve after it is recovered from the well so the sample can be decanted into sample bottles (not shown).
- Just above the self-sealing check valve at the top of the sleeve are two holes which provide attachment points for the spring clip and/or suspension line or tether. At the bottom of the sample sleeve are two holes which provide attachment points for the weight clip and weight.

A.\_\_\_\_\_B.\_\_\_\_

Figure 1. HydraSleeve components.

**Note:** The sample sleeve and the discharge tube are designed for one-time use and are disposable. The spring clip, weight and weight clip may be reused after thorough cleaning. Suspension cord is generally disposed after one use although, if it is dedicated to the well, it may be reused at the discretion of the sampling personnel.

#### Selecting the HydraSleeve Size to Meet Site-Specific Sampling Objectives

It is important to understand that each HydraSleeve is able to collect a finite volume of sample because, after the HydraSleeve is deployed, you only get one chance to collect an undisturbed sample. Thus, the volume of sample required to meet your site-specific sampling and analytical requirements will dictate the size of HydraSleeve you need to meet these requirements.

The volume of sample collected by the HydraSleeve varies with the diameter and length of the HydraSleeve. Dimensions and volumes of available HydraSleeve models are detailed in Table 1.

Diameter	Volume	Length	Lay-Flat Width	Filled Dia.		
2-Inch HydraSleeves	625 ml	< 30"	2.5"	1.4"		
Standard 625-ml HydraSleeve Standard 1-Liter HydraSleeve	1 Liter	38"	3"	1.9"		
1-Liter HydraSleeve SS	1 Liter	36"	3"	1.9"		
2-Liter HydraSleeve SS	2 Liters	60"	3"	1.9"		
4-Inch HydraSleeves						
Standard 1.6-Liter HydraSleeve	1.6 Liters	30"	3.8"	2.3"		
Custom 2-Liter HydraSleeve	2 Liters	36"	4"	2.7"		

Table 1. Dimensions and volumes of HydraSleeve models.

HydraSleeves can be custom-fabricated by the manufacturer in varying diameters and lengths to meet specific volume requirements. HydraSleeves can also be deployed in series (i.e., multiple HydraSleeves attached to one tether) to collect additional sample to meet specific volume requirements, as described below.

If you have questions regarding the availability of sufficient volume of sample to satisfy laboratory requirements for analysis, it is recommended that you contact the laboratory to discuss the minimum volumes needed for each suite of analytes. Laboratories often require only 10% to 25% of the volume they specify to complete analysis for specific suites of analytes, so they can often work with much smaller sample volumes that can easily be supplied by a HydraSleeve.

#### HydraSleeve Deployment

#### Information Required Before Deploying a HydraSleeve

Before installing a HydraSleeve in any well, you will need to know the following:

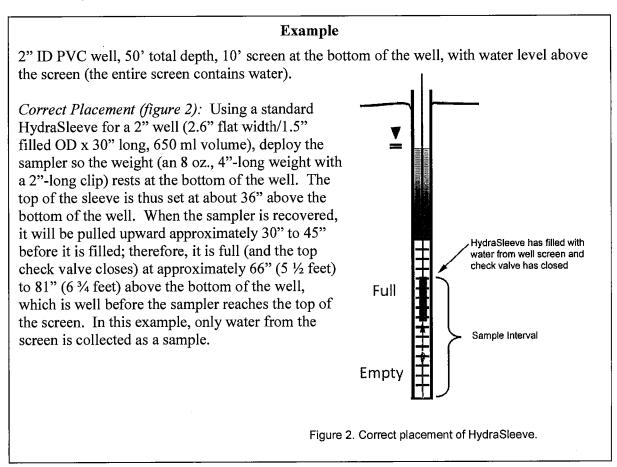
- The inside diameter of the well
- The length of the well screen
- The water level in the well
- The position of the well screen in the well
- The total depth of the well

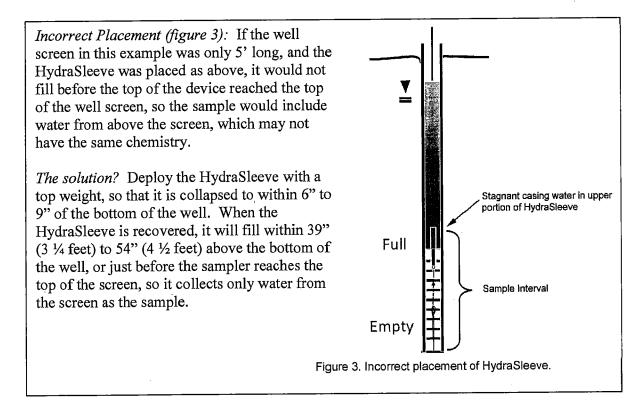
The inside diameter of the well is used to determine the appropriate HydraSleeve diameter for use in the well. The other information is used to determine the proper placement of the HydraSleeve in the well to collect a representative sample from the screen (see HydraSleeve Placement, below), and to determine the appropriate length of tether to attach to the HydraSleeve to deploy it at the appropriate position in the well.

Most of this information (with the exception of the water level) should be available from the well log; if not, it will have to be collected by some other means. The inside diameter of the well can be measured at the top of the well casing, and the total depth of the well can be measured by sounding the bottom of the well with a weighted tape. The position and length of the well screen may have to be determined using a down-hole camera if a well log is not available. The water level in the well can be measured using any commonly available water-level gauge.

#### HydraSleeve Placement

The HydraSleeve is designed to collect a sample directly from the well screen, and it fills by pulling it up through the screen a distance equivalent to 1 to 1.5 times its length. This upward motion causes the top check valve to open, which allows the device to fill. To optimize sample recovery, it is recommended that the HydraSleeve be placed in the well so that the bottom weight rests on the bottom of the well and the top of the HydraSleeve is as close to the bottom of the well screen as possible. This should allow the sampler to fill before the top of the device reaches the top of the screen as it is pulled up through the water column, and ensure that only water from the screen is collected as the sample. In short-screen wells, or wells with a short water column, it may be necessary to use a top-weight on the HydraSleeve to compress it in the bottom of the well so that, when it is recovered, it has room to fill before it reaches the top of the screen.





This example illustrates one of many types of HydraSleeve placements. More complex placements are discussed in a later section.

### Procedures for Sampling with the HydraSleeve

Collecting a ground-water sample with a HydraSleeve is a simple one-person operation.

**Note:** Before deploying the HydraSleeve in the well, collect the depth-to-water measurement that you will use to determine the preferred position of the HydraSleeve in the well. This measurement may also be used with measurements from other wells to create a ground-water contour map. If necessary, also measure the depth to the bottom of the well to verify actual well depth to confirm your decision on placement of the HydraSleeve in the water column.

Measure the correct amount of tether needed to suspend the HydraSleeve in the well so that the weight will rest on the bottom of the well (or at your preferred position in the well). Make sure to account for the need to leave a few feet of tether at the top of the well to allow recovery of the sleeve

Note: Always wear sterile gloves when handling and discharging the HydraSleeve.

#### I. Assembling the HydraSleeve

- 1. Remove the HydraSleeve from its packaging, unfold it, and hold it by its top.
- 2. Crimp the top of the HydraSleeve by folding the hard polyethylene reinforcing strips at the holes.
- 3. Attach the spring clip to the holes to ensure that the top will remain open until the sampler is retrieved.
- 4. Attach the tether to the spring clip by tying a knot in the tether.

		NOT both) of the	
	in the tether.		

- 5. Fold the flaps with the two holes at the bottom of the HydraSleeve together and slide the weight clip through the holes.
- 6. Attach a weight to the bottom of the weight clip to ensure that the HydraSleeve will descend to the bottom of the well.

#### **II. Deploying the HydraSleeve**

1. Using the tether, carefully lower the HydraSleeve to the bottom of the well, or to your preferred depth in the water column

During installation, hydrostatic pressure in the water column will keep the self-sealing check valve at the top of the HydraSleeve closed, and ensure that it retains its flat, empty profile for an indefinite period prior to recovery.

Note: Make sure that it is not pulled upward at any time during its descent. If the HydraSleeve is pulled upward at a rate greater than 0.5'/second at any time prior to recovery, the top check valve will open and water will enter the HydraSleeve prematurely.

2. Secure the tether at the top of the well by placing the well cap on the top of the well casing and over the tether.

Note: Alternatively, you can tie the tether to a hook on the bottom of the well cap (you will need to leave a few inches of slack in the line to avoid pulling the sampler up as the cap is removed at the next sampling event).

#### **III. Equilibrating the Well**

The equilibration time is the time it takes for conditions in the water column (primarily flow dynamics and contaminant distribution) to restabilize after vertical mixing occurs (caused by installation of a sampling device in the well).

• Situation: The HydraSleeve is deployed for the first time or for only one time in a well

The HydraSleeve is very thin in cross section and displaces very little water (<100 ml) during deployment so, unlike most other sampling devices, it does not disturb the water column to the point at which long equilibration times are necessary to ensure recovery of a representative sample.

In most cases, the HydraSleeve can be recovered immediately (with no equilibration time) or within a few hours. In regulatory jurisdictions that impose specific requirements for equilibration times prior to recovery of no-purge sampling devices, these requirements should be followed.

• Situation: The HydraSleeve is being deployed for recovery during a future sampling event

In periodic (i.e., quarterly or semi-annual) sampling programs, the sampler for the current sampling event can be recovered and a new sampler (for the next sampling event)

deployed immediately thereafter, so the new sampler remains in the well until the next sampling event.

Thus, a long equilibration time is ensured and, at the next sampling event, the sampler can be recovered immediately. This means that separate mobilizations, to deploy and then to recover the sampler, are not required. HydraSleeves can be left in a well for an indefinite period of time without concern.

#### IV. HydraSleeve Recovery and Sample Collection

- 1. Hold on to the tether while removing the well cap.
- 2. Secure the tether at the top of the well while maintaining tension on the tether (but without pulling the tether upwards)
- 3. Measure the water level in the well.
- 4. In one smooth motion, pull the tether up between 30" to 45" (36" to 54" for the longer HydraSleeve) at a rate of about 1' per second (or faster).

The motion will open the top check valve and allow the HydraSleeve to fill (it should fill in about 1 to 1.5 times the length of the HydraSleeve). This is analogous to coring the water column in the well from the bottom up.

When the HydraSleeve is full, the top check valve will close. You should begin to feel the weight of the HydraSleeve on the tether and it will begin to displace water. The closed check valve prevents loss of sample and entry of water from zones above the well screen as the HydraSleeve is recovered.

- 5. Continue pulling the tether upward until the HydraSleeve is at the top of the well.
- 6. Decant and discard the small volume of water trapped in the Hydrasleeve above the check valve by turning the sleeve over.

#### **V. Sample Collection**

**Note:** Sample collection should be done immediately after the HydraSleeve has been brought to the surface to preserve sample integrity.

- 1. Remove the discharge tube from its sleeve.
- 2. Hold the HydraSleeve at the check valve.
- 3. Puncture the HydraSleeve just below the check valve with the pointed end of the discharge tube
- 4. Discharge water from the HydraSleeve into your sample containers.

Control the discharge from the HydraSleeve by either raising the bottom of the sleeve, by squeezing it like a tube of toothpaste, or both.

5. Continue filling sample containers until all are full.

#### **Measurement of Field Indicator Parameters**

Field indicator parameter measurement is generally done during well purging and sampling to confirm when parameters are stable and sampling can begin. Because no-purge sampling does not require purging, field indicator parameter measurement is not necessary for the purpose of confirming when purging is complete.

If field indicator parameter measurement is required to meet a specific non-purging regulatory requirement, it can be done by taking measurements from water within a HydraSleeve that is not used for collecting a sample to submit for laboratory analysis (i.e., a second HydraSleeve installed in conjunction with the primary sample collection HydraSleeve [see Multiple Sampler Deployment below]).

#### **Alternate Deployment Strategies**

#### **Deployment in Wells with Limited Water Columns**

For wells in which only a limited water column exists to be sampled, the HydraSleeve can be deployed with an optional top weight instead of a bottom weight, which collapses the HydraSleeve to a very short (approximately 6" to 9") length, and allows the HydraSleeve to fill in a water column only 36" to 45" in height.

#### **Multiple Sampler Deployment**

Multiple sampler deployment in a single well screen can accomplish two purposes:

- It can collect additional sample volume to satisfy site or laboratory-specific sample volume requirements.
- It can accommodate the need for collecting field indicator parameter measurements.
- It can be used to collect samples from multiple intervals in the screen to allow identification of possible contaminant stratification.

It is possible to use up to 3 standard 30" HydraSleeves deployed in series along a single tether to collect samples from a 10' long well screen without collecting water from the interval above the screen.

The samplers must be attached to the tether at both the top and bottom of the sleeve. Attach the tether at the top with a stainless-steel clip (available from the manufacturer). Attach the tether at the bottom using a cable tie. The samplers must be attached as follows (figure 4):

- The first (attached to the tether as described above, with the weight at the bottom) at the bottom of the screen
- The second attached immediately above the first
- The third (attached the same as the second) immediately above the second

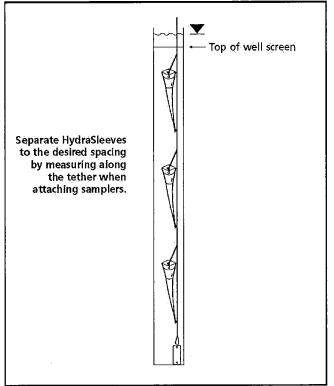


Figure 4. Multiple HydraSleeve deployment.

Alternately, the first sampler can be attached to the tether as described above, a second attached to the bottom of the first using a short length of tether (in place of the weight), and the third attached to the bottom of the second in the same manner, with the weight attached to the bottom of the third sampler (figure 5).

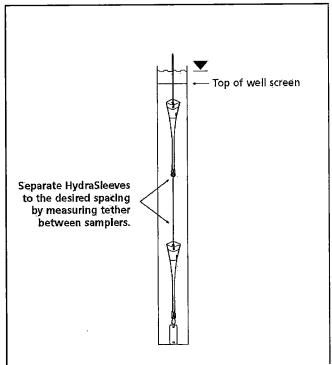


Figure 5. Alternative method for deploying multiple HydraSleeves.

In either case, when attaching multiple HydraSleeves in series, more weight may be required to hold the samplers in place in the well than would be required with a single sampler. Recovery of multiple samplers and collection of samples is done in the same manner as for single sampler deployments.

#### **Post-Sampling Activities**

The recovered HydraSleeve and the sample discharge tubing should be disposed as per the solid waste management plan for the site. To prepare for the next sampling event, a new HydraSleeve can be deployed in the well (as described previously) and left in the well until the next sampling event, at which time it can be recovered.

The weight and weight clip can be reused on this sampler after they have been thoroughly cleaned as per the site equipment decontamination plan. The tether may be dedicated to the well and reused or discarded at the discretion of sampling personnel.

#### References

McAlary, T. A. and J. F. Barker, 1987, Volatilization Losses of Organics During Ground-Water Sampling From Low-Permeability Materials, <u>Ground-Water Monitoring Review</u>, Vol. 7, No. 4, pp. 63-68

Parsons, 2005, Results Report for the Demonstration of No-Purge Ground-Water Sampling Devices at Former McClellan Air Force Base, California; Contract F44650-99-D-0005, Delivery Order DKO1, U.S. Army Corps of Engineers (Omaha District), U.S. Air Force Center for Environmental Excellence, and U.S. Air Force Real Property Agency

Robin, M. J. L. and R. W. Gillham, 1987, Field Evaluation of Well Purging Procedures, <u>Ground-</u> Water Monitoring Review, Vol. 7, No. 4, pp. 85-93



## Instructions for Installing HydraSleeves with Spring Clip and Top Weight

Your HydraSleeve will attach directly to the bottom of the rope, as follows:

You will not have a weight on the end of your rope. Instead, you will only have a SST ring and black snap connector.

Prepare your HydraSleeve for deployment as pictured to the right. Flex the top of the HydraSleeve then insert it into the hollow top weight, being sure to align the holes of the HydraSleeve with the holes of the top weight.

Next, connect the stainless steel spring clip to the top of the HydraSleeve and the top weight.

Squeeze the clip closed slightly and insert the legs into the top of the HydraSleeve.

Release so the legs spread and extend through the holes in the HydrsSleeve and the weight; Jocking clip, weight and HydraSleeve together.

Attach tether to the apex of the clip.







Attach the spring clip to the end of the tether using the black snap connector provided. Finally, attach the solid weight to the bottom of the HydraSleeve using a cable tie.

Please give us a call if you need further assistance. Thank you.



P.O. Box 443, Snellville, Georgia 30078-0443 800-474-2490 770-978-9971 Fax: 770-978-8661 www.eonpro.com



Attach Snap Connector on tether to Split Ring on bottom of Well Cap

Aluminum Identification tag

Attach Spring Clip to Split Ring on bottom of tether.

Insert HydraSleeve into Top Weight, aligning holes. Insert Spring Clip into holes, catching both HydraSleeve and Top Weight. When deployed, HydraSleeve will be compressed to sample near bottom of well.

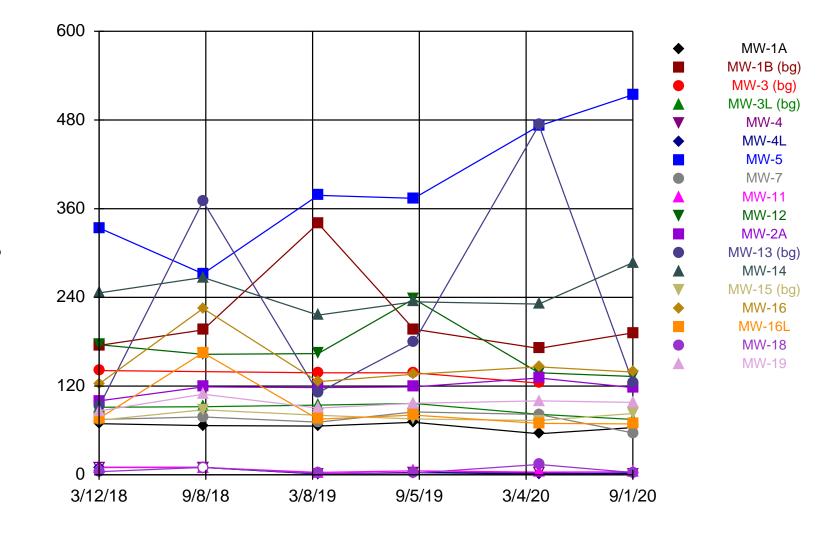
Attach weight to bottom of Hydrasleeve

P.O. Box 443, Snellville, Georgia 30078-0443 **800-474-2490** 770-978-9971 Fax: 770-978-8661 Prices are subject to change. <u>www.eonpro.com</u> Page 1 of 1

## **APPENDIX E**

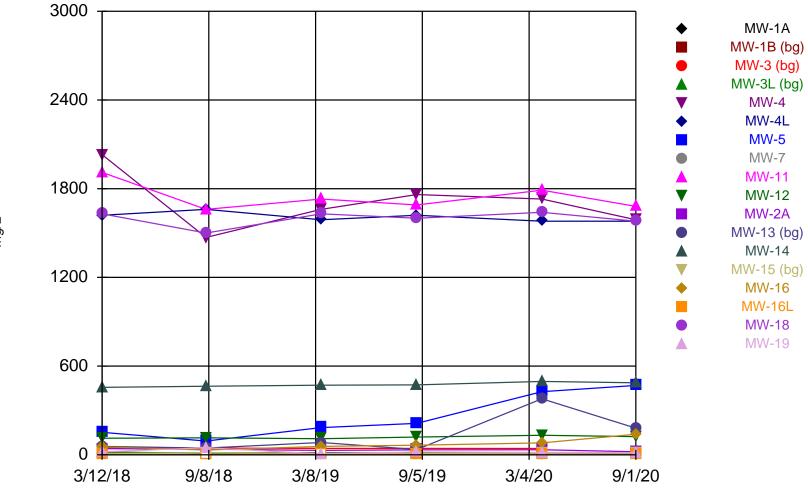
CONTINENTAL CEMENT COMPANY Time Series Plots

**Time Series** 



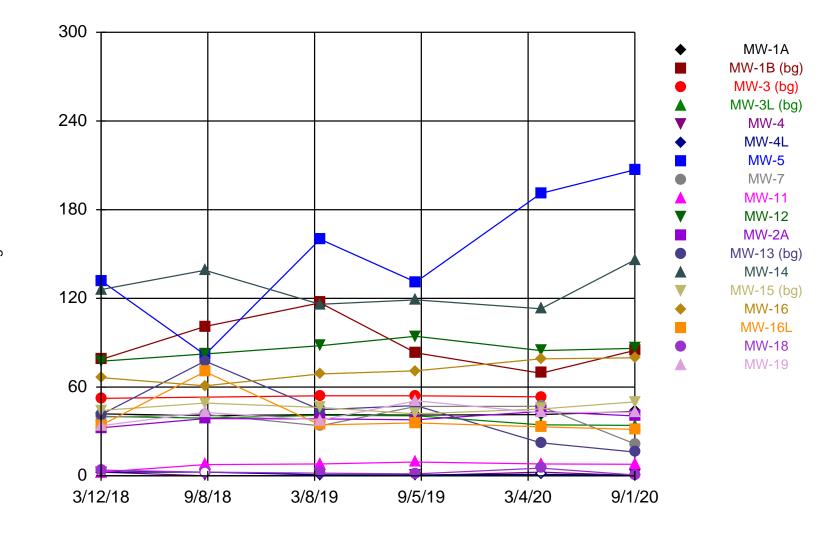
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**Time Series** 



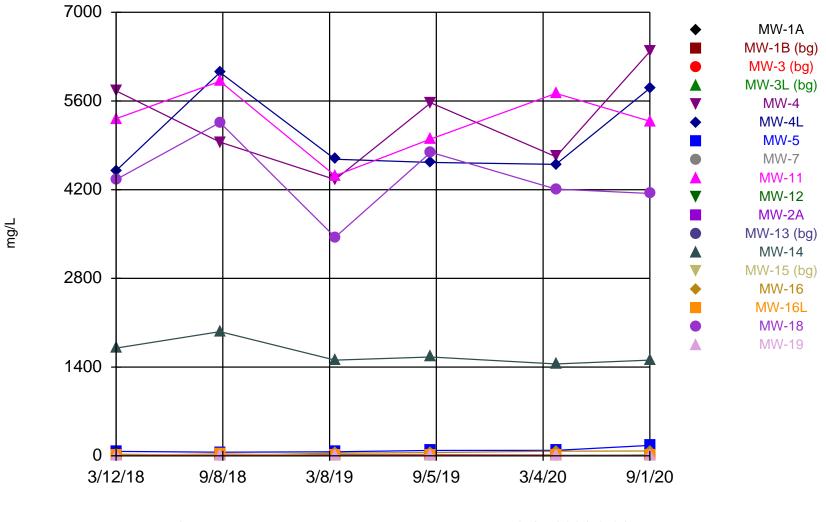
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**Time Series** 



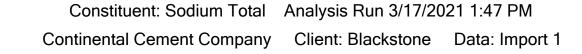
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**Time Series** 

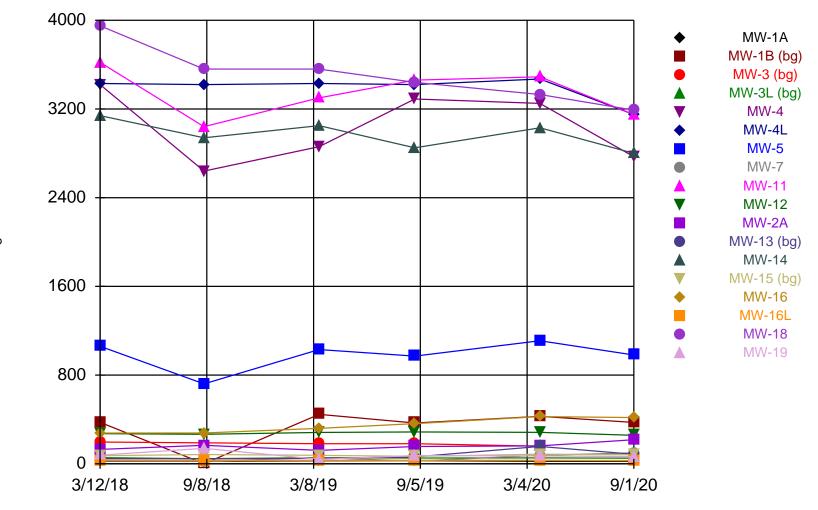


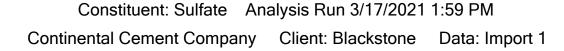
Constituent: Potassium Total Analysis Run 3/17/2021 2:01 PM Continental Cement Company Client: Blackstone Data: Import 1 700 MW-1A MW-1B (bg) MW-3 (bg) MW-3L (bg) 560 MW-4 MW-4L **MW-5** MW-7 MW-11 420 MW-12 V MW-2A MW-13 (bg) MW-14 MW-15 (bg) V 280 MW-16 **MW-16L** MW-18 MW-19 140 0 3/12/18 9/8/18 9/1/20 3/8/19 9/5/19 3/4/20





**Time Series** 







**APPENDIX D** 

Site Operations Plan



# **REVISED Site Operations Plan**

Continental Cement CKD Monofill Landfill 301 East Front Street Buffalo, Iowa IDNR Landfill Permit Number 82-SDP-16-97P

> Prepared for: Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by: Blackstone Environmental 514 17<sup>th</sup> Street, #206 Moline, Illinois 61265



November 5, 2021



REVISED SITE OPERATIONS PLAN CONTINENTAL CEMENT CKD MONOFILL LANDFILL 301 EAST FRONT STREET BUFFALO, IOWA IDNR LANDFILL PERMIT NUMBER 82-SDP-16-97P

Prepared for: Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by:

Krista A. Brodersen Senior Project Manager

**Reviewed by:** 

Lindsay E. James, R.G Senior Project Manager



# TABLE OF CONTENTS

Section Page
TABLE OF CONTENTS ii
1.0 INTRODUCTION 1
1.1 Site Information (567 IAC 115.13(1)) 1
1.2Site Legal Description (567 IAC 115.13(2)) and Proof of Ownership (567 IAC 115.13(9))1
1.3 Site Map (567 IAC 115.13(3)) 2
1.4 Waste Data (567 IAC 115.13(4),(6)) 2
1.5         Organization of Project Management (567 IAC 115.13(5))         2           1.6         Disposal Process (567 IAC 115.13(6))         3
1.6         Disposal Process (567 IAC 115.13(6))         3           1.7         Equipment Plan         4
1.7.1 Equipment (567 IAC 115.13(7)) 4
1.8 Equipment Contingency Plan (567 IAC 115.13(8)) 4
1.9 Additional Information 4
1.9.1 Construction and Operation (567 IAC 115.6) 4
1.9.2 Inspection Prior to Start-Up (567 IAC 115.12) 5
1.9.3 Facility Development Timetable 5
2.0 GENERAL OPERATING INFORMATION 5
2.1         Cover Materials Quantities and Sources (567 IAC 115.26(1)1(1))         5           2.2         Site Area (567 IAC 115.26(1)1(2))         5
2.2 Site Area (567 IAC 115.26(1)1(2)) 5
2.3         Solid Waste Unloading (567 IAC 115.26(2)a)         6
2.4 Facility Access (567 IAC 115.26(2)b 6
2.5 Site Records (567 IAC 115.26(2)c) 6
2.6         Permanent Sign (567 IAC 115.26(2)d         6           2.7         Collection of Leachate (567 IAC 115.26(2)e)         6
2.7         Collection of Leachate (567 IAC 115.26(2)e)         6           2.8         Inclement Weather Operations (567 IAC 115.26(2)f)         7
2.9 Cover Material (567 IAC 115.26(2)g) 7
2.11 Finished Surface Maintenance (567 IAC 115.26(2)i)
2.10       Grading and Drainage Control (567 IAC 115.26(2)h)       8         2.11       Finished Surface Maintenance (567 IAC 115.26(2)i)       8         2.12       Landfill Inspections (567 IAC 115.26(2) j, k, and l)       8
2.13 Hydrologic Monitoring System (567 IAC 115.26(3) 8
3.0 OPÉRATING REQUIREMENTS FOR ALL SANITARY DISPOSAL PROJECTS (567 IAC 115.27) 9
4.0 SPECIFIC REQUIREMENTS FOR A SANITARY LANDFILL PROPOSING TO ACCEPT A
SPECIFIC TYPE OF SOLID WASTE 9
4.1 Plan Requirements (567 IAC 115.28(1)) 9
4.2 Specific operating requirements for sanitary landfills proposing to accept a specific type of solid
waste (567 IAC 115.28(2)) 10
4.3 Daily, Intermediate, and Final Cover (567 IAC 115.28(2)a) 10
4.4Number and Duties of Personnel (567 IAC 115.28(2)b)104.5Storage and Preliminary Processing of Solid Waste (567 IAC 115.28(2)c)11
<ul> <li>4.5 Storage and Preliminary Processing of Solid Waste (567 IAC 115.28(2)c)</li> <li>4.6 Safety Procedures and Equipment and Operating Equipment (567 IAC 115.28(2)d</li> </ul>
and e)
4.7 Buildings and Shelter (567 IAC 115.28(2)f) 11
4.8 Mine Monitoring 11
5.0 EMERGENCY RESPONSE AND REMEDIAL ACTION PLANS (567 IAC 115.30) 12

# FIGURES

- Topographic Map
   Site Plan
- 3 Landfill Location

# APPENDICES

- A Legal Description
  B CKD Analytical Results
  C Monthly Certified Operators Inspection Form
  D Emergency Response and Remedial Action Plan



# 1.0 INTRODUCTION

This Site Operations Plan (SOP) presents a written plan that details the operations related to the Cement Kiln Dust (CKD) monofill operated by Continental Cement Company, LLC (Continental) at 301 East Front Street in Buffalo, Scott County, Iowa (Site).

Quarrying and manufacturing of Portland cement products have been conducted at the Continental facility since 1924 and other uses are not anticipated in the future. The cement manufacturing process includes the heating of limestone with silica, alumina, and iron minerals to form clinker. The clinker (nodules of sintered material) is mixed with gypsum and other additives and ground into a fine powder to form cement. As part of the manufacturing process, particulate matter is generated as a by-product of maintaining kiln chemistry to control the composition of the cement product. This material is known as CKD. Continental operates an approximately 20-acre monofil for the disposal of CKD. The southern portion of the monofill has been filled to original grade and closed in general accordance with the requirements of the lowa Department of Natural Resources (IDNR) Permit Number 82-SDP-15-96C. An active monofill disposal cell is operated under IDNR Permit Number 82-SDP-16-97P. Historically, an average of 30 tons of CKD per day has been disposed at the monofill. Current operations and practices have reduced the amount of CKD sent to the monofill on a regular basis, with typical monthly disposal rates of 10 tons.

Information	Name	Address	Telephone	
			Number	
Owner/Applicant	Continental Cement Company,	301 East Front Street	563-323-2751	
	LLC	Buffalo, Iowa 52728	505-525-2751	
Responsible	Shawn Mages, Plant Manager	301 East Front Street	563-328-6236	
Official	Shawn Mages, Flant Manager	Buffalo, Iowa 52728	505-526-0250	
Licensed Design Engineer	Kyle Kukuk, P.E., Blackstone	16200 Foster		
	Environmental, Inc., Iowa	Overland Park, Kansas	913-495-9990	
	License Number: 22790	66085		

# 1.1 Site Information (567 IAC 115.13(1))

# 1.2 Site Legal Description (567 IAC 115.13(2)) and Proof of Ownership (567 IAC 115.13(9))

The Site is shown on Figure 1 and is located approximately four miles west of Davenport, Iowa within Sections 14, 15, 22, and 23 of Township 77 North, - Range 2 East (Buffalo Township), Scott County, Iowa. The development fill area is located between N 1500 to N 2300 and W 300 to E 500. The facility has been in operation, under various ownership, from 1924 for the quarrying of limestone rock and the manufacture of Portland cement. The CKD landfill is located in an inactive portion of the quarry approximately 2,000 feet east of the active quarry area and comprises approximately 20 acres. A copy of the legal description is provided in Appendix A.



# 1.3 Site Map (567 IAC 115.13(3))

Figure 2 is a map of the Continental facility that includes the zoning and land use, haul routes, homes and buildings within a half-mile, and section lines and legal boundaries. Airports or runways are not located near the Site. Figure 3 is the landfill location.

#### 1.4 Waste Data (567 IAC 115.13(4),(6))

The cement manufacturing process includes the heating of limestone with silica, alumina, and iron minerals to form clinker. The clinker (nodules of sintered material) is mixed with gypsum and other additives and ground into a fine powder to form cement. As part of the manufacturing process, particulate matter, referred to as CKD, is generated as a by-product of maintaining kiln chemistry to control the composition of the cement product. Continental operates an approximately 20-acre monofil for the disposal of CKD. The southern portion of the monofill has been filled to original grade and closed in general accordance with the requirements of the lowa Department of Natural Resources (IDNR) Permit Number 82-SDP-15-96C. An active monofill disposal cell is operated under IDNR Permit Number 82-SDP-16-97P. An average of 10 tons of CKD per month is disposed at the monofill.

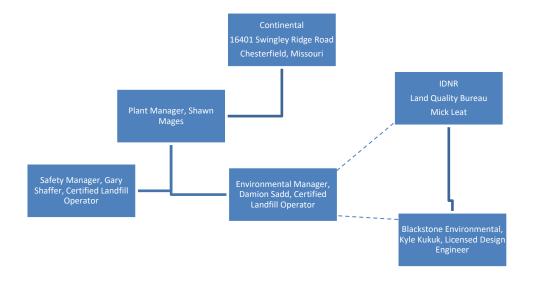
A sample of the CKD material was collected on October 8, 2021 and analyzed for Toxicity Characteristic Leaching Procedure (TCLP) metals, calcium, aluminum, magnesium, iron, and potassium. These sample results are considered representative of the wastes currently disposed in the landfill. The results are presented in Appendix B. The CKD was also sampled for TCLP metals in 2003, 2010, and 2013. The previous results are also included in Appendix B.

# 1.5 Organization of Project Management (567 IAC 115.13(5))

The Site is owned and operated by Continental. Mr. Shawn Mages is the Plant Manager and is the landfill operator responsible for the overall operation of Continental. The two certified landfill operators are Mr. Damion Sadd, Continental Environmental Manager, and Mr. Gary Shaffer, Continental Safety Manager. Mr. Sadd and Mr. Shaffer, as well as other personnel, report to Mr. Mages. An organization chart is below.

The Licensed Design Engineer for Continental is: Kyle Kukuk, P.E., Iowa License Number: 22790 Blackstone Environmental, Inc. 16200 Foster Street Overland Park, Kansas 66085 913-495-9990





# 1.6 Disposal Process (567 IAC 115.13(6))

The CKD area operates in a consistent and predictable manner because the source and nature of the CKD are known. Other waste materials are not allowed in the area.

The CKD is captured with air quality control equipment and stored in a silo located south of the landfill. When the silo is filled, the CKD is wetted to control dust and transported by haul truck to the monofill where it is dumped. End loaders and bulldozers level and push the piles as needed. In general, the monofill is raised uniformly over the surface. The CKD is placed by dumping the trucks onto the landfill working face. The placement is determined by the landfill operator on a weekly basis.

The CKD is hauled from the silo on an on-site gravel access road, across East Front Street, and then again on an on-site gravel access road to the landfill. The gravel access roads have speed limits and are wetted as necessary. East Front Street also has a speed limit. Continental personnel are responsible for maintaining the access roads in a suitable condition for traffic by vehicles.

Due to the cementitious nature of the conditioned CKD, the material tends to bind together when placed at the landfill forming a relatively uniform and solid deposit. The material is able to stand at a relatively steep angle of repose with negligible risk of slumping or slope failure. Further, the material is relatively impervious thereby reducing the likelihood of saturation which could reduce the shear strength and lead to slope instability.

Employees with duties associated with the storage, handling, transport, or disposal of CKD are trained to place CKD in a manner which will reduce the likelihood of slope failures, waste shifts, and waste subsidence. Transport vehicle drivers are instructed to place material at a safe distance back from the edge of the active cell to avoid surcharging the edge of the cell. Accumulated



material is periodically pushed into the active cell with earthmoving equipment. The landfill is also inspected weekly so that situations which would lead to mass movement of waste are avoided or quickly corrected.

# 1.7 Equipment Plan

Generally, end loaders and bulldozers are used for placement, compaction, and cover of CKD. Other equipment is available for the operators as needed from the maintenance building located south of the monofill.

# 1.7.1 Equipment (567 IAC 115.13(7))

The table below details the equipment to be used, capacities, and expected loads.

Equipment	Capacity	Expected Loads
End loader	12 yards	12 yards
Haul trucks	60 tons	60 tons
Bulldozer	none	none
Leachate Pump	20 gallons per minute	20 gallons per minute

# 1.8 Equipment Contingency Plan (567 IAC 115.13(8))

In the event of equipment breakdown, the equipment is either repaired where it broke down or the CKD is removed from the equipment with an excavator and placed into another operating vehicle for disposal.

During maintenance downtime of equipment, Continental has other equipment stored in the maintenance building that will be used.

In the event of a fire in equipment or vehicles, the fire would be extinguished using fire extinguishers located in each vehicle. If the equipment is drivable and safe to be driven after the fire has been extinguished, the CKD will be disposed at the landfill. If the equipment is not drivable/safe, the CKD will be removed from the equipment with an excavator and placed into another operating vehicle for disposal.

# **1.9** Additional Information

Additional information required by the IDNR is provided below.

# 1.9.1 Construction and Operation (567 IAC 115.6)

The landfill has been constructed and operates according to the approved plans and term of IDNR Landfill Permit Number 82-SDP-16-97P.



# 1.9.2 Inspection Prior to Start-Up (567 IAC 115.12)

The IDNR will be notified when the initial construction of a sanitary disposal project has been completed in order that an inspection may be made to determine that the project is constructed as designed. Solid waste will not be accepted until that project has been inspected and approved by the IDNR.

# 1.9.3 Facility Development Timetable

The facility has been in operation, under various ownership, since 1924 for the quarrying of limestone rock and the manufacture of Portland cement. The first CKD was placed in the landfill in 1980s. The southern portion of the monofill was filled to original grade and closed in 2005 in general accordance with the requirements of the Iowa Department of Natural Resources (IDNR) Permit Number 82-SDP-15-96C. The northern portion of the monofill is an active cell that was first used in 1998. It is operated under IDNR Permit Number 82-SDP-16-97P. It is expected to provide approximately 11 years of capacity at the current waste generation rates.

# 2.0 GENERAL OPERATING INFORMATION

The general operating requirements outlined in 567 IAC 115.26 are detailed in the following sections.

# 2.1 Cover Materials Quantities and Sources (567 IAC 115.26(1)1(1))

The monofill is approximately 20 acres in area. The southern portion of the monofill has been filled to original grade and closed in general accordance with the requirements of IDNR Permit Number 82-SDP-15-96C. Cell 2 is the active cell and is approximately 10 acres in area. It is estimated that it has approximately 11 years before it is at capacity. As the active cell has over a decade before it is closed, the source, volume, and characteristics of cover material to be used is undetermined at this time. It is expected that clay and topsoil overburden from the quarry would be used as cover materials.

# 2.2 Site Area (567 IAC 115.26(1)1(2))

The Continental CKD monofill is located in an inactive portion of Continental's former rock quarry approximately 2,000 feet east of the active quarry area and comprises approximately 20 acres. The monofill is located approximately 1.3 miles east/northeast of the City of Buffalo in Scott County, Iowa, and approximately 700 feet north of the Mississippi River. Please refer to Figures 1, 2, and 3 for the Site location.

The Continental facility is bound by the Mississippi River to the south, Linwood Mining to the east, farmland to the north, and undeveloped land, farmland, and residences to the west. The CKD



monofill is located approximately 200 feet from the Linwood Mining facility to the east, approximately 1,400 feet from the Mississippi River to the south, and over a mile from the northern and western boundaries.

# 2.3 Solid Waste Unloading (567 IAC 115.26(2)a)

CKD is unloaded at the CKD disposal area only when an operator is on duty at that area. An equipment operator unloads and spreads the waste.

# 2.4 Facility Access (567 IAC 115.26(2)b

Access to the CKD disposal area is restricted to Continental personnel. The Site is not open to the public and a gate is located at the entrance to the Site.

#### 2.5 Site Records (567 IAC 115.26(2)c)

Copies of permits, engineering plans, and reports are kept at the Continental offices located at 301 East Front Street in Buffalo, Iowa.

# 2.6 Permanent Sign (567 IAC 115.26(2)d

The Site is not open to the public and has a permanent sign posted at the site entrance specifying:

- Name of operation.
- That the site is not open to the public.
- An emergency telephone number.

# 2.7 Collection of Leachate (567 IAC 115.26(2)e)

The monofill has an engineered clay liner and leachate collection system to contain and remove leachate from the landfill units. Design plans for the leachate collection system were completed in 1997 and an as-built construction drawing for the system was completed in 2001. The leachate collection system consists of upper and lower drainage layers that include a 4-foot-thick clay layer between the two. The upper drainage layer has two 2-inch diameter slotted polyvinyl chloride (PVC) collection lines installed in a 1-foot-thick sand drainage layer. Three monitoring points (UL-1, UL-2, and UL-3) monitor the leachate thickness in the upper drainage layer. The lower drainage layer is located below the 4-foot-thick clay liner and consists of a 1-foot-thick sand drainage layer. No PVC leachate collection lines were installed in the lower drainage layer. Three monitoring points (LL-1, LL-2, and LL-3) monitor the leachate thickness in the upper drainage layer.

The slotted 2-inch PVC collection lines in the upper drainage layer connect to the 6-inch solid PVC header line which drains into the leachate collection sump. Both leachate collection lines have cleanout points installed at the intersections with the header line on the west side of the



monofill. The leachate collection lines are jetted and cleared a minimum of once per year or as needed.

A 10-foot diameter, 12-foot deep, leachate collection sump is located along the southwest portion of the monofill. The 6-inch leachate header drains to the collection sump where it is ultimately pumped out and conveyed back up to the top of the landfill and applied to the waste mass via sprinkler system for dust suppression. Recent updates include installation of solar powered equipment and a supervisory control and data acquisition (SCADA) system to allow for the operators to monitor the leachate sump pump status remotely.

The solar powered leachate pumping system equipment includes solar panels, leachate pump with level-sensing transducer, leachate piping to the active face, leachate sprayer, and mounting equipment. The SCADA system and monitoring station at the leachate sump includes a leachate sump level, high level alarm of leachate sump, and low-level shutoff of leachate sump.

The total volume of leachate collected for each month is recorded as well as the elevation of leachate in the piezometers. If the water column is greater than one foot, these monitoring points are purged until the water column is less than one foot. This information is provided to the IDNR in the Annual Water Quality Control Report.

The combined landfill liner system, drainage, and leachate collection systems are present to prevent contaminants from being released to groundwater.

Leachate recirculation is not an approved activity, nor is it currently conducted at the Site. Leachate is only used to control dusts and prevent erosion as these activities are not expected to exacerbate leachate head issues. Should recirculation be desired in the future, a request for approval will be submitted to IDNR.

# 2.8 Inclement Weather Operations (567 IAC 115.26(2)f)

An all-weather fill area, which is accessible for disposal during all weather conditions, is present at the Site. The roads at the Continental Site are inspected periodically and are resurfaced as necessary. The CKD is wetted prior to transport and is therefore, not susceptible to high winds. Additionally, leachate is sprayed on the CKD to reduce dust entrainment. A snowplow or bulldozer are used when snow is present to maintain the roadways.

# 2.9 Cover Material (567 IAC 115.26(2)g)

Daily cover is accomplished through placement of CKD and spraying of leachate. CKD is covered if inactive for 60 days. Clay is used as cover material followed by topsoil for long-term cover material.



# 2.10 Grading and Drainage Control (567 IAC 115.26(2)h)

Surrounding area runoff is not allowed into the landfill. Area grade diverts any runoff away from or around the landfill area. Rain that falls directly onto the uncapped monofill area is contained within the monofill and percolates into the landfilled waste. Such percolation is collected as leachate.

#### 2.11 Finished Surface Maintenance (567 IAC 115.26(2)i)

The finished surface of the monofill is repaired as required, covered with soil, and seeded with native grasses or other suitable vegetation immediately upon completion or promptly in the spring on areas terminated during winter conditions. As necessary, seeded slopes are covered with straw or similar material to prevent erosion.

# 2.12 Landfill Inspections (567 IAC 115.26(2) j, k, and I)

The monofill area is staked and inspected semi-annually by a professional engineer registered in the State of Iowa. A Semi-Annual Engineers Report is prepared by the engineer and submitted to the IDNR within 30 days of the inspection. The report includes areas of conformance or nonconformance with the approved plans and specifications.

If any pockets, seams, or layers of sand or other highly permeable material are encountered at the landfill, the permit holder will promptly notify the IDNR and will ensure that a professional engineer registered in the State of Iowa has certified that sands encountered were excavated or sealed off properly or otherwise handled as explicitly provided for in the permit before solid waste is disposed of in that area of the monofill.

The total volume of leachate collected for each month is recorded as well as the elevation of leachate in the piezometers. This information is provided to the IDNR in the Annual Water Quality Control Report.

# 2.13 Hydrologic Monitoring System (567 IAC 115.26(3)

A Revised Hydraulic Monitoring System Plan dated March 29, 2021 (Revised April 19, 2021) was submitted to the IDNR that presents sampling and analysis procedures for the Continental monofill. The Revised Hydraulic Monitoring System Plan describes the hydrogeologic setting of the facility, the groundwater monitoring network, groundwater bearing zones, background and compliance monitoring parameters and frequencies, sampling procedures, groundwater flow characteristics, and statistical methodology.



# 3.0 OPERATING REQUIREMENTS FOR ALL SANITARY DISPOSAL PROJECTS (567 IAC 115.27)

Continental's general operating procedures to comply 567 IAC 115.27 (455B) are presented below.

- 115.27(1) Open burning is not conducted at the Site.
- 115.27(2) Litter is not disposed of at the Site. Litter from Site operations is containerized and disposed of at the Scott County Landfill.
- CKD is confined to the CKD disposal area. Due to the nature of CKD, it is not strewn beyond the confines of the operating area.
- 115.27(3) Scavenging is prohibited. As the waste disposed consists of CKD, materials to be scavenged or salvaged are not present.
- 115.27(4) As the landfill only accepts CKD, the waste stream does not support rodents, insects, or other vermin. The landfill does not produce a nuisance odor.
- 115.27(5) Equipment designated in the plans and specifications, or equivalent equipment are used to operate the site. Generally, end loaders and bulldozers are used for placement, compaction, and cover of CKD. Other equipment is available for the operators as needed from the maintenance building located south of the monofill.
- 115.27(6) The major internal roads consist of all-weather construction and are maintained in good condition. Dust is controlled on internal roads.
- 115.27(7) The Site is not open to the public.
- 115.27(8) Free liquids or waste containing free liquids are not disposed at the CKD landfill.

# 4.0 SPECIFIC REQUIREMENTS FOR A SANITARY LANDFILL PROPOSING TO ACCEPT A SPECIFIC TYPE OF SOLID WASTE

# 4.1 Plan Requirements (567 IAC 115.28(1))

The cement manufacturing process includes the heating of limestone with silica, alumina, and iron minerals to form clinker. The clinker is mixed with gypsum and other additives and ground into a fine powder to form cement. As part of the manufacturing process, CKD is generated as a by-product of maintaining the composition quality of the cement product. The average chemical composition of CKD reflects the composition of the feed rock and soils and includes the following



compounds: CaCO<sub>3</sub>, CaO, AL<sub>2</sub>O<sub>3</sub>, Ca(OH)<sub>2</sub>, Ca(MgFe)(CO<sub>3</sub>)<sub>2</sub>, SiO<sub>2</sub>, K<sub>2</sub>SO<sub>4</sub>, KCl, and CaMg(CO<sub>3</sub>)<sub>2</sub>.

A sample of the CKD material was collected on October 8, 2021 and analyzed for TCLP Metals, calcium, aluminum, magnesium, iron, and potassium. These sample results are considered representative of the wastes currently disposed in the landfill. The results are presented in Appendix B.

The monofill has an engineered clay liner and leachate collection system to contain and remove leachate from the landfill units. Please refer to Section 2.7 for further details. A Revised Hydraulic Monitoring System Plan dated March 29, 2021 (Revised April 19, 2021) is in use at the Site that presents sampling and analysis procedures for the monofill. Please refer to Section 2.13 for further details.

# 4.2 Specific operating requirements for sanitary landfills proposing to accept a specific type of solid waste (567 IAC 115.28(2))

Continental's monofill is used for the disposal of CKD fill only. Other wastes are not accepted. Continental's specific operating requirements to comply 567 IAC 115.28(2) are presented below.

# 4.3 Daily, Intermediate, and Final Cover (567 IAC 115.28(2)a)

In general accordance with the permit, the CKD waste is covered and graded with a minimum of 6-inches of compacted soil if inactive for 60 days rather than daily as CKD is the only waste accepted.

Disposal areas in the monofill not used for more than 60 days will be covered with an additional six inches of soil for a total of one foot of cover material. Areas will be seeded as required to prevent erosion.

The final cover will be consistent with the proposed land use and will not be less than two feet. Final cover is described in the Closure and Development Plan dated January 1997 and a Supplemental to Cement Kiln Dust Closure and Development Plan dated June 1997 that has been submitted to the IDNR.

# 4.4 Number and Duties of Personnel (567 IAC 115.28(2)b)

The CKD monofill is owned, operated, and managed by Continental. The designated person responsible for operations is identified in Section 1.5 above. There are two certified operators and multiple employees that operate landfill equipment and perform filling and cover operations. Key features of the facility will be inspected on an approximately monthly basis in order to supplement the biannual inspections. The form included in Appendix C will be used by the Certified Operators on an approximately monthly basis to inspect the facility.



# 4.5 Storage and Preliminary Processing of Solid Waste (567 IAC 115.28(2)c)

The CKD area operates in a consistent and predictable manner because the source and nature of the CKD are known. Other waste materials are not allowed in the area. The CKD is wetted and transported by haul truck to the monofill where it is dumped. CKD is wetted prior to transport to control dusts during transport of wastes to the working face for disposal. End loaders and bulldozers level and push the piles as needed. In general, the monofill is raised uniformly over the surface.

# 4.6 Safety Procedures and Equipment and Operating Equipment (567 IAC 115.28(2)d and e)

Typical equipment used to manage landfill operations includes end loaders and bulldozers. Other equipment is available to the operators if the need arises from the maintenance building located south of the monofill. In the event of an equipment breakdown, equipment is repaired. In the event of fire, landfill equipment is equipped with a fire extinguisher. The Scott County fire department will be called depending on the severity of the condition or in the event of personnel injury. Maintenance downtime is predictably rare and of very short duration.

Equipment designated in the plans and specifications, or equivalent equipment will be used to operate the Site.

# 4.7 Buildings and Shelter (567 IAC 115.28(2)f)

An approximately 4,200 square foot maintenance building is located south of the monofill. The maintenance building contains an office, breakroom, and maintenance area.

# 4.8 Mine Monitoring

In a letter dated September 9, 2020, IDNR required the sampling of monitoring well MW-2CR annually to monitor groundwater quality downgradient from the landfill. The monitoring well is located on Continental's property and closely adjacent to the landfill. The well was installed in 2017 by Terracon Consultants. According to Terracon Consultants' Well Record, the well was drilled to a depth of 107 feet where an open mine was encountered. Based on the Well Record, the well casing was grouted to 19 feet below ground surface (bgs) and was not sealed from 19 feet bgs down. The Well Record indicates the bottom of the well is open to a Linwood Mining and Materials (Linwood) mine shaft. Linwood is located adjacent to Continental and has mine shafts that are under the Continental property. The mine shafts beneath the Continental property are no longer mined and are used to exhaust lime kiln dust and gases. Continental has not granted Linwood permission to exhaust beneath their property and there are no agreements between the companies regarding the exhaust.



In the past, MW-2CR was not able to be sampled due to the amount of exhaust released when the well cap was opened. Continental has coordinated with Linwood to sample the well during a temporary shutdown of Linwood kilns and/or during a period when exhausts are treated through other emission control equipment. During 2021, Linwood indicated they were having a temporary shutdown of their kilns on October 8, 2021 and the well was sampled.

In July 2021, groundwater monitoring well MW-21 was installed on the eastern boundary of the Site, adjacent to the Linwood property but not within the mine shaft. This well is now sampled as part of the routine semi-annual monitoring.

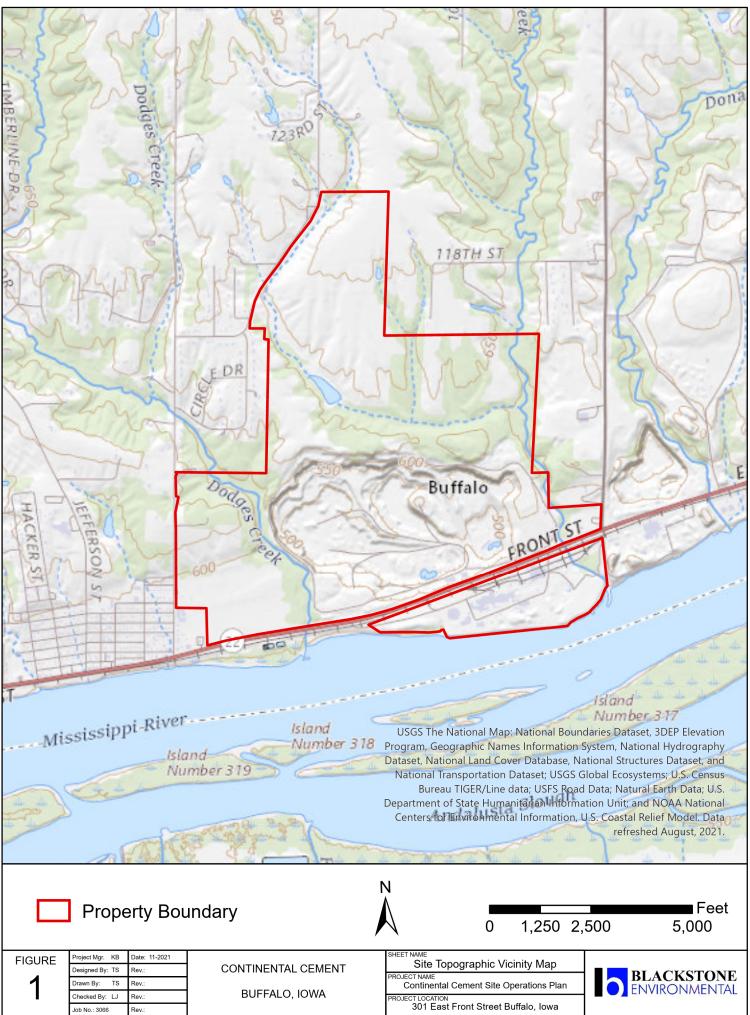
These samples will be used along with the routine groundwater results to monitor and evaluate conditions within the mine as they relate to Continental operations to ensure that the materials present within the mine are not contributing to or exacerbating leachate releases associated with Continental. The results of MW-2CR and MW-21 monitoring will be included as part of a separate report.

# 5.0 EMERGENCY RESPONSE AND REMEDIAL ACTION PLANS (567 IAC 115.30)

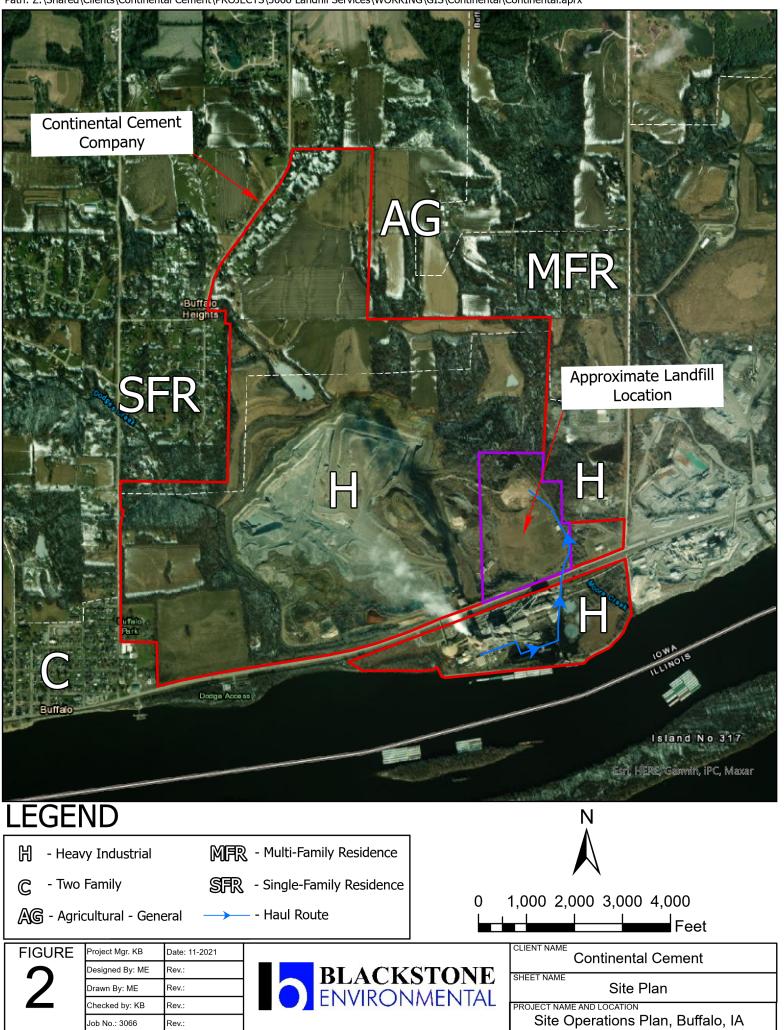
In 2021, Continental updated their Emergency Response and Remedial Action Plan (ERRAP) to comply with 567 IAC 115.30. A copy of the updated plan is included in Appendix D.

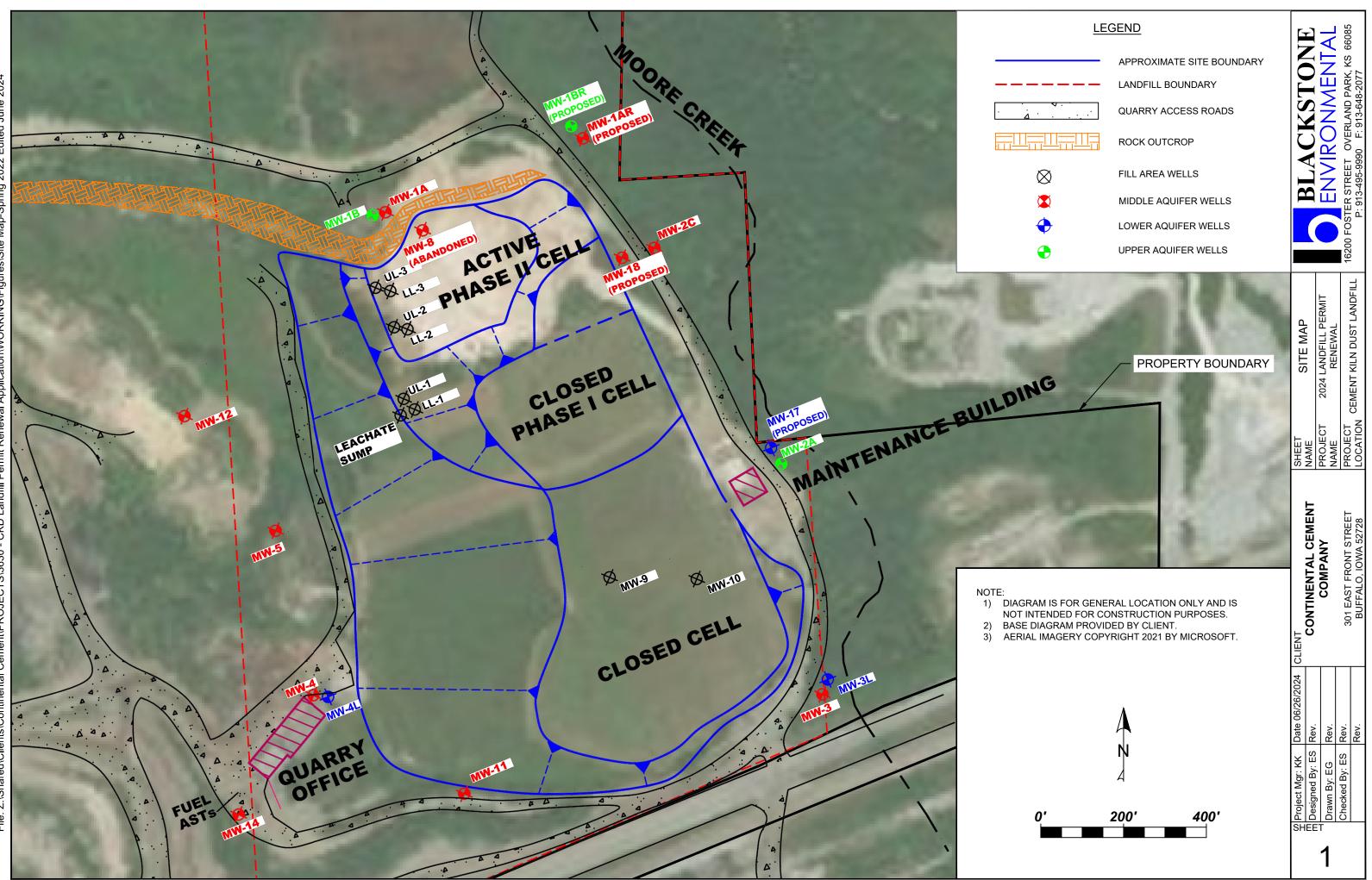
FIGURES

Z:\Shared\Clients\Continental Cement\PROJECTS\3066 Landfill Services\WORKING\GIS\Continental



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**APPENDIX A** 

Legal Description

# CONTINENTAL CEMENT COMPANY, L.L.C.

#### **ASSISTANT SECRETARY'S CERTIFICATE**

#### May 9, 2018

The undersigned, being the duly appointed and acting Assistant Secretary of Continental Cement Company, L.L.C., a Delaware limited liability company (the "<u>Company</u>"), hereby certifies, as of the date hereof, on behalf of the Company, solely in such person's capacity as Assistant Secretary of the Company and not in such person's individual capacity, as follows:

- Pursuant to that certain Asset Purchase Agreement, dated as of April 16, 2015, by and among the Company, Lafarge North America, Inc., a Maryland corporation ("Seller") and certain other parties, as guarantors for the Company, the Company purchased from Seller and Seller sold to the Company certain assets of Seller, including, among other assets, (a) a cement plant located in Buffalo, Iowa (the "Cement Plant"), (b) a quarry located in Davenport, Iowa (the "Quarry") and (c) a cement distribution terminal located in West Des Moines, Iowa (the "Terminal"), in each case more particularly described on the attached <u>Exhibit A</u> (collectively, the "Davenport Properties"), each of which are used in the business of (i) mining aggregates at the Quarry and (ii) producing, marketing, distributing and selling portland cement and related products at or from the Cement Plant and the Terminal (the "Transferred Business").
- 2. The Company owns all right, title and interest in and to the Davenport Properties used in connection with the Transferred Business.

[Signature page follows]

IN WITNESS WHEREOF, the undersigned has hereunto set his hand on behalf of the Company as of the date first written above.

1/ By:

Name: Chris Gaskill Title: Assistant Secretary

# EXHIBIT A

#### **Davenport Properties**

#### WEST DES MOINES

THAT PART OF LOT ONE (1) OF THE WEST 854 FEET OF LOT F VALLEY FUNCTION; PART OF LOTS D, E, F AND THE VACATED STREET NORTH OF LOT E IN VALLEY JUNCTION, MORE PARTICULARLY DESCRIBED AS FOLLOWS;

A TRACT OF LAND LYING IN THE NORTHEAST QUARTER OF SECTION 15, TOWNSHIP 78 NORTH, RANGE 25 WEST OF THE FIFTH PRINCIPAL MERIDIAN, MORE PARTICULARLY DESCRIBED AS FOLLOWS. COMMENCING AT THE NORTHWEST CORNER OF LOT F OF THE RECORDED PLAT OF VALLEY JUNCTION, IOWA, WITH SAID NORTHWEST CORNER BEING ON THE LINE BETWEEN THE NORTH QUARTER CORNER AND THE CENTER OF SAID SECTION 15, AND HAVING AN ASSUMED TRUE BEARING SOUTH 0°00' WEST WITH ALL SUBSEQUENT BEARINGS REFERENCED THEREFROM; THENCE SOUTH 87°24' EAST ALONG THE NORTH LINE OF SAID LOT F, A DISTANCE OF 858.3 FEET; THENCE SOUTH 0°00' EAST, A DISTANCE OF 375 FEET; THENCE SOUTH 90°00' EAST, A DISTANCE OF 200 FEET TO THE POINT OF BEGINNING, SAID POINT ALSO BEING THE NORTHEAST CORNER OF PROPERTY DESCRIBED IN DEED DATED AUGUST 31,1953, FROM THE CHICAGO, ROCK ISLAND AND PACIFIC RAILROAD COMPANY TO PENN-DIXIE CEMENT CORPORATION AND AS RECORDED ON PAGE 207, BOOK 2631 IN THE OFFICE OF THE RECORDER OF POLK COUNTY, IOWA; THENCE SOUTH 0°00' EAST A DISTANCE OF 1016.34 FEET; THENCE SOUTH 30°54' WEST, A DISTANCE OF 172.84 FEET TO A POINT OF INTERSECTION WITH A LINE 200 FEET NORTHWESTERLY OF, AS MEASURED AT RIGHT ANGLES TO, AND PARALLEL WITH THE CENTERLINE OF THE MAIN TRACT OF SAID RAILROAD COMPANY; SAID LAST TWO BEARING LINES BEING THE TWO NORTHERLY LINES OF THE EASTERLY BOUNDARIES OF THE PROPERTY DESCRIBED IN SAID DEED DATED AUGUST 31, 1953; THENCE NORTH 47°44' EAST ALONG SAID LINE PARALLEL AND 200 FEET NORTHWESTERLY FROM THE CENTERLINE OF SAID MAIN LINE TRACK, A DISTANCE OF 557.65 FEET TO THE WESTERLY LINE OF ELEVENTH STREET IN THE CITY OF WEST DES MOINES, POLK COUNTY, IOWA; THENCE NORTH 39°46' WEST ALONG THE WESTLINE OF SAID ELEVENTH STREET; A DISTANCE OF 51.7 FEET; THENCE SOUTH 50°14' WEST ALONG SAID WEST LINE OF SAID STREET, A DISTANCE OF 10 FEET; THENCE NORTHERLY ALONG SAID WEST LINE OF SAID STREET, A DISTANCE OF 251.25 FEET ALONG A 316.5 FOOT RADIUS CURVE CONCAVE NORTHEASTERLY AND TANGENT TO THE FOLLOWING COURSE; THENCE NORTH 0°00' EAST ALONG THE SAID WEST LINE OF SAID STREET, A DISTANCE OF 529.87 FEET; THENCE NORTHERLY ALONG SAID WEST LINE OF SAID STREET ON A 256.5 FOOT RADIUS CURVE CONCAVE SOUTHWESTERLY AND

TANGENT TO THE PRECEDING COURSE, A DISTANCE OF 3.2 FEET; THENCE NORTH 90°00' WEST, A DISTANCE OF 197.8 FEET TO THE POINT OF BEGINNING.

AND

COMMENCING AT THE NORTH 1/4 CORNER OF SECTION 15-T78NR25 WEST OF THE 5TH P.M., WEST DES MOINES, POLK COUNTY, IOWA, THENCE S 0°00 E, ALONG THE WEST LINE OF THE N.E. 1/4 OF SAID SECTION 15, 185.15 FEET, TO THE SOUTH RIGHT-OF-WAY LINE OF THE MINNEAPOLIS AND ST. LOUIS RAILROAD, AS II IS PRESENTLY ESTABLISHED, THENCE S 87°26' 1/2" E, ALONG SAID SOUTH RIGHT-OF-WAY LINE, 87.12 FEET. THENCE CONTINUING S 87°26' 1/2" E, ALONG THE SOUTH RIGHT-OF-WAY LINE OF THE MINNEAPOLIS AND ST. LOUIS RAILROAD. AND PARALLEL WITH AND 50.0 FEET NORMALLY DISTANT FROM AND SOUTH OF THE CENTER LINE OF SAID MINNEAPOLIS AND ST. LOUIS RAILROAD, 567.53 FEET, TO THE POINT OF BEGINNING, THENCE CONTINUING S 87°26 1/2' E ALONG SAID SOUTH RIGHT-OF-WAY LINE OF THE MINNEAPOLIS AND ST. LOUIS RAILROAD, 200.2 FEET, THENCE S 0°00' E, PARALLEL TO AND 854.0 FEET EAST OF THE WEST LINE OF THE NE 1/4 OF SAID SECTION 15, 375.0 FEET, THENCE N 90°00 E, 200.0 FEET, THENCE S 0°00' E, PARALLEL WITH AND 1054.0 FEET EAST OF THE WEST LINE OF THE NE 1/4 OF SAID SECTION 15, 1018.8 FEET, THENCE S 30°44' W 173.86 FEET, TO THE NORTHWESTERLY RIGHT-OF-WAY LINE OF THE CHICAGO-ROCK ISLAND AND PACIFIC RAILROAD, AS IT IS PRESENTLY ESTABLISHED, THENCE S 47°42 1/2' W, PARALLEL WITH AND 200.0 FEET NORMALLY DISTANT FROM AND NORTHWESTERLY OF THE CENTER LINE OF THE MAIN LINE TRACK OF THE CHICAGO-ROCK ISLAND PACIFIC RAILROAD, AND ALONG THE NORTHWESTERLY RIGHT-OF-WAY OF SAID CHICAGO-ROCK ISLAND AND PACIFIC RAILROAD 420.63 FEET TO A POINT ON SAID NORTHWESTERLY RIGHT-OF-WAY OF THE CHICAGO-ROCK ISLAND AND PACIFIC RAILROAD, THENCE N 0°00' W, PARALLEL WITH AND 654.0 FEET EAST OF THE WEST LINE OF THE NE 1/4 OF SAID SECTION 15,1834.21 FEET TO THE POINT OF BEGINNING.

ALL BEING AN OFFICIAL PLAT, NOW INCLUDED IN AND FORMING A PART OF THE CITY OF WEST DES MOINES. POLK COUNTY, IOWA (EXCEPT THAT PART PLATTED AS SCHRODER INDUSTRIAL PARK).

DAVENPORT (BUFFALO, IOWA):

CHAIN ONE AND TWO:

PARCEL NO. 1: PART OF THE NORTHEAST QUARTER OF SECTION 23 IN TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING ON THE NORTH LINE OF SAID QUARTER SECTION AT A POINT 15 CHAINS AND 40 LINKS WEST OF THE NORTHEAST CORNER OF SAID NORTHEAST QUARTER; THENCE RUNNING WEST 24 CHAINS AND 60 LINKS TO THE NORTHWEST CORNER OF SAID QUARTER SECTION; THENCE SOUTH 40 CHAINS AND 55 LINKS TO THE NORTH BANK OF THE MISSISSIPPI RIVER; THENCE NORTH 66 DEGREES EAST, 1 CHAIN AND 43 LINKS TO A POINT ON SAID RIVER BANK; THENCE NORTH 84 DEGREES EAST, ON AND ALONG SAID RIVER BANK TO A POINT 24 CHAINS AND 1 LINK DISTANT; THENCE NORTH 37 CHAINS AND 47 LINKS TO THE PLACE OF BEGINNING.

EXCEPTING THEREFROM THE RIGHT OF WAY OF THE CHICAGO, ROCK ISLAND AND PACIFIC RAILWAY COMPANY; AND EXCEPTING PUBLIC HIGHWAYS.

PARCEL NO. 2: THE WEST ONE-HALF OF THE SOUTHEAST QUARTER OF SECTION 4, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M., SCOTT COUNTY, IOWA.

PARCEL NO. 3: LOTS 3 AND 4 OF THE SUBDIVISION OF THE ESTATE OF ELIAS MOORE, DECEASED, IN THE NORTHEAST QUARTER OF SECTION 23, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M. MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING AT A POINT IN THE EAST LINE OF SECTION 23 WHICH IS 8 CHAINS 59 LINKS SOUTH OF THE NORTHEAST CORNER OF SAID SECTION; THENCE RUNNING DUE WEST 15 CHAINS AND 40 LINKS; THENCE RUNNING DUE SOUTH 28 CHAINS AND 88 LINKS TO A STAKE STANDING ON THE BANK OF THE MISSISSIPPI RIVER; THENCE WITH THE MEANDERS OF THE SAID RIVER NORTH 84 DEGREES EAST 12 CHAINS AND 99 LINKS; THENCE WITH THE MEANDERS OF SAID RIVER NORTH 62 DEGREES EAST 2 CHAINS 82 LINKS; MORE OR LESS, TO A EAST LINE OF SAID SECTION; THENCE DUE NORTH ALONG THE EAST LINE OF SAID SECTION 26 CHAINS AND 13 LINKS TO THE PLACE OF BEGINNING, SUBJECT TO RAILROAD RIGHTS-OF WAY AND TO PUBLIC HIGHWAYS.

PARCEL NO. 4: THE EAST HALF OF THE SOUTHWEST QUARTER OF SECTION 14, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M. (DOES NOT INCLUDE PARCEL NO. 5 TRACT.)

PARCEL NO. 6: ALL THAT PART OF THE LAND INCLUDED IN THE PLAT OF THE ESTATE OF LEROY DODGE RECORDED IN PARTITION SUIT NO. 13437 IN THE DISTRICT COURT OF IOWA IN AND FOR SCOTT COUNTY, SAID PLAT INCLUDING LAND SITUATED IN SECTIONS 14, 15, 22 AND 23, TOWNSHIP 77 NORTH, RANGE 2 EAST, DESCRIBED AS FOLLOWS:

ALL OF LOT 1, ACCORDING TO SAID PLAT,

ALL OF LOT 2, ACCORDING TO SAID PLAT,

ALL OF LOT 3, ACCORDING TO SAID PLAT,

ALL OF THAT PART OF THE LOT 7, ACCORDING TO SAID PLAT, WHICH LIES SOUTH OF THE SECTION LINE BETWEEN SAID SECTIONS 15 AND 22,

ALL OF LOT 8, ACCORDING TO SAID PLAT, EXCEPT (A) THAT PART CONVEYED BY FRANK L. DODGE TO DAVENPORT PAVING BRICK & TILE COMPANY BY DEED RECORDED IN BOOK 57 OF LAND DEEDS, AT PAGE 490, (B) THAT PART CONVEYED BY FRANK L. DODGE TO HORACE H. CASS BY DEED RECORDED IN BOOK 48 OF LAND DEEDS, AT PAGE 283, AND IN BOOK 49 OF LAND DEEDS, AT PAGE 288, (C) THAT PART CONVEYED BY FRANK L. DODGE TO DORMAN & MOOREHEAD BY DEED RECORDED IN BOOK 52 OF LAND DEEDS, AT PAGE 83, (D) THAT PART THERETOFORE CONVEYED BY FRANK L. DODGE TO THE CHICAGO, ROCK ISLAND & PACIFIC RAILWAY COMPANY FOR STATION GROUNDS, (E) THAT PART CONVEYED BY DEWEY PORTLAND CEMENT COMPANY TO BUFFALO, IOWA, INDEPENDENT SCHOOL DISTRICT NO. 1 BY DEED RECORDED IN BOOK 90 OF LAND DEEDS, AT PAGE 45, AND (F) THAT PART CONVEYED BY DEWEY PORTLAND CEMENT COMPANY TO IOWA-ILLINOIS GAS AND ELECTRIC COMPANY BY DEED RECORDED IN BOOK 243 OF DEEDS, AT PAGE 238.

ALL OF LOT 9, ACCORDING TO SAID PLAT.

EXCEPTING THEREFROM THAT PORTION THEREOF CONVEYED TO THE CITY OF BUFFALO, IOWA, BY QUIT CLAIM DEED DATED JULY 22, 1980 AND RECORDED AS DOCUMENT #7502-81 IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

EXCEPTING THEREFROM THAT PORTION THEREOF CONVEYED TO THE STATE OF IOWA BY DEED DATED AUGUST 3, 1982 AND RECORDED AS DOCUMENT #12944-82 IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

PARCEL NO. 7: THAT 8 ACRE PORTION OF THE BED OF THE MISSISSIPPI RIVER WHICH LIES ADJACENT TO THE IOWA BANK OF SAID RIVER AND ADJACENT TO THE SOUTHERLY LINE OF GOVERNMENT LOTS TWO (2) AND THREE (3) OF SECTION TWENTY-THREE (23) OF TOWNSHIP SEVENTY-SEVEN (77) NORTH, RANGE TWO (2) EAST OF THE FIFTH PRINCIPAL MERIDIAN, MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING AT THE NORTHEAST CORNER OF SAID SECTION THENCE SOUTH 1740.10 FEET ALONG THE EAST LINE OF SAID SECTION: THENCE SOUTH 32 DEGREES 40 MINUTES WEST 1162.25 FEET TO THE NORTHEAST CORNER OF THE PRESENT SEA-WALL; THENCE ALONG THE FACE OF SAID SEA-WALL AND ALONG THE IOWA BANK OF SAID RIVER, SOUTH 33 DEGREES 48 MINUTES WEST 51.20 FEET; THENCE SOUTH 82 DEGREES 6 MINUTES WEST 455.70 FEET; THENCE SOUTH 81 DEGREES 39 MINUTES WEST 419.70 FEET TO THE WESTERLY END OF SAID SEA-WALL; THENCE SOUTH 85 DEGREES 16 1/2 MINUTES WEST 310 FEET TO THE POINT OF BEGINNING; THENCE SOUTH 85 DEGREES 16 1/2 MINUTES WEST 1100 FEET TO THE EASTERLY BANK OF A PRESENT CREEK OUTLET AT A POINT APPROXIMATELY 2930 FEET WEST OF AND 3000 FEET SOUTH OF THE NORTHEAST CORNER OF SAID SECTION; THENCE NORTHERLY ALONG SAID CREEK OUTLET BANK TO THE PRESENT IOWA SHORE LINE OF SAID RIVER AT ELEVATION OF 547 FEET ABOVE MEAN SEA-LEVEL; THENCE EASTERLY ALONG SAID SHORE LINE TO A POINT 1860 FEET WEST OF AND 2550 FEET SOUTH OF THE NORTHEAST CORNER OF SAID SECTION; THENCE SOUTHERLY 330 FEET ALONG THE WEST LINE OF THE

PREMISES OWNED BY DEWEY PORTLAND CEMENT COMPANY TO THE POINT OF BEGINNING.

#### EXCEPTIONS TO ALL THE ABOVE PARCELS

EXCEPT THAT PORTION DEEDED TO THE STATE OF IOWA BY DEED DATED AUGUST 31, 1982 AND RECORDED AS DOCUMENT NO. 12944-82 IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA, AND EXCEPTING THOSE LANDS CONDEMNED BY THE UNITED STATES OF AMERICA UNDER ORDER DATED AUGUST 11, 1939 AND RECORDED IN THE OFFICE OF THE SCOTT COUNTY, IOWA RECORDER AT BOOK 82 LAND DEEDS, PAGE 264 AND EXCEPTING THE TRACT CONVEYED TO THE CITY OF BUFFALO, IOWA BY DEED DATED JULY 22, 1980 AND RECORDED IN THE OFFICE OF THE SCOTT COUNTY, IOWA RECORDER AS DOCUMENT NO. 7502-81.

PARCELS NO. 10 AND 11: THE NORTHWEST QUARTER OF THE SOUTHWEST QUARTER OF SECTION 14, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M. ALSO DESCRIBED AS LOT 4 IN THE PARTITION OF THE ESTATE OF LEROY DODGE.

ALSO PART OF THE SOUTHEAST QUARTER OF SECTION 15, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5<sup>TH</sup> P.M., DESCRIBED AS COMMENCING AT THE NORTHEAST CORNER OF THE SOUTHEAST QUARTER OF SAID SECTION 15; THENCE WEST ON THE NORTH LINE OF SAID SOUTHEAST QUARTER OF SECTION 15, 15 CHAINS; THENCE SOUTH ON THE EAST LINE OF LOT 6, 20 CHAINS; THENCE EAST ON THE NORTH LINE OF LOT 1, 15 CHAINS; THENCE NORTH ON THE WEST LINE OF LOT 4, 20 CHAINS TO THE PLACE OF BEGINNING, WHICH REAL ESTATE IS ALSO DESCRIBED AS LOT 5 IN THE PARTITION OF THE ESTATE OF LEROY DODGE, DECEASED.

THE ABOVE DESCRIBED TRACTS OF REAL ESTATE ARE PARTICULARLY DESCRIBED BY SURVEY AS FOLLOWS:

BEGINNING AT THE NORTHEAST CORNER OF THE SOUTHEAST ¼ OF SECTION 15, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH PRINCIPAL MERIDIAN SAID POINT BEING ALSO THE NORTHWEST CORNER OF THE SOUTHWEST ¼ OF SECTION 14, TOWNSHIP AND RANGE AFORESAID, THENCE NORTH 89 DEGREES 52 MINUTES 14 SECONDS EAST ALONG THE NORTH LINE OF THE SAID SOUTHWEST

<sup>1</sup>⁄<sub>4</sub> OF SECTION 14 A DISTANCE OF 1331.0 FEET; THENCE SOUTH 0 DEGREES 42 MINUTES 49 SECONDS WEST 1331.34 FEET; THENCE NORTH 89 DEGREES 52 MINUTES 41 SECONDS WEST 2325.32 FEET TO THE SOUTHEAST CORNER OF LOT 44 DEVIL'S CREEK ESTATES ADDITION; THENCE NORTH 0 DEGREES 37 MINUTES 00 SECONDS EAST ALONG THE EAST LINE OF SAID DEVIL'S CREEK ESTATES ADDITION A DISTANCE OF 1325.43 FEET; THENCE SOUTH 89 DEGREES 52 MINUTES 53 SECONDS EAST 996.64 FEET TO THE PLACE OF BEGINNING. SITUATED IN BUFFALO TOWNSHIP, SCOTT COUNTY, IOWA.

#### CHAIN THREE:

PARCEL 12

THE NORTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 14; THE NORTH 16 ACRES OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 14; THE EAST 20 ACRES OF THE NORTHEAST QUARTER OF THE NORTHEAST QUARTER OF SECTION 15; EXCEPT THOSE PORTIONS THERE CONVEYED BY DOCUMENT NUMBERS 13993-82 AND 18202 83, RECORDS OF THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

ALSO, THE NORTH HALF OF THE SOUTHEAST QUARTER OF THE NORTHEAST QUARTER OF SECTION 15 EXCEPT THAT PART DESCRIBED AS COMMENCING AT A POINT ON SECTION LINE BETWEEN SECTIONS 14 AND 15; THENCE NORTH 20 FEET FROM CENTER LINE OF SOUTHEAST QUARTER OF THE NORTHEAST QUARTER OF SECTION 15; THENCE WEST 73 RODS, THENCE SOUTH 20 FEET; THENCE EAST 73 RODS TO THE PLACE OF BEGINNING, AND ALSO EXCEPTING THEREFROM THAT PORTION SOLD ON CONTRACT RECORDED AS DOCUMENT NUMBER 9033 75, RECORDS OF THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA, ALL IN TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH PRINCIPAL MERIDIAN.

CHAIN FOUR:

PARCEL 13

THE SOUTH 16 ACRES OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 14, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M. THE NORTH 8 ACRES OF THE SOUTH 24 ACRES, BEING LOT THREE OF THE SOUTHWEST QUARTER OF THE NORTHWEST QUARTER OF SECTION 14, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M.

THE SOUTH 20 ACRES OF THE SOUTHEAST QUARTER OF THE NORTHEAST QUARTER OF SECTION 15, TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH P.M., EXCEPTING THEREFROM THE LAND INCLUDED IN LOTS 15 AND 16 IN BUFFALO HEIGHTS, AS APPEARS FROM THE PLAT OF SAID SUBDIVISION RECORDED IN BOOK 63 OF MISCELLANEOUS RECORDS, ON PAGE 291, IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

ALSO, A STRIP OF LAND COMMENCING AT THE NORTHWEST CORNER OF LAST TRACT ABOVE, THENCE WEST 73 RODS, NORTH 20 FEET, EAST 73 RODS, AND SOUTH 20 FEET TO THE PLACE OF BEGINNING.

EXCEPT THAT PORTION OF THE ABOVE DESCRIBED REAL ESTATE THAT WAS CONVEYED TO ALBERT VINER AND WINONA B. VINER BY THE QUIT CLAIM DEED DATED JANUARY 18, 1973, AND RECORDED AS DOC. #963-73 IN THE OFFICE OF THE RECORDER OF SCOTT COUNTY, IOWA.

#### CHAIN 5:

PARCEL 14

ALL THAT PORTION OF THE LAND INCLUDED IN THE PLAT OF THE ESTATE OF LEROY DODGE, RECORDED IN PARTITION SUIT NO 13437 IN THE DISTRICT COURT OF IOWA, AND SCOTT COUNTY, SAID PLAT INCLUDING LAND SITUATED IN SECTIONS 14, 15, 22 & 23 OF TOWNSHIP 77 NORTH, RANGE 2 EAST OF THE 5TH PRINCIPAL MERIDIAN SCOTT COUNTY, IOWA, LYING SOUTH OF THE SOUTHERLY RIGHT-OF-WAY LINE OF IOWA STATE HIGHWAY 22 AND NORTH OF THE ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER, MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING AS A POINT OF REFERENCE AT THE NORTHEAST CORNER OF SECTION 23, TOWNSHIP 77 NORTH, RANGE 2 EAST;

THENCE SOUTH 00°1'51" WEST 1139.58 FEET ALONG THE EAST LINE OF THE NORTHEAST QUARTER OF SAID SECTION 23 TO A POINT ON THE SOUTHERLY RIGHT-OF-WAY LINE OF THE CHICAGO, ROCK ISLAND AND PACIFIC RAILROAD SAID RIGHT-OF-WAY LINE BEING 50 FEET IN PERPENDICULAR DISTANCE SOUTHEASTERLY FROM THE CENTERLINE OF THE WEST-BOUND MAIN LINE (NORTHERLY OF TWO) TRACK (FOR PURPOSES OF THIS DESCRIPTION, THE SAID EAST LINE OF THE NORTHEAST QUARTER OF SECTION 23 IS ASSUMED TO BEAR SOUTH 00°1'51" WEST);

THENCE SOUTH 68° 24''17" WEST 3916.36 FEET ALONG THE SAID SOUTHERLY RIGHT-OF-WAY LINE OF THE CHICAGO, ROCK ISLAND AND PACIFIC RAILROAD PARALLEL TO THE CENTERLINE OF THE SAID WEST-BOUND MAIN LINE TRACK, TO A POINT OF TANGENCY OF THE SAID RAILROAD RIGHT-OF-WAY LINE;

THENCE SOUTHWESTERLY 799.65 FEET ALONG THE SAID SOUTHERLY RIGHT-OF- WAY LINE OF THE CHICAGO, ROCK ISLAND AND PACIFIC RAILROAD ALONG A

5799.58 FEET RADIUS CURVE, CONCAVE NORTHWESTERLY, PARALLEL TO THE CENTERLINE OF THE SAID WEST-BOUND MAIN LINE TRACK TO THE POINT OF BEGINNING (THE CHORD OF SAID CURVE BEARS SOUTH 77° 22' 03" WEST 79.03 FEET);

THENCE SOUTH 61° 13'53" EAST 307.06 FEET TO A POINT AT THE ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER;

THENCE ALONG THE FOLLOWING DESCRIBED MEANDER OF THE ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER;

NORTH 87° 50'58" WEST 418.37 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 80° 10" 32" WEST 325.68 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 76° 47' 55" WEST 293.01 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 6° 40' 17" WEST 351.51 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 4° 36'47" WEST 74.21 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 36° 24'29" WEST 191.26 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 6° 56'22" WEST 250.63 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE SOUTH 6° 24' 17" WEST 245.81 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE NORTH 88° 05'04" WEST 276.83 FEET ALONG THE SAID ORDINARY HIGH WATER LINE OF THE MISSISSIPPI RIVER TO A POINT;

THENCE NORTH 88° 51' 27" WEST 254.28 FEET ALONG THE SAID ORDINARY HIGH WATER POINT OF THE MISSISSIPPI RIVER TO A POINT;

THENCE NORTH 88° 06' 32" WEST 422.12 FEET ALONG THE SAID ORDINARY HIGH WATER POINT OF THE MISSISSIPPI RIVER TO A POINT.

#### SPECIAL WARRANTY DEEL

### KNOW ALL MEN BY THESE PRESENTS:

15.00 That MARTIN MARIETTA CORPORATION, a corporation organized and existing under the laws of the State of Maryland, in the consideration of the sum of one dollar and other valuable consideration in band paid does hereby CONVEY unto Davenport Cement Company, 35 TSLIA

The following described real estate situated in Scott County, Iowa:

Parcel No. 11 Part of the Northeast Quarter of Section 23 in Township 77 North, Range 2 Bast of the 5th P.M., more particularly described as follows:

Commencing on the North line of said quarter section at a point 15 chains and 40 links West of the Northeast corner of said Northeast Quarter; thence running West 24 chains and 60 links to the Northwest corner of said quarter section; thence South 40 chains and 55 links to the North bank of the Mississippi River; thence North 66 degrees East, 1 chain and 43 links to a point on said river bank; thence North 84 degrees East, on and along said river bank to a point 24 chains and 1 link distant; thence North 37 chains and 47 links to the place of beginning.

Excepting therefrom the right of way of The Chicago, Rock Island and Pacific Railway Company; and excepting public highways.

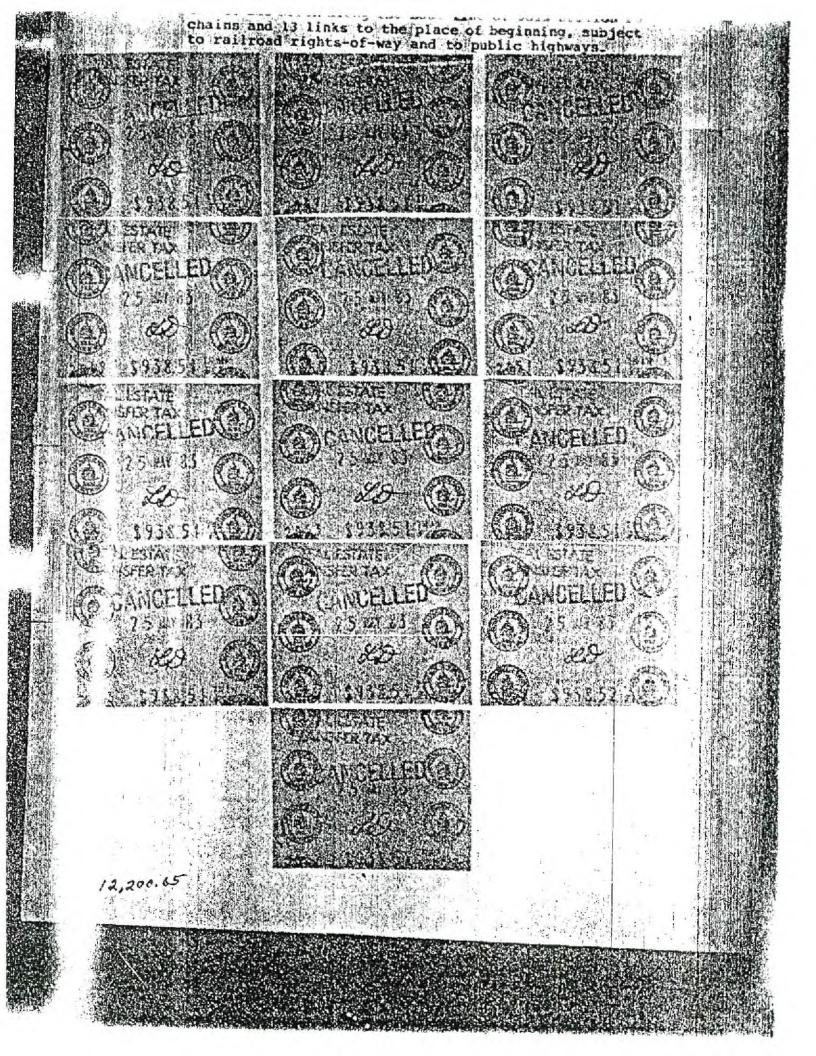
Parcel No. 2: The West one-half of the Southeast Quarter of Section 14, Township 77 North, Range 2 East of the 5th P.M., Scott County, Iowa:

2.5 1 1 4

Parcel No. 3: Lots 3 and 4 of the subdivision of the Estate of Elias Moore, deceased, in the Northeast Quarter of Section 23, Township 77 North, Range 2 East of the 5th P.M., more particularly described as follows:

Commencing at a point in the East line of Section 23 which is 8 chains 59 links South of the Northeast corner of said section; thence running due West 15 chains and 40 links; thence running due South 28 chains and 88 links to a stake standing on the bank of the Hississippi River; thence with the meanders of the said river worth 84 degrees East 12 chains and 99 links; theace with the meanders of said river North 62 degrees East 2 chains 82 links; more or less, to the East line of said section; thence due North along the East line of said Section 26 chains and 13 links to the place of beginning, subject to railroad rights-of-way and to public highways.

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Parcel Nor 4. The East Half of the Southwest Quarter of Section 14. Township 77 North, Range 2 East of the 5th 2 P.N. (This Deed does not contain a Parcel 5 tract.)

Parcel No. 6. All that part of the land included in the plat of the Estate of LeRoy Dodge recorded in partition suit No. (13437 in the District Court of Iowa in and for Scott County, said plat including land situated in Sections 14, 15, 22 and 23, Township 77 North, Range 2 East, described as follows:

All of Lot 1. according to said plat.

All of Lot 2, according to said plat,

All of Lot 3, according to said plat,

All that part of the Lot 7; according to said Plat, which lies south of the section line between said Sections 15 and 22,

All of Lot 8, according to said plat, <u>EXCEPT</u> (a) that part conveyed by Frank L. Dodge to Davenport Paving Brick & Tile Company by deed recorded in Book 57 of Land Deeds, at page 490, (b) that part conveyed by Frank L. Dodge to Horace H. Cass by deed recorded in Book 48 of Land Deeds, at page 283, and in Book 49 of Land Deeds, at page 288, (c) that part conveyed by Frank L. Dodge to Dorman & Moorehead by deed recorded in Book 52 of Land Deeds, at page 83, (d) that part heretofore conveyed by Frank L. Dodge to The Chicago, Rock Island & Pacific Railway Company for station grounds, (e) that part conveyed by Dewey Portland Cement Company to Buffalo, Iowa, Independent School District No. 1 by deed recorded in Book 90 of Land Deeds, at page 45, and (f) that part conveyed by Dewey Portland Cement Company to Iowa-Illinois Gas and Electric Company by deed recorded in Book 243 of Deeds, at page 238.

All of Lot 9, according to said plat.

18 A

Excepting therefrom that portion thereof conveyed to the City of Buffalo, Iowa, by Quit Claim Deed dated July 22, 1980 and, recorded as Document #7502-81 in the office of the Recorder of Scott County, Iowa.

Excepting therefrom that portion thereof conveyed to the State of Towa by Deed dated August 3, 1982 and recorded as Document #12944-82 In the office of the Recorder of Scott County, Iowa.

Parcel No. 7. That 6 acre portion of the bed of the Mississippi River which lies adjacent to the Iowa Bank of said river and adjacent to the Southerly line of Government Lots Two (2) and Three (3) of Section Twenty-Three (23) of Township Seventy-seven (77) North, Range Two (2) East of the Fifth Principal Meridian, more particularly described as follows:

Commencing at the Northeast corner of said Section; thence south 1740.10 feet along the East line of said section; thence south 32 degrees 40 minutes west 1162.25 feet to the northeast corner of the present sea-wall; thence along the face of said sea-wall and along the Iowa

Bar Anna Andrew Changes and In the Like

12.11

Further subject to all other existing leases and rights of tenants in possession, existing railroad rights of way and depot grounds, easements, restrictions, reservations, or agreements of record, the rights of the public and the State of Iowa in roads and highways through the same, taxes and

1 garage

Further subject to the terms, provisions, covenants, conditions and restrictions contained in and rights and obligations created by a Lease Agreement dated May 21, 1971 and filed for record February 8, 1978 in the Office of the Scott County, Iowa Recorder as Document Number 2311-78 by and between Martin Marietta Corporation, Linwood Stone Products Company, an Iowa Corporation and Schwerman Trucking Company a Wisconsin corporation; and

Subject to a certain Grant of Easement to the Town of Buffalo, Iowa, dated December 1, 1972 and filed for record in the Office of the Recorder of Scott County, Iowa, as Document Number 1100-73 on January 24, 1973 and a certain Lease Agreement between the Town of Buffalo, Iowa, as lessor, and Marietta Facilities, Inc., a Delaware Corporation as lessee dated December 1, 1972 and recorded in the Office of the Recorder of Scott County, Iowa, as Document No. 1101-73 on January 24, 1973 and a certain Indenture of Trust dated December 1, 1972 between the Town of Buffalo, Iowa, and Trustee which Indenture of Trust is dated December 1, 1972 and is recorded in the Office of the Scott County, Iowa Recorder as Document No. 1102-73 on January 24, 1973; and

ALL OF THE FOREGOING PARTICULARLY DESCRIBED PARCELS OF REAL ESTATE ARE CONVEYED SUBJECT TO THE FOLLOWING:

Except that portion deeded to the State of Iowa by Deed dated August 31, 1982 and recorded as Document No. 12944-82 in the office of the Recorder of Scott County, Iowa, and excepting those lands condemned by the United States of America under order dated August 11, 1939 and recorded in the office of the Scott County, Iowa, Recorder at Book 82 Land Deeds, Page 264 and excepting the tract conveyed to the City of Buffalo, Iowa by deed dated July 22, 1960 and recorded in the office of the Scott County, Iowa Recorder as Document No. 7502-81.

### EXCEPTIONS TO ALL OF THE ABOVE PARCELS

51.20 feet; thence South 33 degrees 48 minutes West 455.70 feet; thence South 81 degrees 6 minutes West 419.70 feet; to the Westerly end of said sea-wall; thence South 85 degrees 16.1/2 minutes West 310 feet to the point of beginning; thence South 85 degrees 16.1/2 minutes West 1100 feet to the Easterly bank of a present creek outlet at a point approximately 2930 feet West of and 3000 feet South of the Northeast corner of said section; thence Northerly along said creek outlet bank to the present lowa shore line of said river at elevation of 547 feet above mean sea-level; thence Easterly along said shore line to a point 1860 feet West of and 2550 feet South of the Northeast corner of said section; thence Southerly 330 feet along the West line of the premises owned by Dewey Portland Cement Company to the point of beginning. assessments; general and special, not now due and payable, and a certain boundary adjustment Agreement between Grantor and the State of lows recorder on October 4, 1982 in the office of the Recorder of Scott County. Lows as Document No. 12345-82, and TOGETHER NITH any easements appurchant or of record for the benefit of the real estate herein conveyed; and further subject to any rights or claims of the United States of America in and its the subject premises acquired pursuant to a certain order vesting title entered in the United States District Court for the Southern District of Iowa, Davenport Division, dated August 11, 1939 and filed in the office of the Recorder of Scott County, Iowa on August 18, 1939 at Book 82 Land Deeds 264; and

Further subject to the rights of the United States of America, the State of Iowa, the City of Buffalo, Iowa, and the Public in and to that part of the subject premises falling in the bed of the Mississippi River; also rights of property owners in and to the free and unobstructed flow of the waters of said river.

THE GRANTOR HEREIN ALSO CONVEYS TO THE GRANTEE HEREIN THE FOLLOWING ADDITIONAL PARCELS OF REAL ESTAVE SITUATED IN SCOTTICOUNTY, IOWA: Parcel No. 8: That part of the Southwest Quarter of the Southeast Quarter of Section 17, Township 77 North, Range 2 East of the 5th P.M., which lies West of the highway running through said quarter section as the same was located and established by Easement dated November 3, 1926 and recorded in Book 77 of Land Deeds at Page 235, records of the office of the Recorder of Scott County, Iowa.

Except that portion thereof included in the tract conveyed by Jacob Fridley and wife to Christ Rautz by Deeds dated June 14, 1862 and November 22, 1864 and recorded in Book 32 of Land Deeds, Page 150 and 159, respectively; and excepting the piece one rod in width conveyed by Jacob Fridley and wife to Conrad Appel by Deed dated March 12, 1872 and recorded in Book 43 of Land Deeds at Page 13, records of the office of the Recorder of Scott County; Iowa;

Also excepting that portion thereof conveyed to Scott County, Iowa by Quit Claim Deed dated April 29, 1964 and recorded in Book 278 of Deeds on Page 571 in the office of the Recorder of Scott County, Iowa.

Parcel No. 91 All of the Southeast Quarter of the Southwest Quarter in Section 17. Township 77 North, Range 2 East of the 5th P.M., excepting 3 acres, more or less, lying and being situated Northeast of the Blue Grass Road, which was conveyed to Stephen A. Collins by deeds recorded in Book 53 of Land Deeds, Page 626, and in Book 66 of Land Deeds, Page 601 in the office of the Recorder of Scott County, Iowa, and also excepting 3 acres, more of less, which was conveyed to Jack 0. Phillips, et al, by deed recorded in Book 87 of Land Deeds, Page 352 in the office of the Recorder of Scott County, Iowa

Except that portion thereof conveyed to Scott County, Iowa, by Quit Claim Deed dated April 29, 1964 and recorded in Book 278 of Deeds on Page 571 in the office of the Recorderiof Scott County, Iowa, Parcels no. (10 and 11) The Northwest Quarter of the Southwest Quarter of Section 14, township 77 North, Range 2 East of the 5th P.N., Also described as Lot 4

In the partition of the Estate of LeRoy Dodge. Also part of the Southeast Quarter of Section 15. Township 77 North, Range 2 East of the 5th P.N., described as commencing at the Northeast corner of the Southeast Quarter of said Section 15; thence West on the North line of said Southeast Quarter of Section 15, 15 chains; thence South on the East line of Lot 6, 20 chains; thence East on the North line of Lot 1, 15 chains; thence East on the North line of Lot 4, 20 chains; thence North on the West line of Lot 4, 20 chains to the place of beginning, which real estate is also described as Lot 5 in the partition of the Estate of LeRoy Dodge, deceased.

The above described tracts of real estate are particularly described by survey as follows:

Beginning at the Northeast corner of the Southeast 1/4 of Section 15, Township 77 North, Range 2 East of the 5th Principal Meridian said point being also the Northwest corner of the Southwest 1/4 of Section 14, Township and Range aforesaid, thence North 89 degrees 52 minutes 14 seconds East along the North line of the said Southwest 1/4 of Section 14 a distance of 1331.0 feet; thence South 0 degrees 42 minutes 49 east Corner of Lot 44 Devil's Creek Estates Addition: thence North 0 degrees 37 minutes 00 seconds East along the Bast line of said Devil's Creek Estates Addition a distance of 1325.43 feet; thence South 83 degrees 52 minutes 53 seconds East 996.64 feet to the place of beginning. Situated in Buffalo Township, Scott County, Iowa.

ALL OF THE FOREGOING PARTICULARLY DESCRIBED PARCELS OF REAL ESTATE ARE CONVEYED SUBJECT TO THE FOLLOWING:

Subject to existing leases and rights of tenants in possession, easements, restrictions, reservations, or agreements of record, the fights of the public and the State of Iowa in roads and highways through the same, taxes and assessments, general and special, not now due and payable, and TOGETHER WITH any easements appurtenant or of record for the benefit of the real estate herein conveyed.

Martin Marletta Corporation hereby convenants with said grantee, and successors in interest, to Warrant and Defend the said premises against the lawful claims of all persons claiming by, through or under it, except as may be above stated

IN WITNESS WHEREOF said corporation has caused this instrumentito be duly executed this \_\_\_\_\_\_ day of May, 1983.

MARTIN MARIETTA CORPORATION

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State of state of the seal of said corporation; that said instrument was signed, and sealed on behalf of said corporation by said corporation to seal arfived COUNTY, ment was signed and sealed on behalf of said corporation by authority of its Board of Directors; and that the said  $\frac{P_{\rm b}}{P_{\rm b}} = \frac{M}{2} \frac{P_{\rm c}}{P_{\rm b}}$  and  $\frac{Ta_{\rm c}}{Ta_{\rm c}} = \frac{1}{2} \frac{E_{\rm c}}{E_{\rm c}} \frac{1}{E_{\rm c}}$ as such officers, acknowledged the execution of said instrument to be the voluntary act and deed of said corporation, by it and by them voluntarily executed. Edward S. Rosenthal Notary Public in and for said State EDWARD S. ROSCHTHAL Hotary Public, State of New York No. 31-771304 Ocseffed In New York County Completion Expires Namiti 30, 1963

**APPENDIX B** 

**CKD Analytical Results** 



November 02, 2021

Lindsay E. James Blackstone Environmental, Inc. 16200 Foster Street Overland Park, KS 66085

RE: Project: Cont. 3185 Pace Project No.: 60384336

Dear Lindsay James:

Enclosed are the analytical results for sample(s) received by the laboratory on October 09, 2021. The results relate only to the samples included in this report. Results reported herein conform to the applicable TNI/NELAC Standards and the laboratory's Quality Manual, where applicable, unless otherwise noted in the body of the report.

The test results provided in this final report were generated by each of the following laboratories within the Pace Network: • Pace Analytical Services - Kansas City

If you have any questions concerning this report, please feel free to contact me.

Sincerely,

AAA

Hank Kapka hank.kapka@pacelabs.com (913)599-5665 PM Lab Management

Enclosures





Pace Analytical Services, LLC 9608 Loiret Blvd. Lenexa, KS 66219 (913)599-5665

#### CERTIFICATIONS

Project: Cont. 3185 Pace Project No.: 60384336

#### **Pace Analytical Services Kansas**

9608 Loiret Boulevard, Lenexa, KS 66219 Missouri Inorganic Drinking Water Certification #: 10090 Arkansas Drinking Water Arkansas Certification #: 20-020-0 Arkansas Drinking Water Illinois Certification #: 2000302021-3 Iowa Certification #: 118 Kansas/NELAP Certification #: E-10116 Louisiana Certification #: 03055 Nevada Certification #: KS000212020-2 Oklahoma Certification #: 9205/9935 Florida: Cert E871149 SEKS WET Texas Certification #: T104704407-19-12 Utah Certification #: KS000212019-9 Illinois Certification #: 004592 Kansas Field Laboratory Accreditation: # E-92587 Missouri SEKS Micro Certification: 10070



#### SAMPLE SUMMARY

Project: Pace Project No.:	Cont. 3185 : 60384336			
Lab ID	Sample ID	Matrix	Date Collected	Date Received
60382604002	CKD 1	Water	10/08/21 11:53	10/09/21 08:45



#### SAMPLE ANALYTE COUNT

Project:Cont. 3185Pace Project No.:60384336

Lab ID	Sample ID	Method	Analysts	Analytes Reported	Laboratory
60382604002	CKD 1	EPA 6010	JLH	12	PASI-K
		EPA 7470	VRB	1	PASI-K

PASI-K = Pace Analytical Services - Kansas City



#### ANALYTICAL RESULTS

Project: Pace Project No.:	Cont. 3185 60384336								
Sample: CKD 1		Lab ID: 603	82604002	Collected: 10/08/2	1 11:53	B Received: 10	)/09/21 08:45 M	latrix: Water	
Paran	neters	Results	Units	Report Limit	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP, TCI	_P	Analytical Meth	od: EPA 6	010 Preparation Meth	nod: EP	A 3010			
		Leachate Meth	od/Date: E	PA 1311; 10/21/21 18	:21 Ini	tial pH: 11.43; Fin	al pH: 11.67		
		Pace Analytica	I Services	Kansas City					
Aluminum		2710	ug/L	2000	1	10/22/21 12:07	10/25/21 11:03	7429-90-5	
Arsenic		ND	mg/L	0.50	1	10/22/21 12:07	10/25/21 11:03	7440-38-2	
Barium		ND	mg/L	2.5	1	10/22/21 12:07	10/25/21 11:03	7440-39-3	
Cadmium		ND	mg/L	0.050	1	10/22/21 12:07	10/25/21 11:03	7440-43-9	
Calcium		830000	ug/L	50000	1	10/22/21 12:07	10/25/21 11:03	7440-70-2	
Chromium		ND	mg/L	0.10	1	10/22/21 12:07	10/25/21 11:03	7440-47-3	
Iron		ND	ug/L	1000	1	10/22/21 12:07	10/25/21 11:03	7439-89-6	
Lead		ND	mg/L	0.50	1	10/22/21 12:07	10/25/21 11:03	7439-92-1	
Magnesium		ND	ug/L	50000	1	10/22/21 12:07	10/25/21 11:03	7439-95-4	
Potassium		68000	ug/L	50000	1	10/22/21 12:07	10/25/21 11:03	7440-09-7	
Selenium		ND	mg/L	0.50	1	10/22/21 12:07	10/25/21 11:03	7782-49-2	
Silver		ND	mg/L	0.10	1	10/22/21 12:07	10/25/21 11:03	7440-22-4	
7470 Mercury, TCL	.P	Analytical Meth	od: EPA 74	470 Preparation Meth	nod: EP	A 7470			
		Leachate Meth	od/Date: E	PA 1311; 10/21/21 18	:21 Ini	tial pH: 11.43; Fin	al pH: 11.67		
		Pace Analytica					-		
Mercury		ND	mg/L	0.0020	1	10/23/21 15:17	10/25/21 09:38	7439-97-6	



#### **QUALITY CONTROL DATA**

- <b>)</b>	Cont. 3185 60384336											
QC Batch:	751580		Anali	ysis Metho	d. E	EPA 7470						
QC Batch Method:	EPA 7470					-						
QC Batch Method:	EPA 7470			ysis Desci	•	7470 Mercu			- C:+ .			
Associated Lab Sam	ples: 603826040	002	Labo	ratory:	F	Pace Analyt	ical Service	es - Kansa	s City			
METHOD BLANK:	3007464			Matrix: V	Vater							
Associated Lab Sam	ples: 603826040	002										
			Blar	nk	Reporting							
Param	eter	Units	Res	ult	Limit	Analy	yzed	Qualifier	s			
Mercury		mg/L		ND	0.0020	0 10/25/2	1 09:34					
LABORATORY CON	TROL SAMPLE:	3009446										
			Spike	L	CS	LCS	% R	ес				
Param	eter	Units	Conc.	Re	sult	% Rec	Limi	ts (	Qualifiers			
Mercury	·	mg/L	0.01	5	0.015	9	9 8	30-120				
MATRIX SPIKE & M	ATRIX SPIKE DUP	_ICATE: 3009	447		3009448							
			MS	MSD								
_		60383151001	Spike	Spike	MS	MSD	MS	MSD	% Rec		Max	<b>.</b> .
	Units	Result	Conc.	Conc.	Result	Result	% Rec	% Rec	Limits	RPD	RPD	Qual
Parameter					· ·							

Results presented on this page are in the units indicated by the "Units" column except where an alternate unit is presented to the right of the result.



Cont. 3185

Project:

#### **QUALITY CONTROL DATA**

QC Batch: 7513	373		Analy	sis Method	l: El	PA 6010						
QC Batch Method: EPA	3010		Analy	sis Descrip	otion: 60	010 MET T	CLP					
				ratory:		ace Analvti	ical Servic	es - Kansa	s Citv			
Associated Lab Samples:	6038260400	)2										
METHOD BLANK: 30074	64			Matrix: Wa	ater							
Associated Lab Samples:	6038260400	)2										
			Blan	k F	Reporting							
Parameter		Units	Resu	ult	Limit	Analy	zed	Qualifier	S			
Arsenic		mg/L		ND	0.50	10/25/21	10:58					
Barium		mg/L		ND	2.5	10/25/21	10:58					
Cadmium		mg/L		ND	0.050	10/25/21	10:58					
Chromium		mg/L		ND	0.10							
Lead		mg/L		ND	0.50							
Selenium		mg/L		ND	0.50							
Silver		mg/L		ND	0.10	10/25/21	10:58					
	SAMPLE: 3	8008359	Spike	LC		LCS	% R					
LABORATORY CONTROL Parameter	SAMPLE: 3	3008359 Units	Spike Conc.	LC Res		LCS % Rec	% R Lim		Qualifiers			
LABORATORY CONTROL Parameter Arsenic	SAMPLE: 3		Conc.		ult	% Rec 101	Lim I		Qualifiers			
Parameter Arsenic Barium	SAMPLE: 3	Units mg/L mg/L	Conc. 10	 0 0	ult 10.1 10.0	% Rec 101 100	Lim	its 80-120 80-120	Qualifiers			
Parameter Arsenic Barium Cadmium	SAMPLE: 3	Units mg/L mg/L mg/L	Conc. 10 10 10	Res 0 0 0 0	ult 10.1 10.0 10.2	% Rec 101 100 102	Lim	its 80-120 80-120 80-120 80-120	Qualifiers	_		
Parameter Arsenic Barium Cadmium Chromium	SAMPLE: 3	Units mg/L mg/L mg/L mg/L	Conc. 10 10 10 10	Res 0 0 0 0 0	ult 10.1 10.0 10.2 10.3	% Rec 101 100 102 103	Lim	its 80-120 80-120 80-120 80-120	Qualifiers	_		
Parameter Arsenic Barium Cadmium Chromium Lead	SAMPLE: 3	Units mg/L mg/L mg/L mg/L mg/L	Conc. 10 10 10 10 10	Res 0 0 0 0 0 0	ult 10.1 10.0 10.2 10.3 10.0	% Rec 101 100 102 103 100	Lim	its 80-120 80-120 80-120 80-120 80-120 80-120	Qualifiers	_		
Parameter Arsenic Barium Cadmium Chromium Lead Selenium	SAMPLE: 3	Units mg/L mg/L mg/L mg/L mg/L	Conc. 10 10 10 10 10 10 10	Res 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ult 10.1 10.0 10.2 10.3 10.0 10.4	% Rec 101 100 102 103 100 104	Lim	its 80-120 80-120 80-120 80-120 80-120 80-120 80-120	Qualifiers	_		
Parameter Arsenic Barium Cadmium Chromium Lead Selenium	SAMPLE: 3	Units mg/L mg/L mg/L mg/L mg/L	Conc. 10 10 10 10 10 10 10	Res 0 0 0 0 0 0	ult 10.1 10.0 10.2 10.3 10.0	% Rec 101 100 102 103 100	Lim	its 80-120 80-120 80-120 80-120 80-120 80-120	Qualifiers	_		
Parameter Arsenic Barium Cadmium Chromium Lead Selenium Silver		Units mg/L mg/L mg/L mg/L mg/L mg/L	Conc. 10 10 10 10 10 10	Res 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ult 10.1 10.0 10.2 10.3 10.0 10.4 5.0	% Rec 101 100 102 103 100 104	Lim	its 80-120 80-120 80-120 80-120 80-120 80-120 80-120	Qualifiers	_		
Parameter Arsenic Barium Cadmium Chromium Lead Selenium Silver		Units mg/L mg/L mg/L mg/L mg/L mg/L	Conc. 10 10 10 10 10 10	Res 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ult 10.1 10.0 10.2 10.3 10.0 10.4	% Rec 101 100 102 103 100 104	Lim	its 80-120 80-120 80-120 80-120 80-120 80-120 80-120	Qualifiers			
Parameter Arsenic Barium Cadmium Chromium Lead Selenium Silver	SPIKE DUPLI	Units mg/L mg/L mg/L mg/L mg/L mg/L	Conc. 10 10 10 10 10 10 10 10 10 10 10	Res 0 0 0 0 0 0 5	ult 10.1 10.0 10.2 10.3 10.0 10.4 5.0	% Rec 101 100 102 103 100 104	Lim	its 80-120 80-120 80-120 80-120 80-120 80-120 80-120	Qualifiers		Max	
Parameter Arsenic Barium Cadmium Chromium Lead Selenium Silver	SPIKE DUPLI	Units mg/L mg/L mg/L mg/L mg/L mg/L	Conc. 10 10 10 10 10 10 10 10 10 10 10 10 10	Res 0 0 0 0 0 0 5 5 MSD	ult 10.1 10.0 10.2 10.3 10.0 10.4 5.0 3008361	% Rec 101 102 103 104 104	Lim	its 80-120 80-120 80-120 80-120 80-120 80-120 80-120 80-120		RPD	Max RPD	Qua
Parameter Arsenic Barium Cadmium Chromium Lead Selenium Silver MATRIX SPIKE & MATRIX Parameter	SPIKE DUPLI	Units mg/L mg/L mg/L mg/L mg/L mg/L ICATE: 3008	Conc. 1( 1( 1( 1( 1( 1( 360 MS Spike	Res 0 0 0 0 0 0 5 5 MSD Spike	ult 10.1 10.0 10.2 10.3 10.0 10.4 5.0 3008361 MS	% Rec 101 102 103 100 104 101 MSD	Lim	its 80-120 80-120 80-120 80-120 80-120 80-120 80-120 80-120	% Rec Limits		RPD	Qua
Parameter Arsenic Barium Cadmium Chromium Lead Selenium Silver MATRIX SPIKE & MATRIX Parameter Arsenic	SPIKE DUPLI	Units mg/L mg/L mg/L mg/L mg/L mg/L ICATE: 3008 60383151001 Result	Conc. 10 10 10 10 10 10 10 10 10 10	Res 0 0 0 0 0 0 5 5 MSD Spike Conc.	ult 10.1 10.0 10.2 10.3 10.0 10.4 5.0 3008361 MS Result	% Rec 101 102 103 100 104 101 MSD Result	MS % Rec	its 80-120 80-120 80-120 80-120 80-120 80-120 80-120 80-120 80-120 MSD % Rec	% Rec Limits 75-125		$\frac{\text{RPD}}{20}$	Qua
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Results presented on this page are in the units indicated by the "Units" column except where an alternate unit is presented to the right of the result.

10

5

10.1

4.9

10.4

5.1

100

98

103

101

75-125

75-125

3 20

3

20

#### **REPORT OF LABORATORY ANALYSIS**

Selenium

Silver

mg/L

mg/L

ND

ND

10

5

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#### QUALIFIERS

Project:Cont. 3185Pace Project No.:60384336

#### DEFINITIONS

DF - Dilution Factor, if reported, represents the factor applied to the reported data due to dilution of the sample aliquot.

ND - Not Detected at or above adjusted reporting limit.

TNTC - Too Numerous To Count

J - Estimated concentration above the adjusted method detection limit and below the adjusted reporting limit.

MDL - Adjusted Method Detection Limit.

PQL - Practical Quantitation Limit.

RL - Reporting Limit - The lowest concentration value that meets project requirements for quantitative data with known precision and bias for a specific analyte in a specific matrix.

S - Surrogate

1,2-Diphenylhydrazine decomposes to and cannot be separated from Azobenzene using Method 8270. The result for each analyte is a combined concentration.

Consistent with EPA guidelines, unrounded data are displayed and have been used to calculate % recovery and RPD values.

LCS(D) - Laboratory Control Sample (Duplicate)

MS(D) - Matrix Spike (Duplicate)

**DUP - Sample Duplicate** 

**RPD** - Relative Percent Difference

NC - Not Calculable.

SG - Silica Gel - Clean-Up

U - Indicates the compound was analyzed for, but not detected.

N-Nitrosodiphenylamine decomposes and cannot be separated from Diphenylamine using Method 8270. The result reported for each analyte is a combined concentration.

Reported results are not rounded until the final step prior to reporting. Therefore, calculated parameters that are typically reported as "Total" may vary slightly from the sum of the reported component parameters.

Pace Analytical is TNI accredited. Contact your Pace PM for the current list of accredited analytes.

TNI - The NELAC Institute.



#### QUALITY CONTROL DATA CROSS REFERENCE TABLE

Project:Cont. 3185Pace Project No.:60384336

Lab ID	Sample ID	QC Batch Method	QC Batch	Analytical Method	Analytical Batch
60382604002	CKD 1	EPA 3010	751373	EPA 6010	751511
60382604002	CKD 1	EPA 7470	751580	EPA 7470	751583

Pace Analytical Sample Condition U	lpon Receipt	WO#:60382604
Courier:       FedEx       UPS       VIA       Clay       I         Tracking #:       2840       852714/4       Pace         Custody Seal on Cooler/Box Present:       Yes       Note         Packing Material:       Bubble Wrap       Bubble Bags	Seals intact: Yes E Foam □ Flce: Wet Blue No or <u>-0-7</u> Correc	Pace No Xroads Client Other Client Other Client No Client No Client No Client None Other Control Client Cli
Chain of Custody present:		
Chain of Custody relinquished:		
Samples arrived within holding time:	Yes No N/A	
Short Hold Time analyses (<72hr):	Yues □No □N/A	Nox
Rush Turn Around Time requested:		
Sufficient volume:	Yes No DN/A	Jotal metals not requested
Correct containers used:	Yes No N/A	DIA revula BRIN.
Pace containers used:	∰Yes □No □N/A	
Containers intact:		Brongte requested but did
Unpreserved 5035A / TX1005/1006 soils frozen in 48hrs?	□Yes □No <b>[]</b> N/A	not receive volume for it.
Filtered volume received for dissolved tests?		
Sample labels match COC: Date / time / ID / analyses		Mil
Samples contain multiple phases? Matrix:		
Containers requiring pH preservation in compliance? (HNO <sub>3</sub> , H <sub>2</sub> SO <sub>4</sub> , HCl<2; NaOH>9 Sulfide, NaOH>10 Cyanide) (Exceptions: VOA, Micro, O&G, KS TPH, OK-DRO) LOT# Cyanide water sample checks:		List sample IDs, volumes, lot #'s of preservative and the date/time added. Initial pH~3.0. Added IMLIHNO3 (Lut #47205)
Lead acetate strip turns dark? (Record only)	□Yes □No	1 MLHN03 (Lut #47265)
Potassium iodide test strip turns blue/purple? (Preserve)	□Yes □No	on 10/9/21 @ 0958. Finel
Trip Blank present:	□Yes □No 🆄N/A	pH~10
Headspace in VOA vials ( >6mm):	□Yes □No ¥N/A	
Samples from USDA Regulated Area: State:	□Yes □No 🕅N/A	
Additional labels attached to 5035A / TX1005 vials in the field?		
Client Notification/ Resolution: Copy COC to		Field Data Required? Y / N
Person Contacted: Date/T	ime:	
Comments/ Resolution:		
Project Manager Review:	Date	3.

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ENV-FRM-LENE-0001, Rev 31

Dated: 08/19/2021

February 11, 2010

Client:			
TERRAG	CON - BETTENDORF	Work Order:	CTA0801
870 40tł	n Avenue	Project Name:	Lafarge CKD Sample - Buffalo, IA
Bettendo	orf, IA 52722	Project Number:	07107001
Attn:	John Brimeyer	Date Received:	01/21/10

The Chain(s) of Custody, 2 pages, are included and are an integral part of this report.

If you have any questions relating to this analytical report, please contact your Laboratory Project Manager at 1-(800)750-2401

	SAMPLE IDENTIFICATION	LAB NUMBER	COLLECTION DATE AND TIME
CKD		CTA0801-01	01/21/10 11:30

Case Narrative: The TCLP extraction temperature range for this sample is 18.3 degrees C to 21.6 degrees C. The SPLP extraction temperature range for this sample is 18.4 degrees C to 24.1 degrees C.

#### Samples were received into laboratory at a temperature of 0.10 °C.

NELAC states that samples which require thermal preservation shall be considered acceptable if the arrival temperature is within 2 degrees C of the required temperature or the method specified range. For samples with a temperature requirement of 4 degrees C, an arrival temperature from 0 degrees C to 6 degrees C meets specifications. Samples that are delivered to the laboratory on the same day that they are collected may not meet these criteria. In these cases, the samples are considered acceptable if there is evidence that the chilling process has begun, such as arrival on ice.

Please refer to the Temperature and Sample Receipt form that is included with this report for additional information regarding the condition of samples at the time of receipt by the laboratory.

The reported results were obtained in compliance with the 2003 NELAC standards unless otherwise noted. Iowa Certification Number: 007

Reproduction of this analytical report is permitted only in its entirety. This report shall not be reproduced except in full without the written approval of the laboratory.

TestAmerica Laboratories, Inc. certifies that the analytical results contained herein apply only to the specific sample analyzed.

Approved By:

anie Notr

**TestAmerica Cedar Falls** Stefanie Nester Project Coordinator

## TestAmerica

#### THE LEADER IN ENVIRONMENTAL TESTING

704 Enterprise Drive Cedar Falls, IA 50613 \* 800-750-2401 \* Fax 319-277-2425

#### **TERRACON - BETTENDORF** 870 40th Avenue Bettendorf, IA 52722

John Brimeyer

CTA0801 Work Order:

01/21/10 Received: Reported: 02/11/10 15:51

Lafarge CKD Sample - Buffalo, IA 07107001

Project Number:

Project:

#### ANALYTICAL REPORT

Analyte	Sample Result	Data Qualifiers	Units	Quan. Limit	Dilution Factor	Date Analyzed	Analyst	Seq/ Batch	Method
Sample ID: CTA0801-01 (CKD - Soil)					Sampled:	01/21/10 11:30	Rec	vd: 01/21	/10 16:00
General Chemistry Parameters									
% Solids	100		%	0.100	1	01/22/10 15:54	sas	10A0701	SM 2540 G
Total Metals by SW 846 Series Methods									
Antimony	<50.0	IE	mg/kg dry	50.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Arsenic	4.90		mg/kg dry	1.00	0.979	01/26/10 12:52	cjt	10A0680	SW 7060A
Barium	68.6		mg/kg dry	5.00	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Beryllium	0.974		mg/kg dry	0.250	0.979	02/04/10 13:54	cjt	10A0680	SW 7091
Boron	55.8		mg/kg dry	50.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Cadmium	<10.0	IE	mg/kg dry	10.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Chromium	22.6		mg/kg dry	10.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Lead	113		mg/kg dry	50.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Manganese	2700		mg/kg dry	5.00	9.65	01/28/10 06:32	cjt	10A0720	SW 6010B
Mercury	< 0.0200		mg/kg dry	0.0200	0.983	02/01/10 16:42	lbb	10B0047	SW 7471A
Molybdenum	<25.0	IE	mg/kg dry	25.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Nickel	25.7		mg/kg dry	25.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Selenium	<75.0	IE	mg/kg dry	75.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Silver	<10.0	IE	mg/kg dry	10.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Thallium	45.0		mg/kg dry	4.00	3.92	01/28/10 12:45	cjt	10A0680	SW 7841
Vanadium	29.8		mg/kg dry	25.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
Zinc	262		mg/kg dry	10.0	9.65	01/28/10 06:33	cjt	10A0720	SW 6010B
TCLP Metals									
Arsenic	<1.50	IE, T6	mg/L	1.50	5	01/29/10 00:54	cjt	10A0762	SW 6010B
Barium	0.552	Т6	mg/L	0.500	5	01/29/10 00:54	cjt	10A0762	SW 6010B
Cadmium	< 0.100	IE, T6	mg/L	0.100	5	01/29/10 00:54	cjt	10A0762	SW 6010B
Chromium	< 0.100	IE, T6	mg/L	0.100	5	01/29/10 00:54	cjt	10A0762	SW 6010B
Lead	< 0.500	IE, T6	mg/L	0.500	5	01/29/10 00:54	cjt	10A0762	SW 6010B
Mercury	< 0.00200	Т6	mg/L	0.00200	1	01/29/10 12:42	bjb	10A0821	SW 7470A
Selenium	< 0.750	IE, T6	mg/L	0.750	5	01/29/10 00:54	cjt	10A0762	SW 6010B
Silver	< 0.100	IE, T6	mg/L	0.100	5	01/29/10 00:54	cjt	10A0762	SW 6010B
SPLP Metals									
Antimony	< 0.0300	M1, RL1,T6	mg/L	0.0300	5	02/10/10 09:20	lbb	10B0017	SW 7041
Arsenic	< 0.0250	Т6	mg/L	0.0250	5	02/04/10 15:55	cjt	10B0017	SW 7060A
Barium	< 0.500	IE, M1,T6	mg/L	0.500	5	02/02/10 15:52	cjt	10B0013	SW 6010B
Beryllium	< 0.0500	IE,T6	mg/L	0.0500	5	02/02/10 15:52	cjt	10B0013	SW 6010B
Cadmium	< 0.100	IE,T6	mg/L	0.100	5	02/02/10 15:52	cjt	10B0013	SW 6010B
Chromium	< 0.100	IE,T6	mg/L	0.100	5	02/02/10 15:52	cjt	10B0013	SW 6010B
Copper	< 0.500	IE,T6	mg/L	0.500	5	02/02/10 15:52	cjt	10B0013	SW 6010B
Lead	< 0.500	IE,T6	mg/L	0.500	5	02/02/10 15:52	cjt	10B0013	SW 6010B
Mercury	< 0.00200	T6	mg/L	0.00200	1	02/03/10 13:53	bjb	10B0132	SW 7470A
Selenium	< 0.750	IE,T6	mg/L	0.750	5	02/02/10 15:52	cjt	10B0013	SW 6010B
Thallium	0.645	M1,T6	mg/L	0.0400	20	02/11/10 09:33	cjt	10B0017	SW 7841

THE LEADER IN ENVIRONMENTAL TESTING

704 Enterprise Drive Cedar Falls, IA 50613 \* 800-750-2401 \* Fax 319-277-2425

TERRACON - BETTENDORF 870 40th Avenue Bettendorf, IA 52722 John Brimeyer CTA0801

Received: 01/21/10

Lafarge CKD Sample - Buffalo, IA

Reported: 02/11/10 15:51

Project:Lafarge CProject Number:07107001

Work Order:

SAMPLE EXTRACTION DATA

Parameter	Batch	Lab Number	Wt/Vol Extracted	Extracted Vol	Date	Analyst	Extraction Method
SPLP Metals							
SW 6010B	10B0013	CTA0801-01	50.00	50.00	02/01/10 08:57	KMD	SW 3010A - SPLP
SW 7041	10B0017	CTA0801-01	50.00	50.00	02/01/10 09:10	KMD	SW 3020A - SPLP
SW 7060A	10B0017	CTA0801-01	50.00	50.00	02/01/10 09:10	KMD	SW 3020A - SPLP
SW 7470A	10B0132	CTA0801-01	3.00	30.00	02/03/10 11:40	BJB	EPA 245.5/SW 7471.
SW 7841	10B0017	CTA0801-01	50.00	50.00	02/01/10 09:10	KMD	SW 3020A - SPLP
TCLP Metals							
SW 6010B	10A0762	CTA0801-01	50.00	50.00	01/27/10 11:05	BJB	SW 3010A - TCLP
SW 7470A	10A0821	CTA0801-01	3.00	30.00	01/28/10 12:54	BJB	EPA 245.2/SW 7470.
Total Metals by SW 846 Series Metho	ds						
SW 6010B	10A0720	CTA0801-01	1.04	50.00	01/26/10 09:25	KMD	SW 3050B
SW 7060A	10A0680	CTA0801-01	1.02	50.00	01/25/10 11:05	KMD	SW 3050B GFAA
SW 7091	10A0680	CTA0801-01	1.02	50.00	01/25/10 11:05	KMD	SW 3050B GFAA
SW 7471A	10B0047	CTA0801-01	0.61	30.00	02/01/10 14:15	BJB	EPA 245.5/SW 7471.
SW 7841	10A0680	CTA0801-01	1.02	50.00	01/25/10 11:05	KMD	SW 3050B GFAA

## TestAmerica

704 Enterprise Drive Cedar Falls, IA 50613 \* 800-750-2401 \* Fax 319-277-2425

CTA0801

THE LEADER IN ENVIRONMENTAL TESTING

#### **TERRACON - BETTENDORF**

870 40th Avenue Bettendorf, IA 52722 John Brimeyer

Project: 07107001

01/21/10 Received: Reported: 02/11/10 15:51

Lafarge CKD Sample - Buffalo, IA

Project Number:

Work Order:

#### LABORATORY BLANK QC DATA

	Seq/	Source	Spike					Dup	%	Dup	% REC		RPD	
Analyte	Batch	Result	-	Units	MDL	MRL	Result	Result			Limits	RPD	Limit	Q
Total Metals by SW 846 Series Metho														
Arsenic	10A0680		1	mg/kg wet	N/A	1.00	<1.00							
Beryllium	10A0680		1	mg/kg wet	N/A	0.250	< 0.250							
Thallium	10A0680		1	mg/kg wet	N/A	1.00	<1.00							
Antimony	10A0720		1	mg/kg wet	N/A	5.00	<5.00							
Barium	10A0720		1	mg/kg wet	N/A	0.500	< 0.500							
Boron	10A0720		1	mg/kg wet	N/A	5.00	< 5.00							
Cadmium	10A0720		1	mg/kg wet	N/A	1.00	<1.00							
Chromium	10A0720		1	mg/kg wet	N/A	1.00	<1.00							
Lead	10A0720		1	mg/kg wet	N/A	5.00	< 5.00							
Manganese	10A0720		1	mg/kg wet	N/A	0.500	< 0.500							
Molybdenum	10A0720		1	mg/kg wet	N/A	2.50	<2.50							
Nickel	10A0720		1	mg/kg wet	N/A	2.50	<2.50							
Selenium	10A0720		1	mg/kg wet	N/A	7.50	<7.50							
Silver	10A0720		1	mg/kg wet	N/A	1.00	<1.00							
Vanadium	10A0720		1	mg/kg wet	N/A	2.50	<2.50							
Zine	10A0720		1	mg/kg wet	N/A	1.00	<1.00							
Mercury	10B0047		1	mg/kg wet	N/A	0.0200	< 0.0200							
TCLP Metals														
Arsenic	10A0762			mg/L	N/A	0.300	< 0.300							
Barium	10A0762			mg/L	N/A	0.100	< 0.100							
Cadmium	10A0762			mg/L	N/A	0.0200	< 0.0200							
Chromium	10A0762			mg/L	N/A	0.0200	< 0.0200							
Lead	10A0762			mg/L	N/A	0.100	< 0.100							
Selenium	10A0762			mg/L	N/A	0.150	< 0.150							
Silver	10A0762			mg/L	N/A	0.0200	< 0.0200							
Mercury	10A0821			mg/L	N/A	0.00200	< 0.00200							
SPLP Metals														
Barium	10B0013			mg/L	N/A	0.100	< 0.100							
Beryllium	10B0013			mg/L	N/A	0.0100	< 0.0100							
Cadmium	10B0013			mg/L	N/A	0.0200	< 0.0200							
Chromium	10B0013			mg/L	N/A	0.0200	< 0.0200							
Copper	10B0013			mg/L	N/A	0.100	< 0.100							
Lead	10B0013			mg/L	N/A	0.100	< 0.100							
Selenium	10B0013			mg/L	N/A	0.150	< 0.150							
Antimony	10B0017			mg/L	N/A	0.00600	< 0.00600							
Arsenic	10B0017			mg/L	N/A	0.00500	< 0.00500							
Thallium	10B0017			mg/L	N/A	0.00200	< 0.00200							
Mercury	10B0132			mg/L	N/A	0.00200	< 0.00200							

## TestAmerica

THE LEADER IN ENVIRONMENTAL TESTING

704 Enterprise Drive Cedar Falls, IA 50613 \* 800-750-2401 \* Fax 319-277-2425

**TERRACON - BETTENDORF** 

870 40th Avenue Bettendorf, IA 52722

John Brimeyer

CTA0801

01/21/10 Received: Reported: 02/11/10 15:51

Lafarge CKD Sample - Buffalo, IA

Project Number:

Work Order:

Project:

#### 07107001 LABORATORY DUPLICATE QC DATA

	Seq/	Source	Sniko					%	Dup	% REC		RPD	
Analyte	Batch	Result	-	Units	MDL	MRL	Result	70 REC		76 KEC	RPD	Limit	Q
Total Metals by SW 846 Series Meth		Kesuit	Level	Units	MDL	MIXL	Kesuit	KEC	/0KEC	Linnts	KFD	Linnt	Q
QC Source Sample: CTA0773-11	lous												
Arsenic	10A0680	9.18		mg/kg dry	N/A	1.32	8.74				5	20	
Beryllium	10A0680	1.08		mg/kg dry	N/A	0.329	1.05				3	20	
Thallium	10A0680	<1.32		mg/kg dry	N/A	1.32	<1.32					20	
QC Source Sample: CTA0773-10													
Antimony	10A0720	<6.48		mg/kg dry	N/A	6.48	<6.48					20	
Barium	10A0720	245		mg/kg dry	N/A	0.648	217				12	20	
Boron	10A0720	18.4		mg/kg dry	N/A	6.48	16.8				9	20	
Cadmium	10A0720	<1.30		mg/kg dry	N/A	1.30	<1.30					20	
Chromium	10A0720	27.6		mg/kg dry	N/A	1.30	25.9				6	20	
Lead	10A0720	15.2		mg/kg dry	N/A	6.48	15.4				2	20	
Manganese	10A0720	885		mg/kg dry	N/A	0.648	1010				13	20	
Molybdenum	10A0720	<3.24		mg/kg dry	N/A	3.24	<3.24					20	
Nickel	10A0720	26.8		mg/kg dry	N/A	3.24	29.5				10	20	
Selenium	10A0720	<9.72		mg/kg dry	N/A	9.72	<9.72					20	
Silver	10A0720	<1.30		mg/kg dry	N/A	1.30	<1.30					20	
Vanadium	10A0720	55.8		mg/kg dry	N/A	3.24	52.9				5	20	
Zinc	10A0720	69.9		mg/kg dry	N/A	1.30	74.6				7	20	
TCLP Metals													
QC Source Sample: CTA0831-01													
Arsenic	10A0762	< 0.900		mg/L	N/A	0.900	< 0.900					20	
Barium	10A0762	< 0.300		mg/L	N/A	0.300	< 0.300					20	
Cadmium	10A0762	< 0.0600		mg/L	N/A	0.0600	< 0.0600					20	
Chromium	10A0762	< 0.0600		mg/L	N/A	0.0600	< 0.0600					20	
Lead	10A0762	< 0.300		mg/L	N/A	0.300	< 0.300					20	
Selenium	10A0762	< 0.450		mg/L	N/A	0.450	< 0.450					20	
Silver	10A0762	< 0.0600		mg/L	N/A	0.0600	< 0.0600					20	
SPLP Metals													
QC Source Sample: CTA0801-01													
Barium	10B0013	< 0.500		mg/L	N/A	0.500	0.584					20	
Beryllium	10B0013	< 0.0500		mg/L	N/A	0.0500	< 0.0500					20	
Cadmium	10B0013	< 0.100		mg/L	N/A	0.100	< 0.100					20	
Chromium	10B0013	0.0512		mg/L	N/A	0.100	< 0.100					20	
Copper	10B0013	< 0.500		mg/L	N/A	0.500	< 0.500					20	
Lead	10B0013	< 0.500		mg/L	N/A	0.500	< 0.500					20	
Selenium	10B0013	< 0.750		mg/L	N/A	0.750	< 0.750					20	
QC Source Sample: CTA0801-01													
Antimony	10B0017	< 0.0300		mg/L	N/A	0.0300	< 0.0300					20	
Arsenic	10B0017	< 0.0250		mg/L	N/A	0.0250	< 0.0250					20	
Thallium	10B0017	0.645		mg/L	N/A	0.0100	< 0.0100					20	
QC Source Sample: CTA0801-01	1050125	.0.000000		~		0.05555	.0.000000					20	
Mercury	10B0132	< 0.00200		mg/L	N/A	0.00200	< 0.00200					20	

704 Enterprise Drive Cedar Falls, IA 50613 \* 800-750-2401 \* Fax 319-277-2425

THE LEADER IN ENVIRONMENTAL TESTING

**TERRACON - BETTENDORF** 

870 40th Avenue

Bettendorf, IA 52722 John Brimeyer CTA0801

07107001

Received: 01/21/10 Reported: 02/11/10 15:51

Lafarge CKD Sample - Buffalo, IA

ıffalo, IA

Project Number:

Work Order:

Project:

#### LCS/LCS DUPLICATE QC DATA

	Seq/	Source	Spike					Dup	%	Dup	% REC		RPD	
Analyte	Batch	Result	-		MDL	MRL	Result	Result	REC		Limits	RPD	Limit	Q
Total Metals by SW 846 Series Meth	ods													
Arsenic	10A0680		1.89	mg/kg wet	N/A	1.00	1.91		101		80-120			
Beryllium	10A0680		0.947	mg/kg wet	N/A	3.75	0.890		94		80-120			
Thallium	10A0680		1.89	mg/kg wet	N/A	2.00	1.77		93		80-120			
Antimony	10A0720		92.0	mg/kg wet	N/A	5.00	79.0		86		85-110			
Barium	10A0720		46.0	mg/kg wet	N/A	0.500	42.2		92		80-115			
Boron	10A0720		92.0	mg/kg wet	N/A	5.00	85.4		93		85-120			
Cadmium	10A0720		46.0	mg/kg wet	N/A	1.00	41.9		91		80-120			
Chromium	10A0720		46.0	mg/kg wet	N/A	1.00	42.6		93		90-115			
Lead	10A0720		92.0	mg/kg wet	N/A	5.00	94.1		102		80-120			
Manganese	10A0720		46.0	mg/kg wet	N/A	0.500	42.9		93		85-115			
Molybdenum	10A0720		92.0	mg/kg wet	N/A	2.50	87.9		95		90-110			
Nickel	10A0720		92.0	mg/kg wet	N/A	2.50	84.9		92		90-110			
Selenium	10A0720		184	mg/kg wet	N/A	7.50	172		93		85-115			
Silver	10A0720		46.0	mg/kg wet	N/A	1.00	43.1		94		80-110			
Vanadium	10A0720		46.0	mg/kg wet	N/A	2.50	43.5		95		85-115			
Zinc	10A0720		46.0	mg/kg wet	N/A	1.00	46.7		101		80-115			
Mercury	10B0047		0.161	mg/kg wet	N/A	0.0200	0.168		104		80-120			
TCLP Metals														
Arsenic	10A0762		2.00	mg/L	N/A	0.300	1.96		98		85-120			
Barium	10A0762		1.00	mg/L	N/A	0.100	0.928		93		80-115			
Cadmium	10A0762		1.00	mg/L	N/A	0.0200	0.912		91		85-120			
Chromium	10A0762		1.00	mg/L	N/A	0.0200	0.927		93		85-115			
Lead	10A0762		2.00	mg/L	N/A	0.100	1.85		93		80-120			
Selenium	10A0762		4.00	mg/L	N/A	0.150	4.26		107		85-120			
Silver	10A0762		1.00	mg/L	N/A	0.0200	0.864		86		80-110			
Mercury	10A0821		0.0167	mg/L	N/A	0.00200	0.0174		104		80-120			
SPLP Metals Barium	10B0013		1.00	mg/L	N/A	0.100	0.947		95		80-110			
Beryllium	10B0013		1.00	mg/L	N/A	0.0100	0.965		96		80-110			
Cadmium	10B0013		1.00	mg/L	N/A	0.0200	0.949		95		80-120			
Chromium	10B0013		1.00	mg/L	N/A	0.0200	0.935		94		80-110			
Copper	10B0013		2.00	mg/L	N/A	0.100	2.11		105		90-110			
Lead	10B0013		2.00	mg/L	N/A	0.100	1.92		96		80-115			
Selenium	10B0013		4.00	mg/L	N/A	0.100	4.57		90 114		90-113 90-120			
Antimony	10B0013 10B0017		0.0400	mg/L	N/A	0.00600	0.0373		93		90-120 80-120			
Arsenic	10B0017 10B0017		0.0400	mg/L	N/A	0.00500	0.0373		93 97		80-120 80-120			
Thallium	10B0017 10B0017		0.0400	mg/L mg/L	N/A	0.00300	0.0388		97 93		80-120 80-120			
Mercury	10B0017 10B0132		0.0400	mg/L mg/L	N/A	0.00400	0.0372		93 100		80-120 80-120			
Mercury	1000152		0.0107	iiig/L	1 N/ PA	0.00200	0.0107		100		00-120			

TERRACON - BETTENDORF				Wa	rk Order		CTA0801				Pagai	Received:		01/21/10	
870 40th Avenue				WO			C1710001				Repo		02/11/10 15:51		
Bettendorf, IA 52722				Pro	ject:		Lafarge	CKD Sar	nple - I	Buffalo, I					
John Brimeyer				Pro	ject Nur	ber:	0710700	1							
-	M	TRIX	SPIK		, ,		DUPLIC	ATE (		АТА					
									-						
	Seq/	Source	-					Dup	%	Dup	% REC		RPD		
Analyte	Batch	Result	Level	Units	MDL	MRL	Result	Result	REC	%REC	Limits	RPD	Limit	Q	
Fotal Metals by SW 846 Series Metho	ods														
QC Source Sample: CTA0773-01 Arsenic	10A0680	2.19	4.09	mg/kg dry	N/A	1.07	6.58	6.39	107	99	75-125	3	20		
Beryllium	10A0680	0.100	2.05	mg/kg dry	N/A	8.03	3.00	3.18	142	145	75-125	6	20	M1	
Thallium	10A0680	<1.07	4.09	mg/kg dry	N/A	1.07	3.72	3.95	91	93	75-125	6	20	1411	
C Source Sample: CTA0773-10	10A0080	~1.07	4.09	iiig/kg ui y	11/71	1.07	5.12	5.95	91	<i>)</i> 5	75-125	0	20		
Arsenic	10A0680	12.2	5.11	mg/kg dry	N/A	2.59	18.6		125		75-125				
Beryllium	10A0680	0.223	2.56	mg/kg dry	N/A	19.4	3.67		135		75-125			M1	
Thallium	10A0680	<1.30	5.11	mg/kg dry	N/A	1.30	4.76		93		75-125				
QC Source Sample: CTA0773-02				5 8 <del></del> 5											
Antimony	10A0720	<6.50	254	mg/kg dry	N/A	6.50	119	104	47	43	75-115	13	20	M1	
Barium	10A0720	186	127	mg/kg dry	N/A	0.650	330	368	113	151	75-125	11	20	MHA	
Boron	10A0720	19.8	254	mg/kg dry	N/A	6.50	215	212	77	80	75-125	2	15		
Cadmium	10A0720	<1.30	127	mg/kg dry	N/A	1.30	105	98.7	82	82	75-115	6	15		
Chromium	10A0720	31.0	127	mg/kg dry	N/A	1.30	134	135	81	86	75-125	1	10		
Lead	10A0720	12.1	254	mg/kg dry	N/A	6.50	246	232	92	92	75-125	6	20		
Manganese	10A0720	461	127	mg/kg dry	N/A	0.650	1430	617	763	130	75-125	79	20	MHA,	
Aolybdenum	10A0720	<3.25	254	mg/kg dry	N/A	3.25	189	179	74	75	75-110	5	10	M1	
Vickel	10A0720	27.1	254	mg/kg dry	N/A	3.25	242	228	84	84	80-110	6	10		
Selenium	10A0720	<9.75	508	mg/kg dry	N/A	9.75	441	423	87	88	85-115	4	10		
silver	10A0720	<1.30	127	mg/kg dry	N/A	1.30	107	77.7	84	65	75-110	32	10	M1,F	
/anadium	10A0720	62.4	127	mg/kg dry	N/A	3.25	170	173	84	92	80-115	2	20		
Line	10A0720	69.5	127	mg/kg dry	N/A	1.30	179	174	86	87	75-125	3	20		
QC Source Sample: CTA0773-09															
Antimony	10A0720	<17.9	219	mg/kg dry	N/A	17.9	84.4		39		75-115			M1	
Barium	10A0720	235	109	mg/kg dry	N/A	1.79	249		12		75-125			MHA	
Boron	10A0720	36.2	219	mg/kg dry	N/A	17.9	214		81		75-125				
Cadmium	10A0720	<3.58	109	mg/kg dry	N/A	3.58	46.1		42		75-115			M1	
Chromium	10A0720	27.3	109	mg/kg dry	N/A	3.58	69.1		38		75-125			MHA	
lead	10A0720	32.2	219	mg/kg dry	N/A	17.9	127		43		75-125			M1	
Manganese	10A0720	915	109	mg/kg dry	N/A	1.79	937		21		75-125			MHA	
Aolybdenum	10A0720	<8.95	219	mg/kg dry	N/A	8.95	75.3		34		75-110			M1	
lickel	10A0720	25.6	219	mg/kg dry	N/A	8.95	118		42		80-110			M1	
elenium	10A0720	<26.8	437	mg/kg dry	N/A	26.8	205		47		85-115			M1	
ilver	10A0720	<3.58	109	mg/kg dry	N/A	3.58	47.9		44		75-110			M1	
/anadium	10A0720	44.8	109	mg/kg dry	N/A	8.95	89.5		41		80-115			MHA	
inc	10A0720	345	109	mg/kg dry	N/A	3.58	555		191		75-125			MHA	
C Source Sample: CTA0773-01 lercury	10B0047	0.00686	0.172	mg/kg dry	N/A	0.0214	0.187	0.176	105	104	80-120	6	20		
ГСLР Metals QC Source Sample: CTA0801-01															
Arsenic	10A0762	<1.50	2.00	mg/L	N/A	1.50	1.89		95		75-125				
Barium	10A0762	0.552	1.00	mg/L	N/A	0.500	1.44		89		75-125				
To denium	10407(2	<0.100	1.00	/1	NT/ A	0.100	0.957		07		75 120				

10A0762 0.552 1.44 1.00 mg/L N/A 0.500 89 10A0762 <0.100 1.00 N/A0.100 0.857 86 Cadmium mg/L Chromium 10A0762 < 0.100 1.00 mg/L N/A 0.100 0.951 95 10A0762 < 0.500 2.00 N/A 0.500 1.87 93 Lead mg/L < 0.750 0.750 108 10A0762 4.00 N/A4.33 Selenium mg/L 10A0762 < 0.100 1.00 N/A0.100 0.848 85 Silver mg/L QC Source Sample: CTA0801-01 10A0821 <0.00200 0.0167 mg/L N/A 0.00200 0.0171 102 Mercury

**TestAmerica Cedar Falls** Stefanie Nester Project Coordinator 75-120

80-115

75-125

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75-125

75-125

THE LEADER IN ENVIRONMENTAL TESTING

704 Enterprise Drive Cedar Falls, IA 50613 \* 800-750-2401 \* Fax 319-277-2425

TERRACON - BETTENDORF 870 40th Avenue	Work Order:	CTA0801	Received: Reported:	01/21/10 02/11/10 15:51
Bettendorf, IA 52722	Project:	Lafarge CKD Sample - Buffalo,	1	02/11/10 10:01
John Brimeyer	Project Number:	07107001		
MATRIX	SPIKE/MATRIX SPIKE	DUPLICATE QC DATA		
Seq/ Source	e Spike	Dup % Dup	% REC	RPD

Analyte	Batch	Result	Level	Units	MDL	MRL	Result	Result	REC	%REC	Limits	RPD	Limit	Q
SPLP Metals														
QC Source Sample: CTA0801-01														
Barium	10B0013	< 0.500	1.00	mg/L	N/A	0.500	1.37		137		75-125			M1
Beryllium	10B0013	< 0.0500	1.00	mg/L	N/A	0.0500	0.918		92		75-125			
Cadmium	10B0013	< 0.100	1.00	mg/L	N/A	0.100	0.890		89		75-125			
Chromium	10B0013	0.0512	1.00	mg/L	N/A	0.100	0.954		90		75-125			
Copper	10B0013	< 0.500	2.00	mg/L	N/A	0.500	2.01		100		75-125			
Lead	10B0013	< 0.500	2.00	mg/L	N/A	0.500	1.90		95		75-125			
Selenium	10B0013	< 0.750	4.00	mg/L	N/A	0.750	3.96		99		75-125			
QC Source Sample: CTA0801-01														
Antimony	10B0017	< 0.0300	0.0400	mg/L	N/A	0.0300	< 0.0300				75-125			M1
Arsenic	10B0017	< 0.0250	0.0400	mg/L	N/A	0.0250	0.0353		88		75-125			
Thallium	10B0017	0.645	0.0400	mg/L	N/A	0.100	0.984		847		75-125			M1
QC Source Sample: CTA0801-01														
Mercury	10B0132	< 0.00200	0.0167	mg/L	N/A	0.00200	0.0160		96		75-125			

THE LEADER IN ENVIRONMENTAL TESTING

**TestAmerica Cedar Falls** 

704 Enterprise Drive Cedar Falls, IA 50613 \* 800-750-2401 \* Fax 319-277-2425

TERRACON - BETTENDORF 870 40th Avenue	Work Order:	CTA0801	Received: Reported:	01/21/10 02/11/10 15:51
Bettendorf, IA 52722	Project:	Lafarge CKD Sample - Buffalo, IA	1	
John Brimeyer	Project Number:	07107001		

#### CERTIFICATION SUMMARY

Method	Matrix	Nelac	Iowa
SM 2540 G	Solid/Soil		Х
SW 1311	Solid/Soil	Х	Х
SW 1312	Solid/Soil	Х	Х
SW 6010B	Solid/Soil	Х	Х
SW 7041	Solid/Soil	Х	Х
SW 7060A	Solid/Soil	Х	Х
SW 7091	Solid/Soil	Х	Х
SW 7470A	Solid/Soil	Х	Х
SW 7471A	Solid/Soil	Х	Х
SW 7841	Solid/Soil	Х	Х

Any abnormalities or departures from sample acceptance policy shall be documented on the 'Sample Receipt and Termperature Log Form' and 'Sample Non-conformance Form' (if applicable) included with this report.

For information concerning certifications of this facility or another TestAmerica facility, please visit our website at www.TestAmericaInc.com

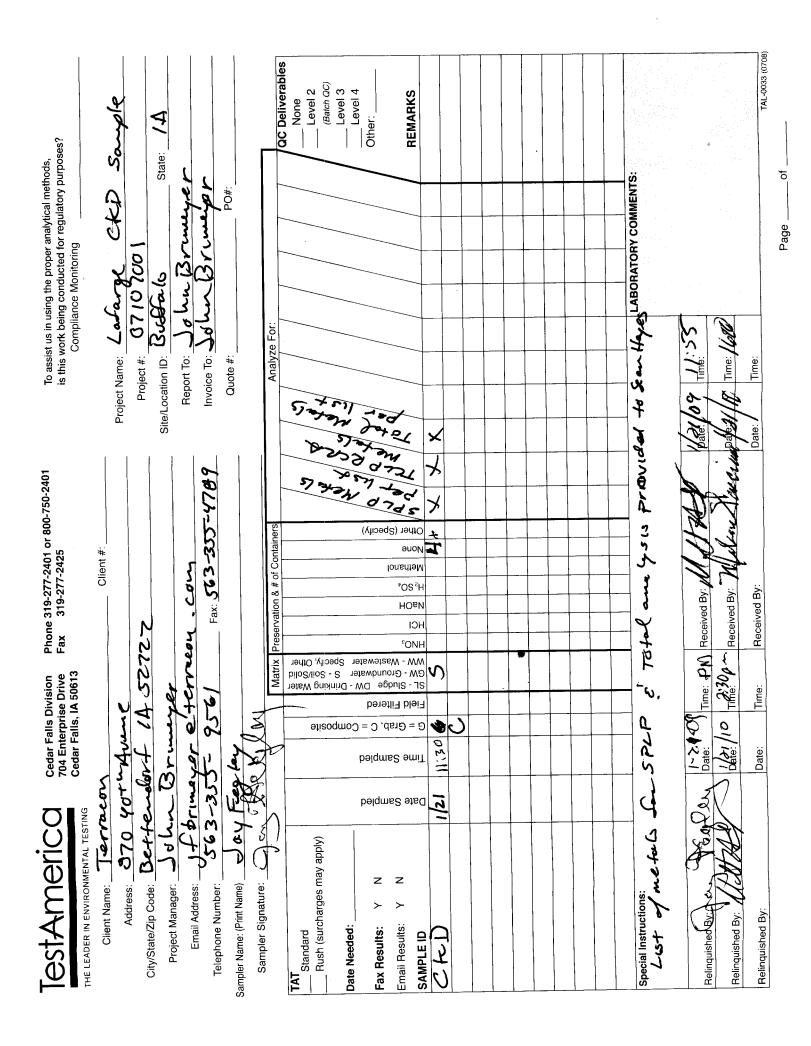
Samples collected by TestAmerica Field Services personnel are noted on the Chain of Custody (COC) and are sampled in accordance with TA-CF SOP CF-FSS-01.

#### DATA QUALIFIERS AND DEFINITIONS

IE	Elevated reporting limit due to interelement interference.
M1	The MS and/or MSD were outside control limits.
MHA	Due to high levels of analyte in the sample, the MS/MSD calculation does not provide useful spike recovery information.
R	Sample duplicate RPD exceeded the laboratory control limit.
RL1	Reporting limit raised due to sample matrix effects.
Т6	The temperature during the 18 hour TCLP/SPLP extraction exceeded the 21-25 degrees C range stated in SW 1311/SW1312.

#### ADDITIONAL COMMENTS

Results are reported on a wet weight basis unless otherwise noted.





704 ENTERPRISE DRIVE • CEDAR FALLS, IA 50613 800-750-2401 • 319-277-2425 FAX

THE LEADER IN ENVIRONMENTAL TESTING

Sample Receipt and Temperature Log Form								
Client: Terrac	on	Pr	roject: Lafarg	e				
City: Date: - 21-10 Rec	eiver's Initials:	СН	Time (Delivere	d): 16:00				
Temperature Record:	Thermometer	:	<u>Courier:</u>					
Cooler ID# (If Applicable) 	IR - 6199767 IR - 9087694 IR - 6185410 22126775	42 'C'	<ul> <li>UPS</li> <li>FedEx</li> <li>FedEx Ground</li> <li>US Postal Service</li> <li>Spee-Dee</li> </ul>	TA Courier TA Field Services				
		Ex	ceptions Noted	······				
Custody seals present?          Yes         Custody seals intact?         Yes         Yes         No	port started	Sa Sa Sa Sa	ample(s) not received in amples(s) received san Evidence of a chilling emperature not taken:	ne day of sampling.				

\*Refer to SOP CF-SS-01 for Temperature Criteria

H:\QA Folder\QA Forms & Log Book pgs\Cooler Receipt rev15.doc

### QUAD CITY WATER TREATMENT CO.



1798 Iowa Drive • P.O. Box 745 • LeClaire, Iowa 52753-0745 Ph. (563) 289-3373 • Fax (563) 289-5526

#### LABORATORY REPORT

Scott Nielson	Report Date	11/23/04
Environmental Manager	Samples Rec	11/21/03
LaFarge of North America	Samples Date	9/5/03
P.O. Box 690	Sample ID	CDK soil sample
Buffalo IA 52728-0690	Lab No	031121-33

	TCLP Results mg/l	RCRA Max Allowable	Methods	Completed By
Parameters		mg/l		
Arsenic	<0.05	5	1311-7061	12-4-03rb
Barium	<5	100	1311-7080	12-4-03rb
Cadmium	<0.05	1	1311-7130	12-5-03ej
Total Chromium	0.18	5	1311-7190	12-5-03ej
Lead	2.02	5	1311-7420	12-5-03ej
Mercury	<0.05	0.2	1311-7470	12-4-03rb
Silver	0.39	5	1311-7760	12-5-03ej
Selenium	<0.05	1	1311-7741	12-4-03rb

ANALYSIS CERTIFIED BY: ROBERT B. BLACK ENVIRONMENTAL CHEMIST

### QUAD CITY WATER TREATMENT CO.



1798 Iowa Drive • P.O. Box 745 • LeClaire, Iowa 52753-0745 Ph. (563) 289-3373 • Fax (563) 289-5526

#### LABORATORY REPORT

Scott Nielson	Report Date	11/23/04
Environmental Manager	Samples Rec	11/21/03
LaFarge of North America	Samples Date	6/2/03
P.O. Box 690	Sample ID	CDK soil sample
Buffalo IA 52728-0690	Lab No	031121-32

	TCLP Results mg/l	RCRA Max Allowable	Methods	Completed By
Parameters		mg/l		
Arsenic	<0.05	5	1311-7061	12-4-03rb
Barium	<5	100	1311-7080	12-4-03rb
Cadmium	<0.05	1	1311-7130	12-5-03ej
Total Chromium	<0.05	5	1311-7190	12-5-03ej
Lead	1.52	5	1311-7420	12-5-03ej
Mercury	<0.05	0.2	1311-7470	12-4-03rb
Silver	<0.05	5	1311-7760	12-4-03ej
Selenium	<0.05	1	1311-7741	12-4-03rb

ANALYSIS CERTIFIED BY: ROBERT/B. BLACK ENVIRONMENTAL CHEMIST tand K

## QUAD CITY WATER TREATMENT CO.

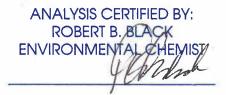


1798 Iowa Drive • P.O. Box 745 • LeClaire, Iowa 52753-0745 Ph. (563) 289-3373 • Fax (563) 289-5526

#### LABORATORY REPORT

Scott Nielson	Report Date	11/23/04
Environmental Manager	Samples Rec	11/8/04
LaFarge of North America	Samples Date	1st quarter 204
P.O. Box 690	Sample ID	CDK soil sample
Buffalo IA 52728-0690	Lab No	041108-27

	TCLP Results mg/l	RCRA Max Allowable	Methods	Completed B y
Parameters		mg/l		
Arsenic	0.08	5	1311-7061	11-15-04rb
Barium	<5	100	1311-7080	11-15-04rb
Cadmium	<0.05	1	1311-7130	11-10-04ej
Total Chromium	0.036	5	1311-7190	11-10-04ej
Lead	7.44	5	1311-7420	11-10-04ej
Mercury	<0.05	0.2	1311-7470	11-15-04rb
Silver	<0.05	5	1311-7760	11-10-04ej
Selenium	0.24	1	1311-7741	11-15-04rb



## QUAD CITY WATER TREATMENT CO.



1798 Iowa Drive • P.O. Box 745 • LeClaire, Iowa 52753-0745 Ph. (563) 289-3373 • Fax (563) 289-5526

#### LABORATORY REPORT

Scott Niels	on	
Environmental Manager		
LaFarge of	North America	
P.O. Box 690		
Buffalo IA	52728-0690	

Report Date11/23/04Samples Rec11/8/04Samples Date1st quarter 2004Sample IDCDK soil sampleLab No041108-28

	TCLP Results mg/l	RCRA Max Allowable	Methods	Completed By
Parameters		mg/l		
	0.05	-	1011 7001	11 15 04.4
Arsenic	<0.05	5	1311-7061	11-15-04rb
Barium	<5	100	1311-7080	11-15-04rb
Cadmium	<0.05	1	1311-7130	11-10-04ej
Total Chromium	0.033	5	1311-7190	11-10-04ej
Lead	1.93	5	1311-7420	11-10-04ej
Mercury	<0.05	0.2	1311-7470	11-15-04rb
Silver	<0.05	5	1311-7760	11-10-04ej
Selenium	<0.05	1	1311-7741	11-15-04rb

ANALYSIS CERTIFIED BY: ROBERT B. BLACK ENVIRONMENTAL CHEMIST





## LABORATORY REPORT

Client Lafarge North America PO Box 690 Buffalo, IA 52728

> Order Number 030592

Project Number CKD

Issued Monday, February 10, 2003

#### **Total Number of Pages**

6

Approved By **Bassam Youssef** Laboratory Manage

NELAC Accreditation #E87688

2LA ISO/IEC 17025 Accreditation #0724.01

"Analytical Integrity" • A2LA Accreditation #0724.01 • ISO 9000 595 East Tallmadge Avenue • Akron, Ohio 44310 • Phone: 330-253-8211 • Fax: 330-253-4489 Email: summitenvironmental@msn.com



2

#### Sample Summary

Client: Lafarge North America Order Number: <u>030592</u>

Laboratory ID	Client ID	Matrix	Sampling Date
030592-01	Cement Kiln Dust	Solid	1/31/03



3

#### **Report Narrative**

Client: Lafarge North America Order Number: 030592

No problems were encountered during analysis of this order number, except as noted.

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"Analytical Integrity" • A2LA Accreditation #0724.01 • ISO 9000 595 East Tallmadge Avenue • Akron, Ohio 44310 • Phone: 330-253-8211 • Fax: 330-253-4489 Email: summitenvironmental@msn.com



February 10, 2003

Client: Lafarge North America Address: PO Box 690 Buffalo, IA 52728

1/31/03
2/5/03
CKD
Cement Kiln Dust
030592-01
Solid
1311
2/6/03

#### **TCLP Metals**

	<b>Detection Limit</b>	Results	<b>Regulatory Level</b>
<u>Parameter</u>	<u>(mg/l)</u>	<u>(mg/l)</u>	<u>(mg/l)</u>
Arsenic	0.50	<0.5	5.0
Barium	2.0	<2.0	100.0
Cadmium	0.10	<0.1	1.0
Chromium	0.20	<0.2	5.0
Lead	0.50	<0.5	5.0
Mercury	0.0020	< 0.002	0.20
Selenium	0.50	<0.5	1.0
Silver	0.50	<0.5	5.0

4



February 10, 2003

5

Client:	Lafarge North America
Address:	PO Box 690
	Buffalo, IA 52728

Date Collected:	1/31/03
Date Received:	2/5/03
Project #:	CKD
Client ID #:	Cement Kiln Dust
Laboratory ID #:	030592-01
Matrix:	Solid
Extraction Method:	1311
Date of Analysis:	2/7/03

#### **TCLP Volatiles**

	<b>Detection Limit</b>	<b>Results</b>	<b>Regulatory Level</b>
<u>Parameter</u>	<u>(mg/L)</u>	<u>(mg/L)</u>	<u>(mg/L)</u>
1,1-Dichloroethene	0.10	<0.1	0.70
1,2-Dichloroethane	0.10	< 0.1	0.50
2-Butanone (MEK)	2.0	<2.0	200.0
Benzene	0.10	< 0.1	0.50
Carbon tetrachloride	0.10	<0.1	0.50
Chlorobenzene	0.10	<0.1	100.0
Chloroform	0.10	< 0.1	6.0
Tetrachloroethene	0.10	< 0.1	0.70
Trichloroethene	0.10	<0.I	0.50
Vinyl Chloride	0.20	<0.2	0.20



February 10, 2003

6

Client:	Lafarge North America
Address:	PO Box 690
	Buffalo, IA 52728

Date Collected:	1/31/03
Date Received:	2/5/03
Project #:	CKD
Client ID #:	Cement Kiln Dust
Laboratory ID #:	030592-01
Matrix:	Solid
Extraction Method:	1311
Date of Analysis:	2/6/03

#### TCLP BNA

	<b>Detection Limit</b>	<b>Results</b>	<b>Regulatory Level</b>
<u>Parameter</u>	<u>(mg/l)</u>	<u>(mg/l)</u>	<u>(mg/l)</u>
1,4-Dichlorobenzene	0.10	<0.1	7.5
2,4,5-Trichlorophenol	0.25	< 0.25	400.0
2,4,6Trichlorophenol	0.25	< 0.25	2.0
2,4-Dinitrotoluene	0.10	<0.1	0.13
Cresols	0.10	<0.1	200.0
Hexachloro-1,3-butadiene	0.10	< 0.1	0.50
Hexachlorobenzene	0.10	<0.1	0.13
Hexachloroethane	0.10	< 0.1	3.0
Nitrobenzene	0.10	< 0.1	2.0
Pentachlorophenol	0.25	< 0.25	100.0
Pyridine	0.25	< 0.25	5.0

<u>Summit Envir</u>	<u>conmental Technologies, Inc.</u>
$\mathbf{D}$	Cooler receipt form
Customer: La farge	Order Number:
Date Received: 2/5/03	Time Received:/19:00 A
Number of Coolers/Boxes:	N/A
Shipper: FED EX UPS Airborne US Cargo US Po	stal Walk-in Pickup Other:
Packaging: Peanuts Bubble wrap Paper For	am None Sample ID all on the
Tape on cooler/box	None <u>Sample ID</u> <u>pH</u> <u>Sample ID</u> <u>pH</u> N/A
Custody Seals intact Y N	N/A
C.O.C. in plastic Y N	) N/A
Ice/Blue Icepresent Y N	N/A
Temperature: 8.5 ° C	C N/A
C.O.C. filled out properly Y	N/A
Samples in separate bags Y N	NTA)
Sample containers intact*	N/A
Label(s) complete (ID, date, time, etc) Y	N/A
Label(s) agree with C.O.C. Y N	N/A
Correct containers used	N/A
Preserved properly Y N	(N/A )
Sufficient Sample (Y) N	N/A
Bubbles absent from 40ml Y N	N/A
*If no which ones broken:	
Was client called about broken samples Y N	
Will client send new sample(s) Y N	,
Talked to	
Date/Time	<i></i>
Loggod in by A	
Logged in by the	
Comments:	1 1 clp No pest or herbs
Date Collected	1 15 1/31/03
we rec. blank C.D.C.	BN 215/03
Rev. 4	

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~

FAX NO. : 6157910423



THE AMERICAN ASSOCIATION FOR LABORATORY ACCREDITATION

## ACCREDITED LABORATORY

A2LA has accredited

## SUMMIT ENVIRONMENTAL TECHNOLOGIES, INC. Akron, OH

### for technical competence in the field of

#### **Environmental Testing**

The accreditation covers the specific tests and types of tests listed on the agreed scope of accreditation. This laboratory meets the requirements of ISO/IEC Guide 25-1990 "General Requirements for the Competence of Calibration and Testing Laboratories" (equivalent to relevant requirements of the ISO 9000 series of standards) and any additional program requirements in the identified field of testing.

Presented this 3rd day of April, 2000.



President / For the Accreditation Council Certificate Number 724.01 Valid to: January 31, 2002

For tests or types of tests to which this accreditation applies, please refer to the laboratory's Environmental Scope of Accreditation

FROM : SUMMITENVIRONMENTAL

02/05/03 WED 13:59 [TX/RX NO 7939]

192403 WED 13:59 [TX/RX NO 7939]

na oli 1724 August Client Address po Box ( Bruffalo, 'Client Name Client Phone No. 328-6206 Client Fax No. Contract Person afarge Sampled by Stoff Nielson 563-328-7001 Summit Environmental Technologies, Inc. 595 East Tallmadge Avenue Akron, Ohio 44310 690 王丹 5:2728 North America 00 Vingles emen Please Fax Results v Kiln Ourt Tel: 330,253,8211 Fax; 330,253,4489 Project Name H Dd Report to Scott Nickson Project Address "Quote No. Check it Ohio VAP samples v CKO Same TENKET STOLE CC-1 ... Analysis Request/Chain of Custody ingle in In the Grad Composite For Summit Environmental Technologies, Inc. use only N TEACHER OF C Page \_ -Tecp 0 ticalParan BET. No. 1999年1 DN XUJ FROM : SUMMITENUIRONIROM W450:20 2002 50 Feb. ЪЗ

200 🛛

LAFARGE DAVENPORT

05/02/03 I2:54 EVX I 318 353 200T

**APPENDIX C** 

Monthly Certified Operators Inspection Form

Site:	Cement Kiln Dust (CKD) Landfill
	Continental Cement Company
	82-SDP-16-97P (Active)
	82-SDP-16-97P (Closed)
Project Location:	301 East Front Street
-	Buffalo, Iowa 52728
Certified Operator:	
Inspection Date:	
Daily Waste Volume:	
CLOSED PHASE I CELL	
Access Roads	
Drainage Structures	
Vegetation	
Monitoring Wells	
Liner Integrity	
Additional Comments	
ACTIVE PHASE II CELL	
Access Roads	
Ditches/Swales/Culverts	
Vegetation	
Monitoring Wells	
Exposed Sand	
Additional Comments	
LEACHATE CONTROL SYSTEM	
Access Roads	
Sump working	
Visible piping	
Pump	
Leachate Structures	
Solar System Performance	
Sprinkler System Performance	
Additional Comments	
COVER INTEGRITY	
Soil Cover Condition	
Stormwater Drainage	
Vegetation	
Monitoring Wells	
0	

APPENDIX D

**Emergency Response and Remedial Action Plan** 





## Emergency Response and Remedial Action Plan (ERRAP)

Continental Cement Davenport Plant CKD Landfill 301 East Front Street Buffalo, Iowa IDNR Landfill Permit Number 82-SDP-16-97P

## Prepared for:

Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by: Blackstone Environmental, Inc. 16200 Foster Street Overland Park, Kansas 66085



August 30, 2024



EMERGENCY RESPONSE AND REMDIAL ACTION PLAN CONTINENTAL CEMENT DAVENPORT PLANT CKD LANDFILL 301 EAST FRONT STREET BUFFALO, IOWA IDNR LANDFILL PERMIT NUMBER 82-SDP-16-97P

Prepared for: Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by:

Maren Williams

Maren Williams Project Engineer

**Reviewed by:** 

Kyle Kukuk, P.E. Senior Project Manager

#### TABLE OF CONTENTS

Section		Page
TABL	E OF CONTENTS	ii
1.0	FACILITY INFORMATION	1
2.0	REGULATORY REQUIREMENTS	1
3.0	EMERGENY RESPONSE AND REMEDIAL ACTION PLAN	2
3.1	Failure of Utilities	2
3.2	Weather Related Events	2
3.3	Fires and Explosions	2
3.4	Regulated Waste Spills and Releases	2
3.5	Hazardous Material Spills and Releases	3
3.6	Mass Movement of Land and Waste	3
3.7	Emergency and Release Notifications and Reporting	4
3.8	Emergency Waste Management Procedures	4
3.9	Primary Emergency Equipment Inventory	4
3.10	) Emergency Aid	4
3.11	I Training	5

#### APPENDICES

A Figures

#### Page



#### 1.0 FACILITY INFORMATION

Continental Cement Company, LLC (Continental) is located at 301 Front Street in Buffalo, Scott County, Iowa (Site). Quarrying and manufacturing of Portland cement products have been conducted at the Continental facility since 1924 and other uses are not anticipated in the future. The cement manufacturing process includes the heating of limestone with silica, alumina, and iron minerals to form clinker. The clinker (nodules of sintered material) is ground into a fine powder and mixed with gypsum to form cement. As part of the manufacturing process, removal of particulate is required to control the composition of the cement product. This material is known as cement kiln dust (CKD). Continental Cement Company operates an approximately 20-acre monofil for the disposal of CKD. The southern portion of the monofill has been filled to original grade and closed in general accordance with the requirements of the Iowa Department of Natural Resources (IDNR) Permit Number 82-SDP-15-96C. An active monofill disposal cell (Phase II) is operated under IDNR Permit Number 82-SDP-16-97P. The amount of CKD per day disposed at the monofill varies by day. Continental continues to operate with the overall goal of minimizing landfilled CKD and beneficially reusing material when able.

The Continental facility is located approximately four miles west of Davenport, Iowa within Sections 14,15,22, and 23, of Township 77 North, - Range 2 East (Buffalo Township), Scott County as shown on the attached Figure 1, Appendix A. The facility has been in operation, under various ownership, from 1924 for the quarrying of limestone rock and the manufacture of Portland cement. The CKD landfill is located in an inactive portion of the quarry approximately 2000 feet east of the active quarry area and comprises approximately 20 acres. A site diagram of the landfill is attached as Figure 2, Appendix A.

The Certified Operator responsible for the operation of the project is as follows:

Damion Sadd, Environmental Manager 301 East Front Street P.O. Box 690 Buffalo, IA 52728 (563)328-6204

#### 2.0 REGULATORY REQUIREMENTS

In accordance with Iowa Code section 455B.306(6)(d) an Emergency Response and Remedial Action Plan (ERRAP) was submitted as part of the December 27, 2021, permit renewal application. Condition X.2.h of the new permit issued by IDNR on January 6, 2022, required submission of a revised ERRAP for subsequent permit renewal applications.



#### 3.0 EMERGENY RESPONSE AND REMEDIAL ACTION PLAN

#### 3.1 Failure of Utilities

The landfill is utilized for the disposal of CKD, which is a byproduct manufactured at the same site. Since no utilities are located within the landfill, operations at the plant will also be affected if a failure of utilities occurs. Due to this fact, it is possible to cease operations at the landfill, if necessary, without adversely affecting CKD storage and disposal for short-term and long-term events.

#### 3.2 Weather Related Events

Disposal operations of CKD are primarily performed during winter when tornadoes, windstorms, intense rainstorms and erosion, lightning strikes, and flooding are historically not factors. Because the landfill is utilized for the disposal of CKD, which is manufactured the same site, if weather related events occur, operations at the plant will also be affected. Due to this fact, it is possible to cease operations at the landfill, if necessary, without adversely affecting CKD storage and disposal.

#### 3.3 Fires and Explosions

The CKD landfill is a monofil constructed and operated to dispose of CKD, a material generated through the manufacture of Portland cement. This material is created in a pyro processing system at temperatures in excess of 2600°F. Once the material leaves the pyro processing system, it has been thoroughly fired, therefore, CKD as a landfilled material being stored, transported, unloaded, or placed cannot: Be altered by fire, support a flame, be susceptible to creating an explosion, or assist in a runaway reaction needed to generate an explosion.

There are no buildings, equipment, utilities, stored fuels, facilities, or working areas located within the landfill that can catch on fire. CKD does not break down to form methane gas, so methane gas does not accumulate in the landfill and lead to explosive atmospheres.

#### 3.4 Regulated Waste Spills and Releases

Continental's current operation procedures were created to minimize the release of CKD to the ambient air during storage, transport, unloading, and placement of the material. These procedures include:

- After processing, CKD is stored within an enclosed structure (e.g., silo).
- During the process of loading for transport to the landfill, CKD is conditioned with water to minimize dusting during transport and placement.



- Conditioned CKD tends to agglomerate in the truck which makes it less vulnerable to spillage during transport.
- Employees operating landfill transport trucks are trained in the correct operating procedures, which include instruction regarding the amount of material suitable for one truckload. Employees are encouraged not to overfill trucks to ensure that material does not leave the truck during transport prior to unloading at the landfill.
- The time between transport and placement in the landfill is minimized to reduce drying time which could lead to wind erosion during placement.
- Employees operating landfill placement equipment are trained in the correct operating
  procedures, which include instruction regarding proper placement of material in the landfill.
  Employees are aware that CKD is not to be pushed into the bermed sides of the landfill,
  ensuring that all placed material is well contained withing the landfill bed.
- The landfill is inspected weekly to ensure that CKD is not being released to the surface water including the quarry sump and that the CKD is well within the bermed area so that releases do not occur during storm events.
- A four-foot clay liner compacted to 1x10-7 cm/sec is in place underlying the CKD material to prevent releases to the groundwater.
- Monthly water level monitoring and semi-annual sampling is conducted to monitor for CKD release to the groundwater utilizing wells located both inside and outside of the landfill.

#### 3.5 Hazardous Material Spills and Releases

The CKD landfill is a monofil constructed and operated to dispose of CKD, a material generated through the manufacturing of Portland cement. This material is created in a pyro processing system at temperatures in excess of 2600°F. Once the material leaves the pyro processing system, it has been thoroughly fired. Only CKD, a non-hazardous solid waste, is disposed of at the facility. Except for small quantities of fuels, oils, and other materials contained in transport vehicles and earth moving equipment, hazardous materials are not stored, used, or disposed of at the landfill site.

#### 3.6 Mass Movement of Land and Waste

Due to the cementitious nature of the conditioned CKD, the material tends to bind together when placed at the landfill forming a relatively uniform and solid deposit. The material is able to stand at a relatively steep angle of repose with negligible risk of slumping or slope failure. Further, the material is relatively impervious thereby reducing the likelihood of saturation which could reduce the shear strength and lead to slope instability.

Employees with duties associated with the storage, handling, transport, or disposal of CKD are trained to place CKD in a manner which will reduce the likelihood of slope failures, waste shifts,



and waste subsidence. Transport vehicle drivers are instructed to place material at a safe distance back from the edge of the active cell to avoid surcharging the edge of the cell. Accumulated material is periodically pushed into the active cell with earthmoving equipment. The landfill is also inspected weekly so that situations which would lead to mass movement of waste are avoided or quickly corrected.

#### 3.7 Emergency and Release Notifications and Reporting

CKD, a non-hazardous material generated through the manufacturing of Portland cement, is not subject to release notification and reporting requirements. If releases of fuel, oils, or other materials occur from the transport vehicle or excavating equipment, Continental will provide proper notification to the IDNR and/or the United States Environmental Protection Agency in accordance with applicable requirements.

Due to the cementitious nature of the CKD material, windblown emissions from the face of the landfill or CKD piles are negligible. Further, the runoff from the exposed material is directed into the lined portion of the active cell allowing suspended sediment to settle out on site. The small quantities of fuel, oils, and other materials contained in transport vehicles or excavating equipment, if released, would likely be absorbed by surficial materials at the site. The likelihood of a release of materials affecting off-site properties is negligible. As such, notification to the city and county agencies, news media, or special populations will not be required.

#### 3.8 Emergency Waste Management Procedures

Since the landfill is utilized for the disposal of CKD, which is manufactured at the same site, operations at the plant will also be affected. Due to this fact, it is possible to cease operations at the landfill, if necessary, without adversely affecting CKD storage and disposal for long-term emergency events. In case of a short-term emergency, CKD is stored in a silo at the plant site. Hauling of CKD can be temporarily discontinued until the emergency is resolved.

#### 3.9 Primary Emergency Equipment Inventory

The landfill is staffed only during CKD unloading activities or while shaping and/or capping placed CKD material. The actual time on-site is less than 25 hours per month. Further, combustible materials are not stored, used, or disposed of at the site. As such, emergency equipment is not maintained at the site and water sources/hydrants are not located at the site. In the event of an emergency, equipment resources would be provided by the City of Buffalo, Iowa and/or Scott County.

#### 3.10 Emergency Aid

In the event of an emergency requiring aid, local authorities will be contacted.



#### 3.11 Training

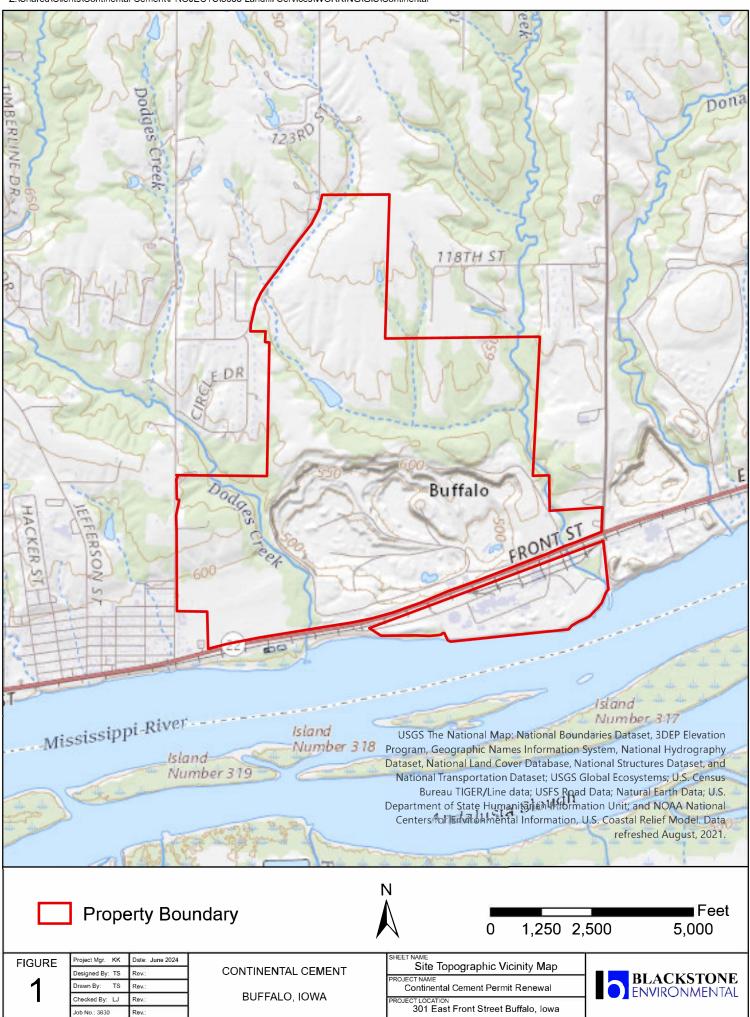
Employees operating landfill transport trucks and/or landfill placement equipment will be trained on the provisions of the ERRAP along with correct operating procedures. Training will be provided by the Environmental Manager or their designee. Training will be conducted for employee's firsttime assignment to duties associated with the storage, handling, transport, or disposal of CKD and periodically thereafter in conjunction with modifications to the ERRAP or issuance of an updated landfill operating permit. Training will be documented in accordance with Continental procedures.



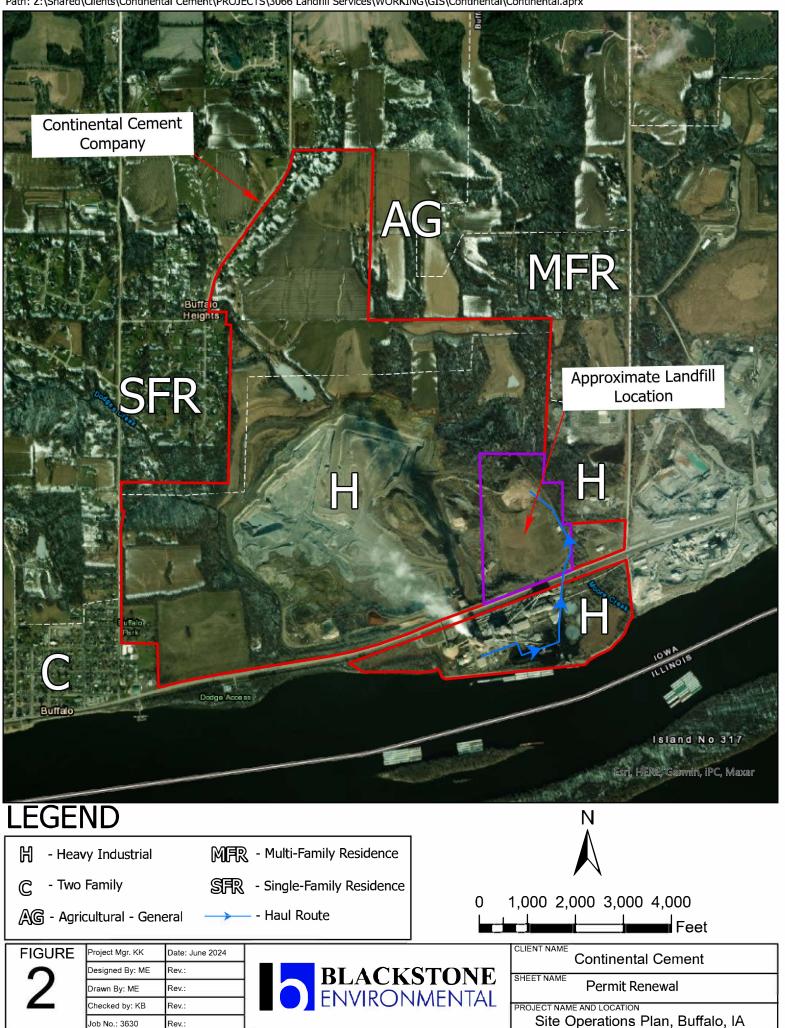
**APPENDIX A** 

Figures

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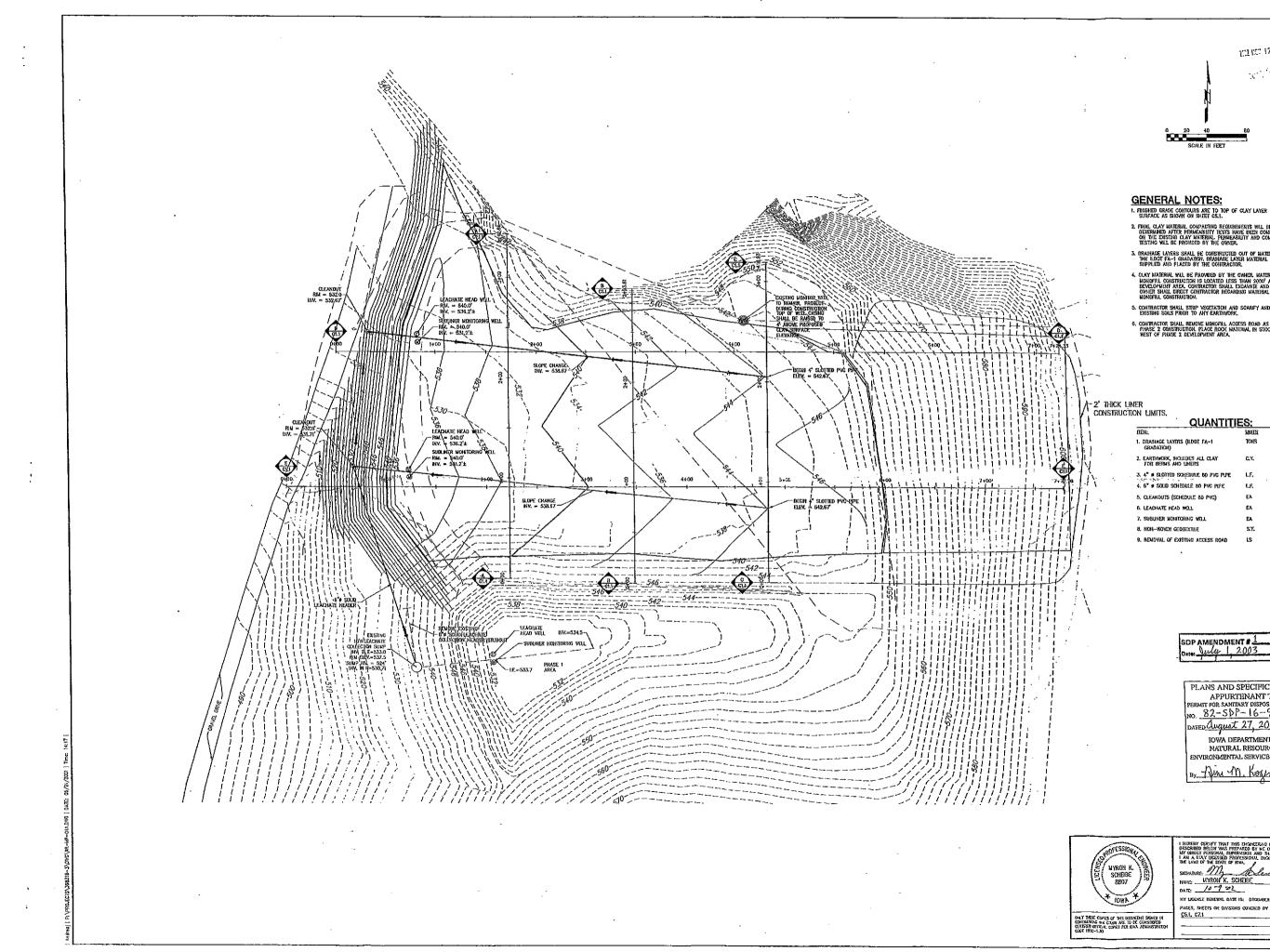
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**APPENDIX E** 

**Facility Development Drawings** 



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- FINAL CLAY MATERIAL COMPACTING REQUIREMENTS DETERMINED AFTER PERMEABILITY TESTS HAVE BEE ON THE ENSTIMA CLAY MATERIAL PERMEABILITY A TESTING WILL BE PRAVATOR OF THE AMERICAN
- RAINAGE LAYERS SHALL BE CONSTRUCTED OUT OF NATERIAL MEET HE LIDOT FA-1 GRADATION, DRAINAGE LAYER MATERIAL SHALL BE SUPPLIED AND PLACED BY THE CONTRACTOR.
- WAL WILL BE PROVIDED BY THE OWNER, MATER CONSTRUCTION IS LOCATED LESS THAN 2000' A NY AREA. CONTRACTOR SHALL EXCAVATE AND LL DIRECT CONTRACTOR REGARDING MATERIAL AND TRANSPORT MATER
- 3. CONTRACTOR SHALL STRIP VEGETATION AND SCARIFY AND COMPACT EXISTING SOLS PRIOR TO ANY EARTHYORK,
- CONTRACTOR SHALL REMOVE MONOFILL ACCESS ROAD AS REQUIRED FOR PHASE 2 CONSTRUCTION, PLACE ROCK MATERIAL IN STOCKPILE AREA DIRECTLY WEST OF PHASE 2 DEVELOPMENT AREA.

MEM:	UNITS	CUANTITY:
1. DRAMAGE LAYERS (ILDOT FA-1 GRADATION)	TONS	13,300
2. EARTHWORK, INCLUDES ALL CLAY FOR BERWS AND UNERS	C.Y.	32,500
3. 4 # SLOTTED SCHEDULE 60 PVC PIPE	LF.	806
4. 6" # SOLID SCHEDULE BO PVC PIPE	LF.	340
5, CLEANDUTS (SCHEDULE 80 PVC)	EA	2
6. LEACHATE KEAD WELL	EA	2
7. Subliner Monitoring Well	EA	2
8. NONHOVEN GEOTEXTILE	S.Y.	720
9. REMOVAL OF EXISTING ACCESS ROAD	LS	1

SDP AMENDMENT # 1

PLANS AND SPECIFICATIONS APPURTENANT TO PERMIT FOR SANTARY DISPOSAL PROJE NO. 82-SDP-16-97P DATED August 27, 2001 IOWA DEPARTMENT OF NATURAL RESOURCES , Jim M. Koza

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CKD MONOFILL PHASE CONSTRUCTION lafarge Buffalo, Ia

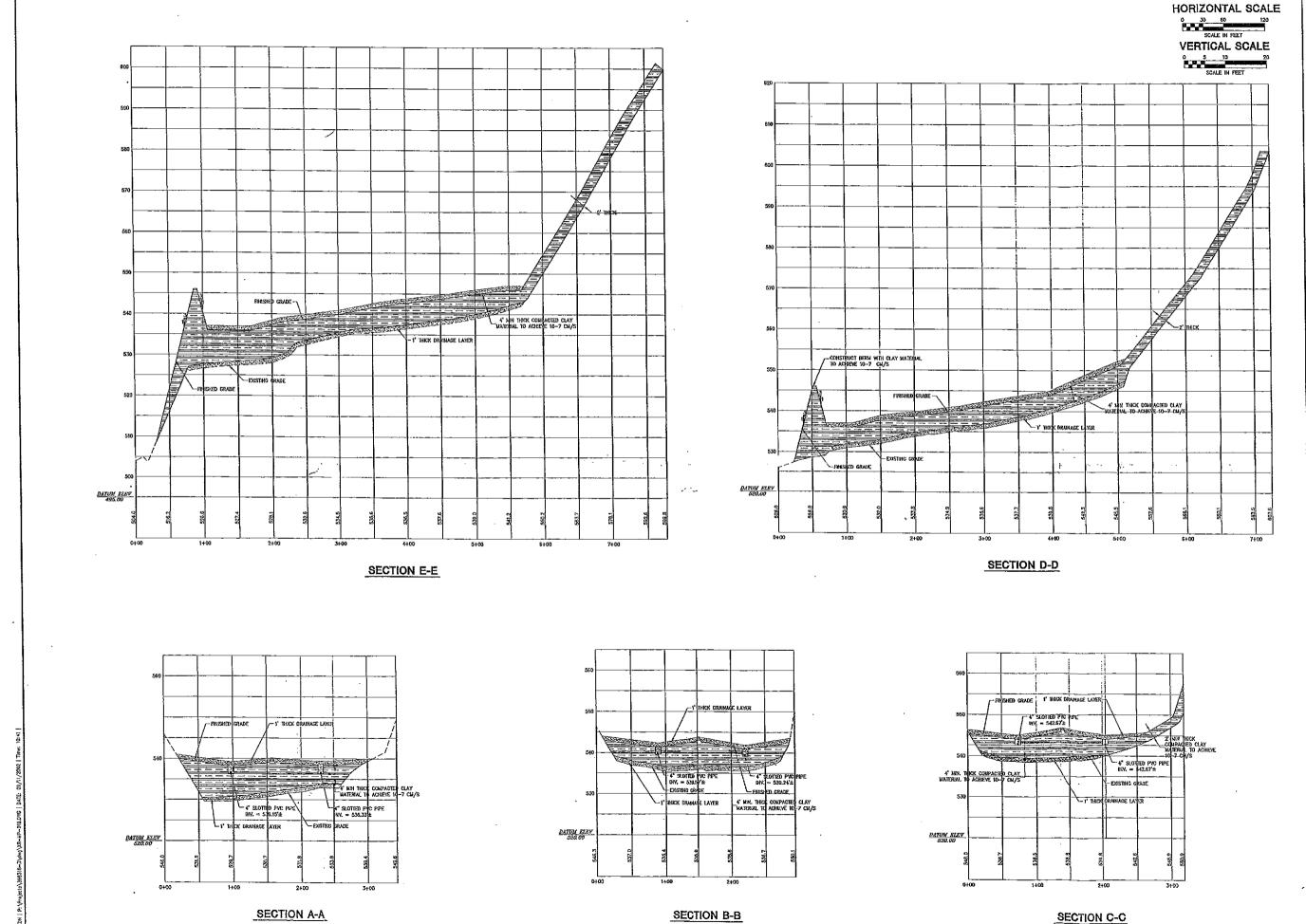
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site plan And grading Plan

PROJECT NO. 398318-3

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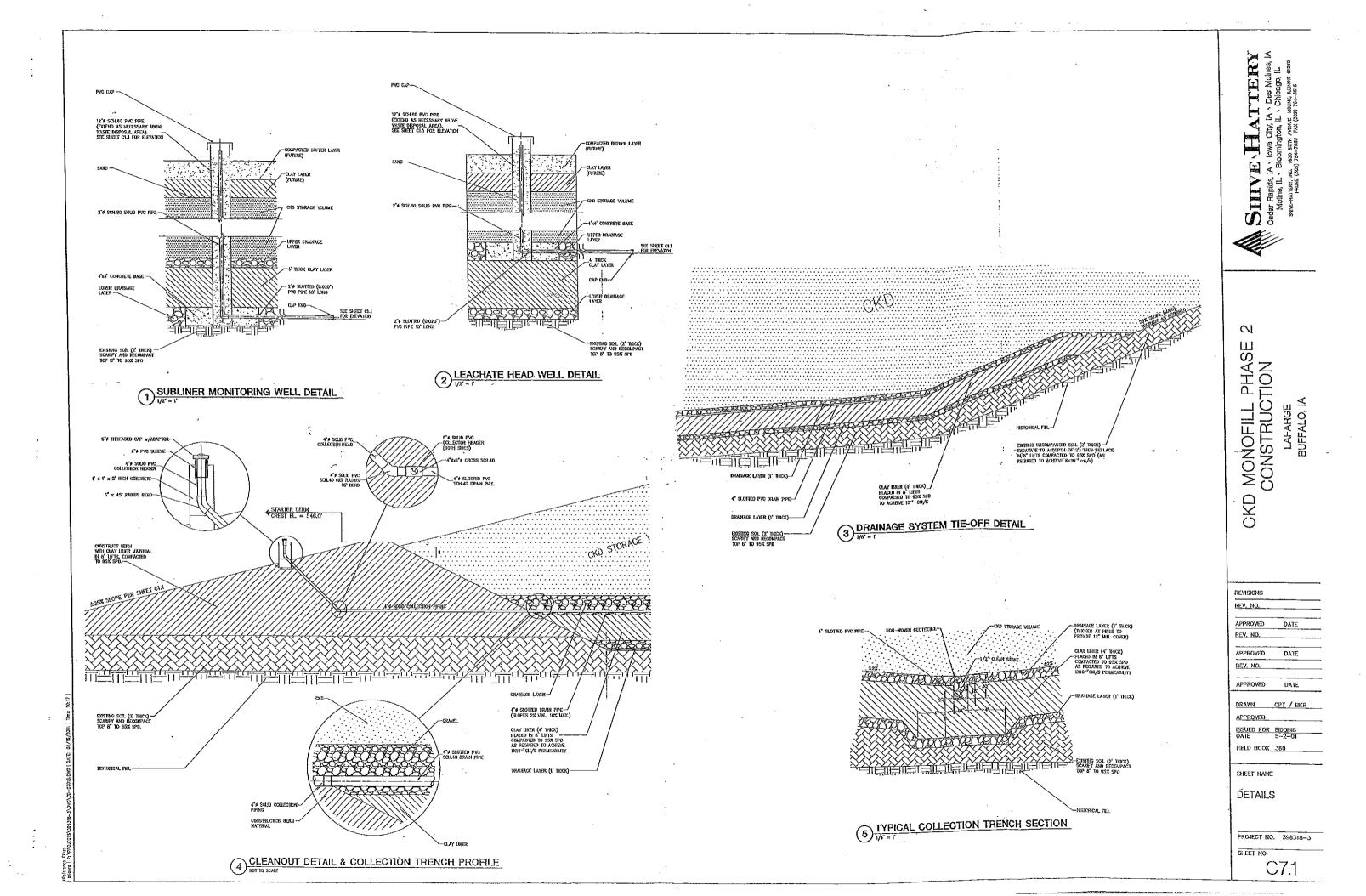


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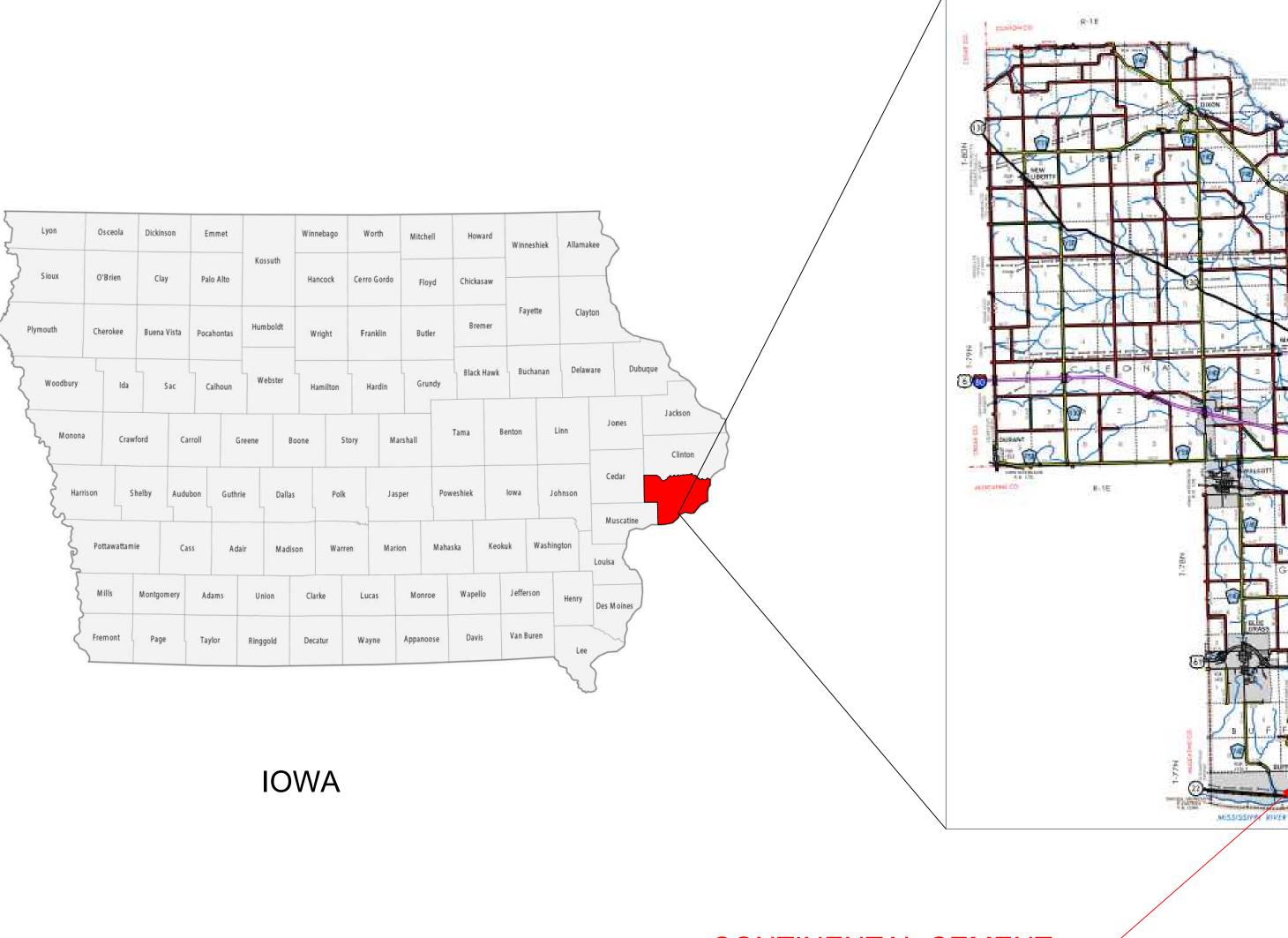


SHEET NO.

C5.1



DRAWING INDEX		
DRAWING NO.	TITLE	
0	COVER SHEET	
1	EXISTING CONDITIONS	
2	FINAL COVER PLAN	
3	CROSS-SECTIONS	
4	DETAILS	



# PREPARED FOR:



CONTINENTAL CEMENT 301 EAST FRONT STREET BUFFALO, IA 52728

**PREPARED BY:** 

BLACKSTONE ENVIRONMENTAL

> 1465 41ST STREET, SUITE 13 MOLINE, ILLINOIS 61265

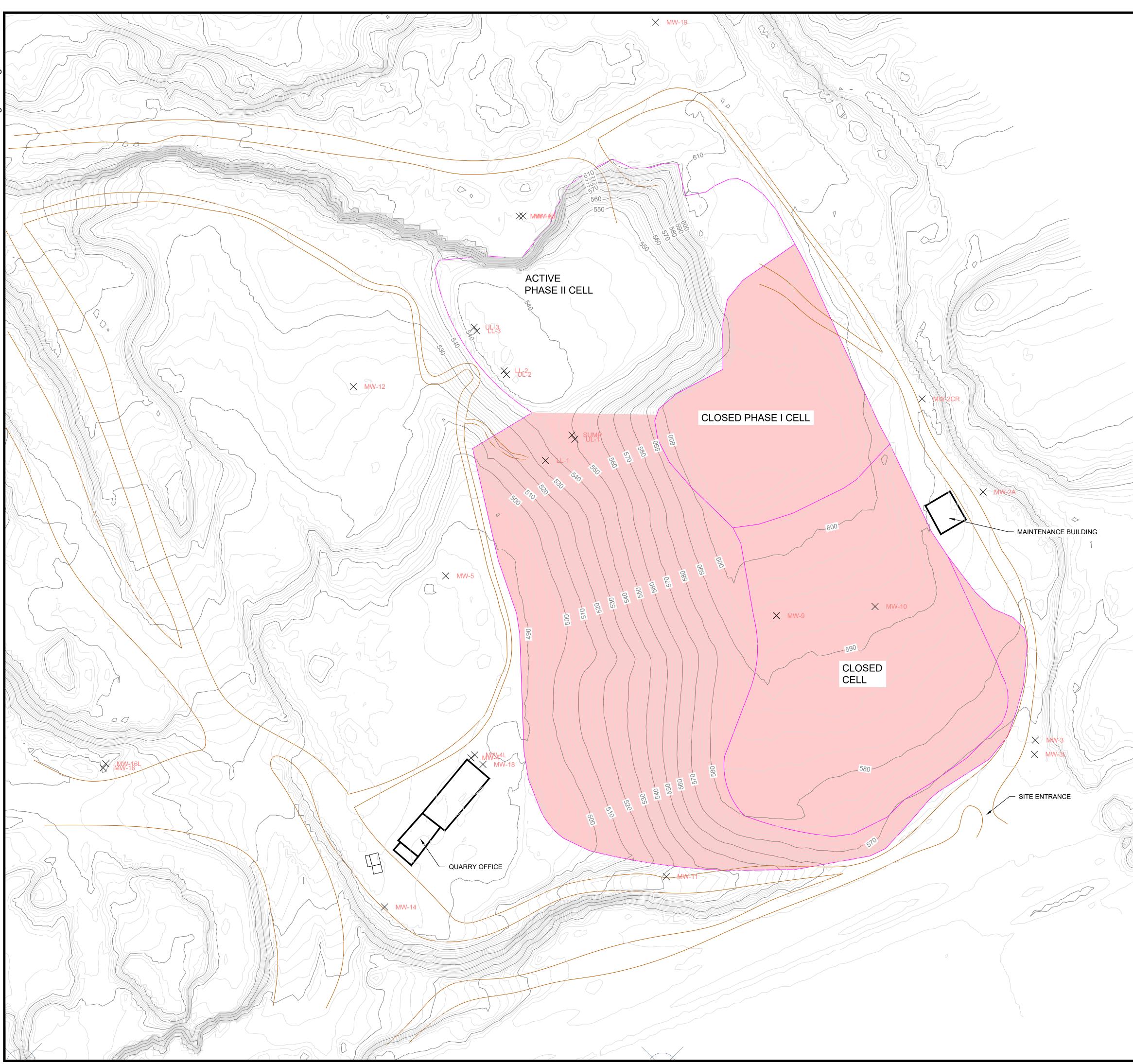
> > PROJECT NO. 3251 MAY 2022

# CLOSURE DRAWINGS CONTINENTAL CEMENT CKD MONOFILL SCOTT COUNTY, IOWA IOWA LANDFILL PERMIT NO. 82-SDP-16-97P MAY 2022

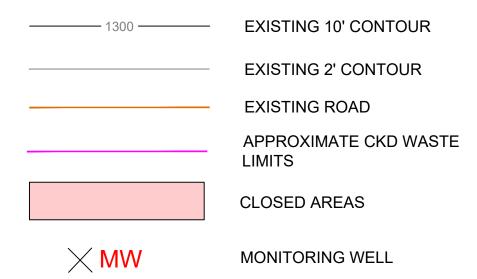
CONTINENTAL CEMENT MONOFILL

## VICINITY MAP

I HEREBY CERTIFY THAT THIS ENGINEERING DOCUMENT WAS PREPARED BY ME OR UNDER MY DIRECT PERSONAL SUPERVISION AND THAT I AM A DULY LICENSED PROFESSIONAL ENGINEER UNDER THE LAWS OF THE STATE OF IOWA. May 31, 2022 SIGNATURE DATE ERIC SONSTHAGEN LICENSE NUMBER: P24844 MY LICENSE RENEWAL DATE IS DECEMBER 31, 2023 SONSTHAGEN P24844 P24844 PAGES OR SHEETS COVERED BY THIS SEAL: SHEETS 0-4

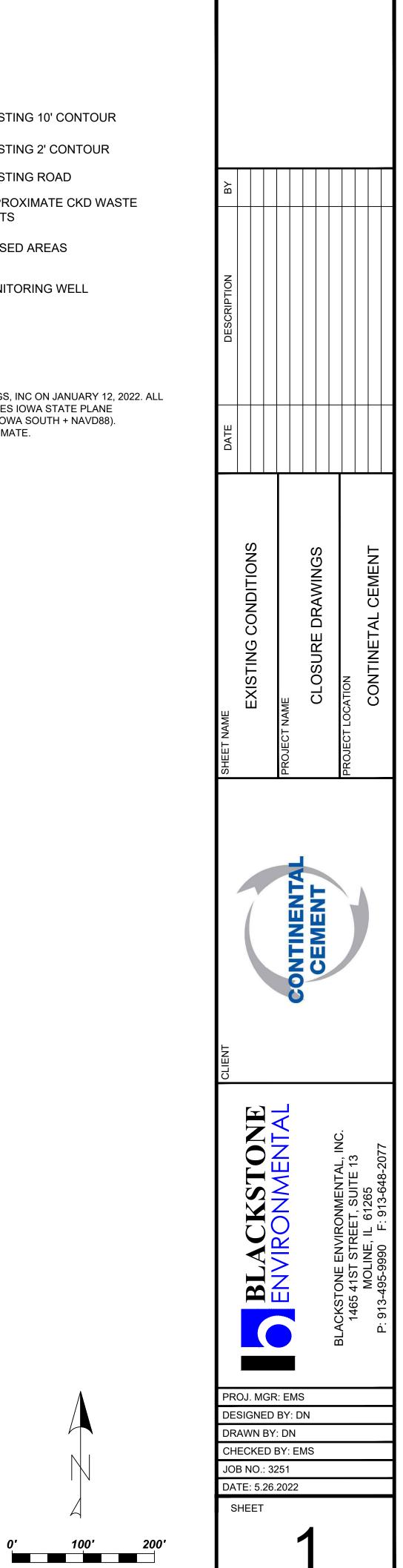


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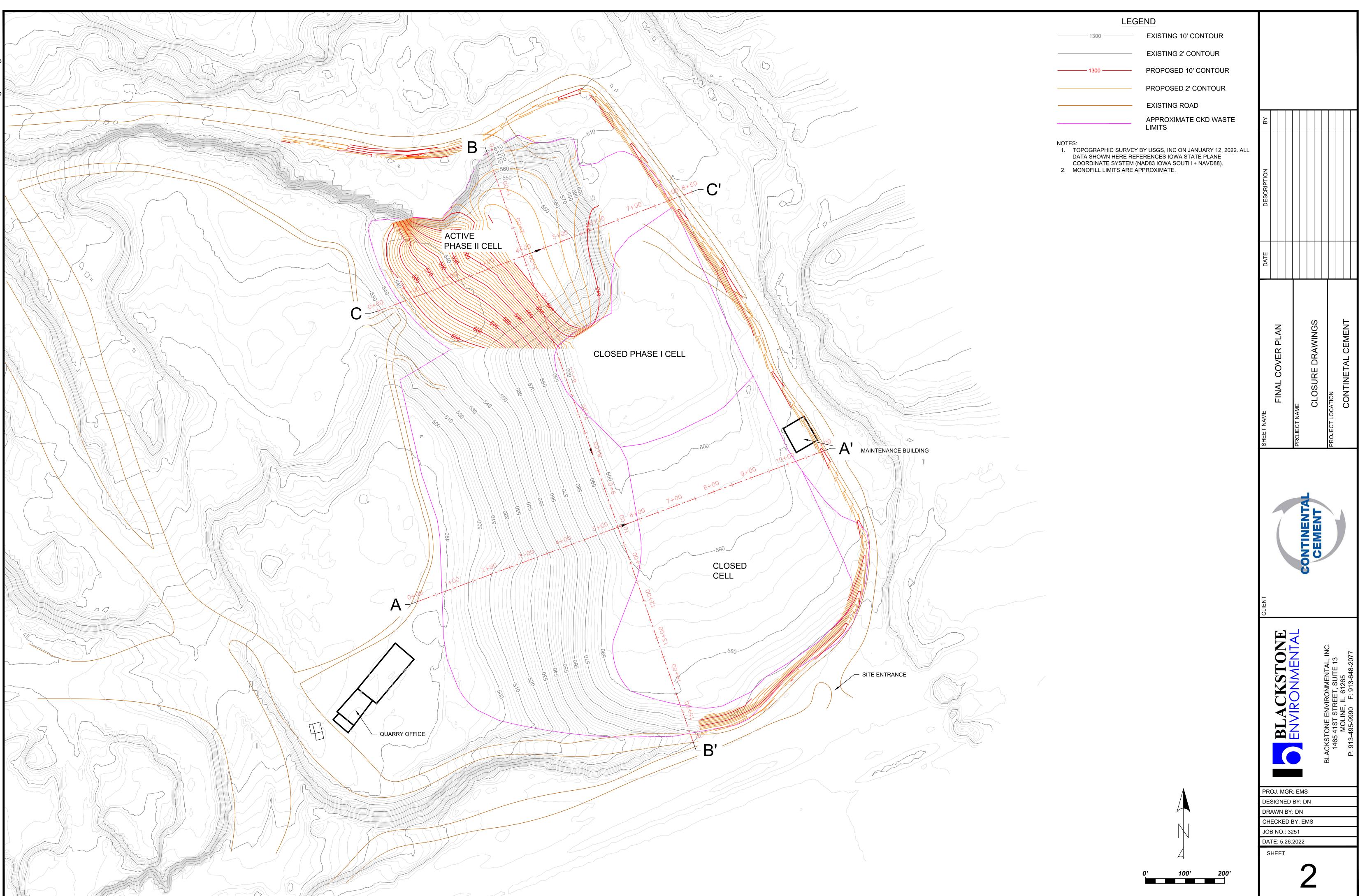


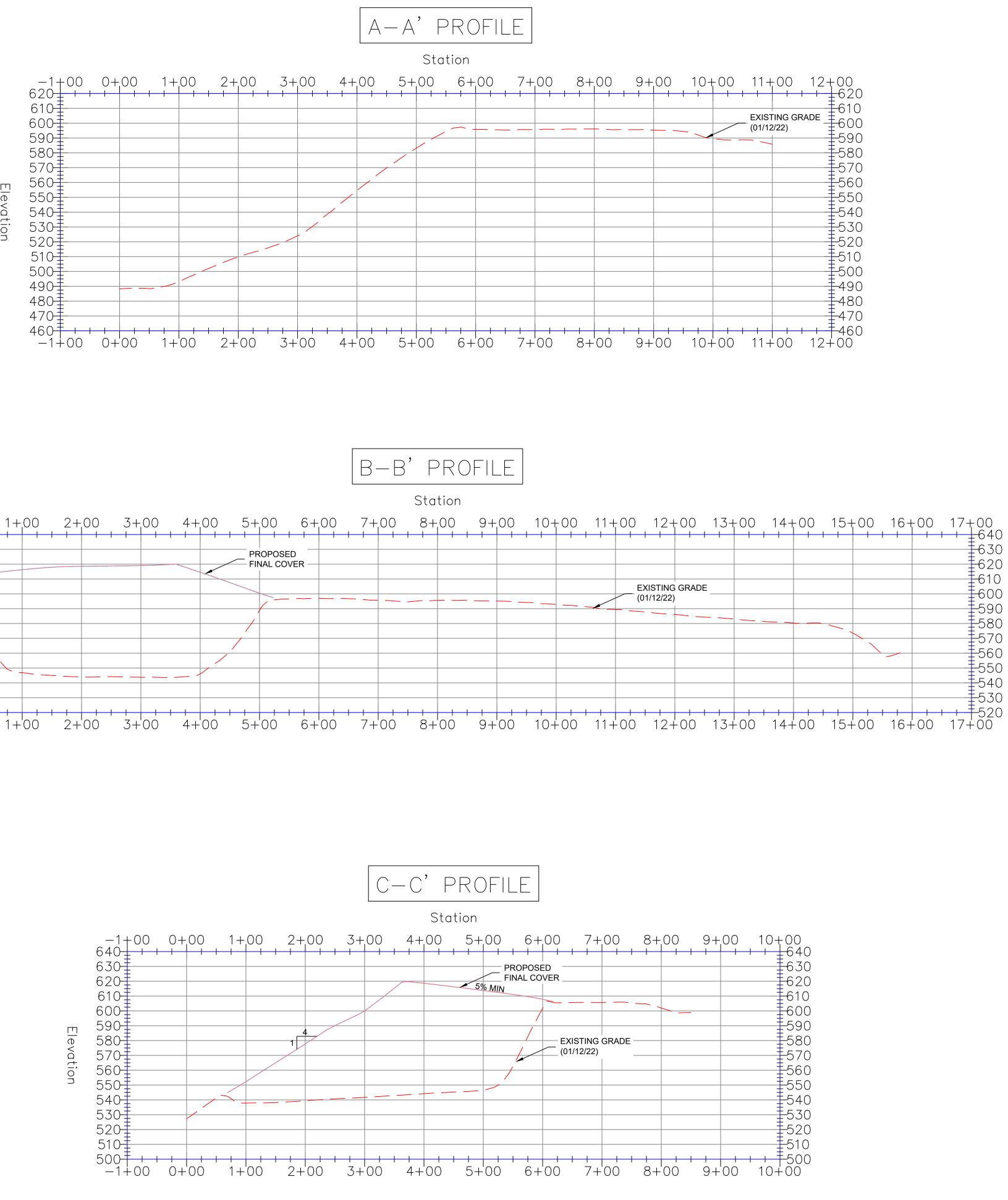
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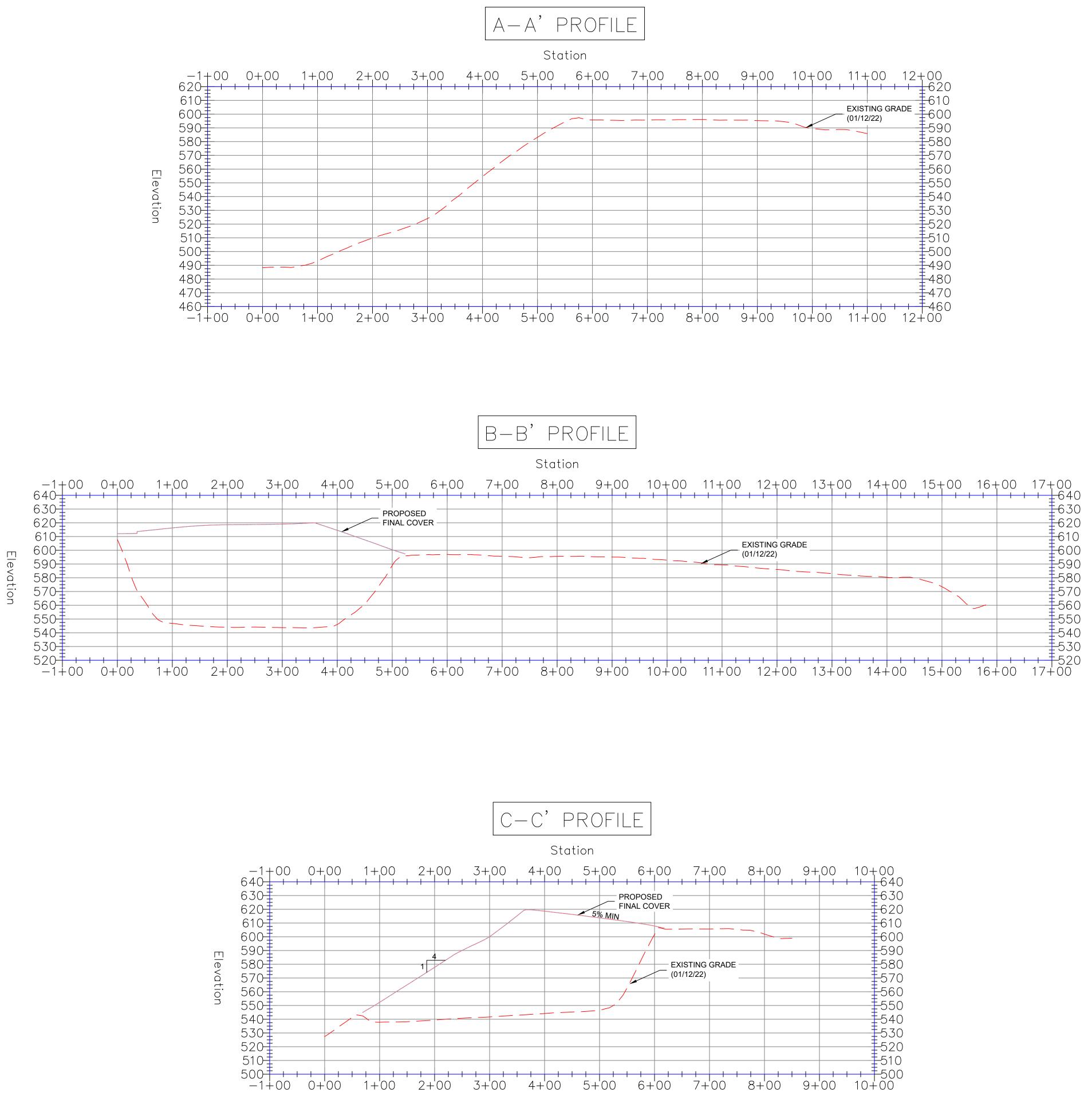
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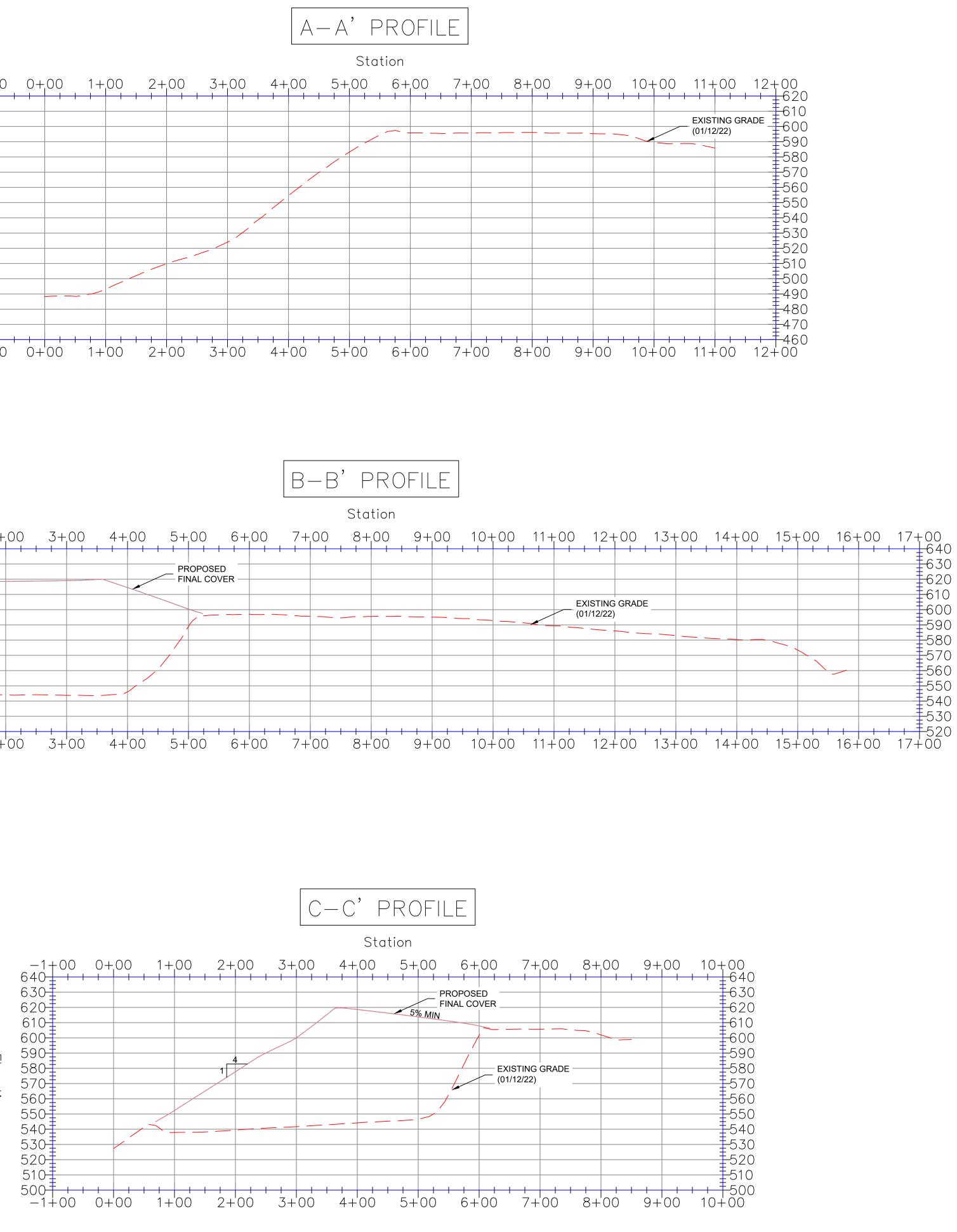


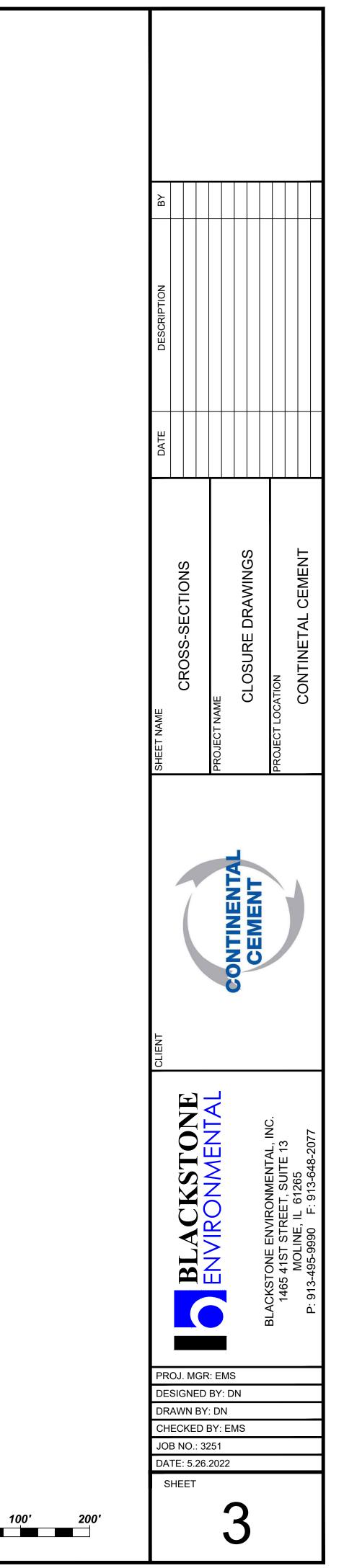
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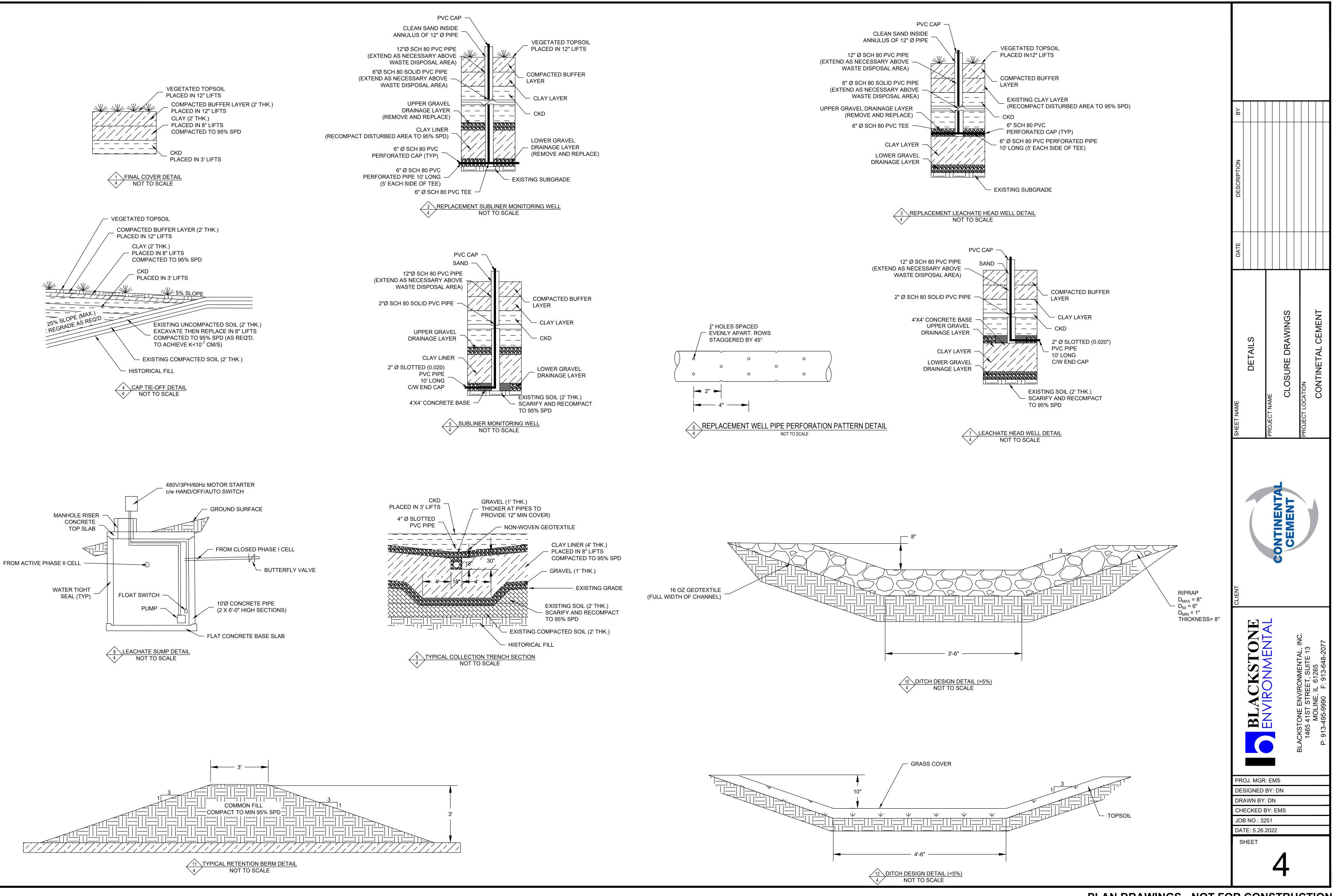












**PLAN DRAWINGS - NOT FOR CONSTRUCTION** 



**APPENDIX F** 

**Closure/Post Closure Plan** 



# **CLOSURE, POST-CLOSURE PLAN**

Continental Cement Cement Kiln Dust Landfill Buffalo, Iowa IDNR Landfill Permit Number 82-SDP-16-97P

#### Prepared for:

Continental Cement 301 East Front Street Buffalo, Iowa 52728

**Prepared by:** Blackstone Environmental 1465 41<sup>st</sup> Street, Suite 13 Moline, Illinois 61265



May 31, 2022

Closure, Post-Closure Plan Continental Cement Cement Kiln Dust Landfill 301 East Front Street Buffalo, Iowa IDNR Landfill Permit Number 82-SDP-16-97P

Prepared for: Continental Cement Company, LLC 301 East Front Street Buffalo, Iowa

Prepared by:

Eric Sonsthagen, P.E.// Senior Project Engineer

**Reviewed by:** 

Edward A. Shepard, Jr., P.E. Senior Project Manager

#### TABLE OF CONTENTS

1.3       Purpose         2.0       CLOSURE PLAN	SECTION	PAGE
2.1       General Closure Requirements       2         2.2       Closure Activities       2         2.2.1       Final Cover       2         2.2.2       Landfill Gas (LFG) Control and Monitoring System       2         2.2.3       Stormwater Control System       2         2.3       Soil Balance       6         2.4       Final Use       6         2.5       Survey Plat       6         3.0       POST-CLOSURE PLAN.       6         3.1       General       7         3.2       Cover System Maintenance       7         3.3       Leachate System Operation and Maintenance       7         3.4       Groundwater and Leachate Monitoring       7         3.4.1       Groundwater Monitoring       7         3.4.2       Leachate Monitoring       7         3.4.3       Lower Lysimeter Monitoring       7         3.5       Miscellaneous Site Maintenance       7	<ol> <li>1.1 Background</li> <li>1.2 Facility Planning</li> </ol>	<b>1</b> 1 1 2
2.3       Soil Balance       2.4         2.4       Final Use       2.5         2.5       Survey Plat       2.5         3.0       POST-CLOSURE PLAN	<ul> <li>2.1 General Closure Requirements</li> <li>2.2 Closure Activities</li> <li>2.2.1 Final Cover</li> <li>2.2.2 Landfill Gas (LFG) Control and Monitoring System</li> </ul>	3 3 4 5
3.1General3.2Cover System Maintenance3.3Leachate System Operation and Maintenance3.4Groundwater and Leachate Monitoring3.4.1Groundwater Monitoring3.4.2Leachate Monitoring3.4.3Lower Lysimeter Monitoring3.5Miscellaneous Site Maintenance	2.3 Soil Balance 2.4 Final Use	5 6 6 6
3.4.3     Lower Lysimeter Monitoring     9       3.5     Miscellaneous Site Maintenance     9	<ul> <li>3.1 General</li> <li>3.2 Cover System Maintenance</li> <li>3.3 Leachate System Operation and Maintenance</li> <li>3.4 Groundwater and Leachate Monitoring</li> </ul>	<b>7</b> 7 7 7 8 8
3.7 Remedial Action 10	<ul> <li>3.4.3 Lower Lysimeter Monitoring</li> <li>3.5 Miscellaneous Site Maintenance</li> <li>3.6 Recordkeeping</li> </ul>	9 9 9 10 10
4.0 FINANCIAL ASSURANCE       10         5.0 LIMITATIONS       11		

Continental Cement Buffalo, Iowa

#### FIGURES



- 1 Site Topographic Vicinity Map
- 2 Site Plan
- 3 Landfill Location

#### TABLES

- 1 Groundwater Monitoring Network
- 2 Leachate Monitoring Locations
- 3 Lower Lysimeter Monitoring Locations

#### APPENDICES

- A. Closure Drawings
- B. Closure and Post-Closure Cost Estimate



#### 1.0 INTRODUCTION

The following section provides information regarding the background and purpose of this Closure, Post-Closure Plan (Plan).

#### 1.1 Background

The Cement Kiln Dust (CKD) Landfill is located within a portion of Continental Cement Company's (Continental's) former rock quarry at the Continental facility located in the Southeast Quarter of Section 23, Township 77 North, Range 02 East, in Scott County, Iowa. The Landfill is located approximately 1.3 miles east/northeast of the City of Buffalo in Scott County, Iowa, and approximately 700 feet north of the Mississippi River. Figure 1 provides a topographic map of the property.

The facility has been used for quarrying and manufacturing cement products dating back to the 1920's. The facility is bordered by the Mississippi River to the south, by Linwood Mining and Minerals Corporation (Linwood) to the east, by the City of Buffalo to the west, and by residential and agricultural land to the north.

The original plant was operated from the 1920s until the late 1970s when a new facility was constructed. The current facility manufactures Portland cement and related products. A byproduct of the process is CKD. The CKD material has historically been landfilled within the east end of the quarry as shown on Figure 2. The facility currently generates approximately 2,500 tons of CKD per year.

The CKD landfill area comprises of approximately 29 acres consisting of three sections; the southern Closed Cell and the Closed Phase I Cell have been filled to original grade, and the northern Active Phase II Cell has been partially filled. The landfill location is provided on Figure 3. CKD will continue to be landfilled in the Active Phase II cell until it reaches final grades when it will then be closed with a cover system.

This Plan includes the methods and schedule anticipated to properly close the landfill. Following closure of the landfill, the 30-year post-closure maintenance period will be initiated.

#### 1.2 Facility Planning

Continental's long-term goal is to reduce the amount of CKD that is landfilled. Efforts to achieve that goal have been implemented that include using the CKD in the cement manufacturing process that has greatly reduced the amount of CKD that has been landfilled in the last several years. New technologies are being explored and trials are being conducted that may allow the CKD to be reclaimed from the landfill and processed into a beneficial product. Over the last six to nine months, the efforts Continental has made include:

• Meeting with multiple potential equipment suppliers to gain understanding on potential CKD reuse options.

Continental Closure, Post Closure Buffalo, Iowa



- Provide initial material samples for a preliminary feasibility evaluation.
- Provide additional material samples for a refined feasibility evaluation.

The preliminary feasibility evaluation had promising results. Continental is currently awaiting the analytical results of the refined feasibility evaluation for one potential supplier. Likely next steps include a feasibility study and conceptual site-specific design.

Updates on the efforts to reduce the landfilling of CKD and possibly reclaiming the CKD from the landfill will be provided to the IDNR in the Semi-Annual Engineering Inspection Reports.

#### 1.3 Purpose

This Plan was developed to comply with the Iowa Department of Natural Resources (IDNR) requirements promulgated under Iowa Administrative Code (IAC) 567 Chapter 115 Sanitary Landfills: Industrial Monofills. The Plan describes how and when the facility will be closed in accordance with applicable requirements and is protective of human health and the environment. It describes the proposed groundwater monitoring plan, leachate control system, and necessary site inspection and maintenance activities; and includes the name, address and telephone number of the person or office to serve as a contact with regard to the facility during the post-closure period.



#### 2.0 CLOSURE PLAN

The following section provides information regarding the closure plan sequencing, closure activities, final use, and record survey plat. The closure plan has been developed in a manner that minimized the potential for post-closure release of pollutants to the air, groundwater, and surface waters.

#### 2.1 General Closure Requirements

In accordance with IAC 567.115.27(9) the IDNR will be notified in writing at least 180 days prior to the date the owner/operator expects to being closure of the facility or suspension of operations. Since this facility is not open to the public and only accepts material generated by the owner/operator, a notice of closure date will not be posted at the facility prior to closure. Additionally, a notice will not be published in a newspaper of local circulation prior to closure.

The owner/operator will make provisions to begin final closure within 90 days after the date on which the phase or permitted area receives the final volume of waste. The owner and an engineer registered in the State of Iowa will certify that this Plan has been implemented in compliance with the rules, this Plan, and the permit. Upon completion of closure activities, as-built plans showing changes from the original design plans; test results indicating compliance with final cover requirements, waste removal, equipment decontamination; a copy of the notation field with the county recorder; and other forms of documentation will be submitted to the IDNR as required.

#### 2.2 Closure Activities

The site will begin closure of the landfill within 90 days after receipt of the final volume of waste. The entire active Phase II Cell is anticipated to be closed in a single phase. The closure activities will consist of construction of the final cover, and construction of the final stormwater control structures. These closure activities will be completed in accordance with the approved permit documents in place at the time of closure, including the design drawings, technical specifications, and construction quality assurance plan.

Closure of the active Phase II Cell is designed to meet the following elements:

- Promote stormwater drainage and minimize erosion.
- Minimize infiltration of stormwater by construction of a low permeability cover system.
- Protect the cover system from temperature and moisture by constructing a buffer layer.
- Minimize erosion and sedimentation by constructing a vegetative soil layer and establishing vegetation.
- Provide a technical basis for closure of the existing CKD landfill for approval by the State of Iowa.

A plan view of the existing CKD landfill area is shown on Drawing 1 of Appendix A. Technical details pertaining to closure are presented on Drawing 4. Drawing 2 presents a plan view of the Closure and Drawing 3 presents three cross-sections through the CKD landfill.

Continental Closure, Post Closure Buffalo, Iowa



Upon completion of each phase of closure activities, a Professional Engineer registered in the State of Iowa, will certify that the facility was properly closed in accordance with the approved plans. The certification documentation will be submitted to the IDNR and include construction quality assurance documentation on the various closure system components including evidence that the barrier soil layer was constructed to meet the  $1 \times 10^{-7}$  centimeters per second (cm/sec) permeability standard, as built drawings of the landfill, verification of depths of the final cover components, and types of soil cover on 100-foot centers, and evidence of establishment of vegetation.

#### 2.2.1 Final Cover

The final cover system will consist of the following components from the top layer to the bottom:

- 24-inch soil layer capable of sustaining vegetative growth.
- 24-inch layer of soil compacted to achieve a permeability of less than or equal to 1 x 10<sup>-7</sup> cm/sec.

A minimum of two permanent surveying monuments will be installed by a land surveyor registered in the State of Iowa from which the location and elevation of wastes, containment structures, and monitoring facilities can be determined throughout the post-closure period.

The final cover system will be built in accordance with the approved permit documents in place at the time of closure, including the design drawings, technical specifications, and construction quality assurance plan. The final cover system will have side slopes no greater than 4H:1V with a crown that is sloped at 5 percent.

The cover system will be constructed using soils excavated as part of the quarry expansion activities or other materials capable of achieving the specified hydraulic conductivity. Soils deemed acceptable for use in the cover system will contain a minimum of 10 percent clay by dry weight. Materials will be spread in lifts no greater than 8 inches thick and will be compacted to a minimum 95 percent standard Proctor density to achieve minimum permeability. Laboratory testing has been completed to verify that the proposed final cover materials compacted in this manner possess a hydraulic conductivity no greater than 1 x  $10^{-7}$  cm/sec, as determined using the falling head permeability test. This cap design complies with the lowa Code which specifies a hydraulic conductivity no greater than 1 x  $10^{-7}$  cm/sec (IAC 567-115.26(13)(b)).

A minimum of one field density test will be performed per lift per acre to verify that the density determined by the laboratory analysis as correlated to permeability has been achieved. Results of field density tests will be submitted to IDNR within the certification documentation. The cover system compacted soil layer will be keyed into the bottom liner at the boundary of the waste cell. If initiation of the application of the final cover has not begun within 60 days of completing the final waste lift, an intermediate cover of 1-foot of soil will be applied in the interim.

Continental Closure, Post Closure Buffalo, Iowa



A 2-foot vegetative soil layer will be placed and graded as soon as reasonably possible after the placement of final cover. The vegetative layer will be fertilized, mulched, and seeded to achieve a healthy stand of vegetation. The vegetative soil layer will have sufficient nutrients required for establishing and sustaining vegetation. Topsoil removed at part of the site operations will be stockpiled and used as the vegetative soil layer during installation of the final cover.

After installation the vegetative soil layer will be seeded with native grasses that will provide vegetative cover that is resistant to erosion. The seed mixture will comprise Merion Blue Grass, Kentucky Blue Grass, Creeping Red Fescue, and Perennial Rye Grass, or other appropriate grasses in proportions optimized to account for the site conditions. Organic matter and fertilizers will be added to the topsoil layer to enhance initial growth. Erosion during the germination stage will be minimized by adding mulch or straw to the seed application.

Orice initial growth is established, erosional features or areas of sparse growth will be refilled with topsoil and reseeded. This process will be repeated until a consistent cover layer of vegetation is established. Slopes will be regularly monitored to ensure that the vegetative cover is performing in accordance with its intended design. The closed areas will be cut at least once per year to prevent development of deep-rooted vegetation, such as trees, that could compromise the integrity of the cover system.

#### 2.2.2 Landfill Gas (LFG) Control and Monitoring System

A landfill gas (LFG) control or monitoring system is not necessary to control and/or recover LFG from the waste mass or to prevent off-site migration as the CKD material does not decompose and generate landfill gas. As such, no LFG system control or monitoring will be installed during closure activities.

#### 2.2.3 Stormwater Control System

Stormwater run-off from the top of the Closed Cell and Closed Phase I Cell landfill will be directed south and east to a collection ditch that runs parallel to a quarry access road. This ditch drains into the quarry and will convey runoff from the 25-year, 24-hour storm event. It will be lined with erosion resistant vegetation over segments where the gradient of the ditch is less than 5 percent. The ditch will be lined with fiber cloth and riprap or will be founded on bedrock over segments where the gradient exceeds 5 percent.

Stormwater run-off from the top of the Phase II Cell will be directed to the east and to the west. Stormwater directed to the east will connect to the existing stormwater ditch adjacent to the quarry access road. Stormwater from directed to the west will drain to the southwest to the quarry.

Stormwater run-off from the CKD landfill will ultimately flow into the quarry where it will flow to the quarry dewatering sump. Stormwater from the quarry dewatering sump is discharged to the Mississippi River through Outfall 001, which is monitored as part of the facilities National Pollution Discharge Elimination System (NPDES) permit.



#### 2.3 Soil Balance

The soil required for the landfill closure was calculated to provide an overall site soil balance. It is anticipated that final cover system described above (2-foot compacted layer and 2-foot vegetative layer) will require approximately 21,250 cubic yards of clayey soils and approximately 21,250 cubic yards of vegetative soils over the approximately 6-acre Active Phase II Cell. The total soil required for final cover (compacted and vegetative cover soils) is estimated at 42,500 cubic yards. Existing stockpiles of soil within the quarry and soils generated from future excavations are anticipated to exceed the quantity necessary for landfill closure. Existing stockpiled soils were previously tested and deemed suitable for use as final cover.

#### 2.4 Final Use

After the site has undergone final closure, the final design grades and cover system of the proposed landfill will allow for the land to be used for open green space. Uses that do not conflict with long-term post-closure care plans for the area may be considered in the future. At this time, significant structures are not planned for development on the completed landfill final cover.

#### 2.5 Survey Plat

Upon completion of final closure of the landfill, the owner/operator will have a licensed surveyor registered in the State of lowa prepare a survey plat of the site. The survey plat will show, at a minimum, the name of the property owner as it appears on the deed; a survey and detailed legal description of the waste limits, the permitted area, and the property boundary; the general types and locations of solid wastes; the depths of fill; the locations of leachate control and groundwater monitoring systems that must be maintained after closure including the length of time that these systems must be maintained; and the location of boundary markers and benchmarks located at the site.

Prior to filing the survey plat with the County Recorder of Deeds, the owner/operator will obtain approval of the survey plat from the IDNR. After receiving approval from the IDNR and before filing with the County Recorder of Deeds, the survey plat will be notarized by a lawful notary public. Filing of the notarized survey plat will take place within 30 days of receipt of IDNR approval. Two copies of the notarized and properly recorded survey plat showing the County Recorder of Deed's seal or stamp, the book and page numbers, and the date of filing will be submitted to the IDNR within 30 days of the date of filing.



#### 3.0 POST-CLOSURE PLAN

The following section describes the Post-Closure Plan for the CKD Landfill and consists of general information; cap maintenance; leachate system operation and maintenance; groundwater and leachate monitoring; miscellaneous site maintenance; recordkeeping; and remedial action.

#### 3.1 General

This Post-Closure Plan includes the maintenance and monitoring activities to be performed at the CKD Landfill for the 30-year post-closure period after IDNR has approved final site closure. The post-closure activities will include maintenance of cover integrity; operation and maintenance of the leachate collection system and groundwater collection system; maintenance, sampling, and testing of groundwater monitoring wells, leachate collection system, and lysimeters; and miscellaneous site maintenance.

Access to the site is limited to the quarry entrance through the use of perimeter fencing. The site entrance is controlled by a lockable gate. Emergency contacts and procedures will be posted at the landfill/site entrance. In the event of an emergency, dial 911 in order to direct the appropriate assistance to the site. Fire, police, and ambulance assistance is available to the site by dialing 911.

#### 3.2 Cover System Maintenance

After the site is closed, the final cover will be inspected on a semi-annual basis for stressed vegetation, poor vegetative coverage, and erosion of the final cover. Final cover system maintenance will consist of filling areas of excessive differential settlement, regrading to control erosion, replacement of eroded cover soils, perimeter drainage channel maintenance, revegetation, weed control, and mowing. Typically, final cover system repairs will be conducted in the spring and fall such that seeding may be effective and not cause further damage to the cover system. Mowing of the facility will be conducted at least annually.

Since the final use for the site is green space, no provisions are needed for additional depth of cover material to allow cultivation and to support vegetation in addition to that required for the final cover.

#### 3.3 Leachate System Operation and Maintenance

Leachate will continue to be collected by the leachate piping within the landfill and transferred to the leachate sump. Leachate will be pumped from the sump and stored in temporary holding tanks located near the quarry office where the leachate will be transferred to haul trucks that will haul the leachate off-site for treatment routed to a leachate pond for storage and evaporation during the post-closure period. The leachate collection system will be operated and maintained during the post-closure care period. Maintenance of the leachate collection system will include pump replacements or repairs and leachate conveyance pipe repairs, as necessary. The anticipated

Continental Closure, Post Closure Buffalo, Iowa



leachate generation for the closed facility is expected to decline significantly overtime upon installation of the final cover system as the CKD material does not retain moisture.

Leachate collection system monitoring and maintenance will include the following:

- Inspecting the system for proper operation
- Cleaning the leachate collection pipes
- Maintaining the leachate pumping system
- Managing leachate disposal

#### 3.4 Groundwater and Leachate Monitoring

Groundwater and leachate will be monitored throughout the 30-year post-closure care period. Sampling and monitoring locations will be inspected during each sampling event. Repairs to the sampling locations will be made, as necessary to maintain a functioning monitoring system.

#### 3.4.1 Groundwater Monitoring

Groundwater monitoring wells will continue to be sampled during the 30-year post-closure care period in accordance with the Hydrologic Monitoring System Plan in place at the time of monitoring and the terms and conditions of the IDNR permit. Semi-annual sampling, analysis, and reporting will be conducted in accordance with the Hydrologic Monitoring System Plan in place at the time of monitoring. The groundwater monitoring system in place at the time of this Plan development consists of 20 groundwater monitoring wells and a single stope well as depicted in Table 1.

Groundwater Well ID	Groundwater Well ID	
MW-1A	MW-1B	
MW-2A	MW-3	
MW-3L	MW-4	
MW-4L	MW-5	
MW-7	MW-11	
MW-12	MW-13	
MW-14	MW-15	
MW-16	MW-16L	
MW-18	MW-19	
MW-20	MW-21	
MW-2CR (stope well)		

 Table 1 – Groundwater Monitoring Network

Groundwater monitoring and reporting will be conducted in accordance with the general requirements contained within IAC 567-115.26 and the most recent Hydrologic Monitoring System Plan. Groundwater monitoring results will be submitted annual to the IDNR in accordance with IAC 567-115.26(8).



#### 3.4.2 Leachate Monitoring

Leachate will continue to be monitored during the 30-year post-closure care period. Leachate samples will be collected in accordance the Hydrologic Monitoring System Plan in place at the time of monitoring and the terms and conditions of the IDNR permit. Semi-annual sampling, analysis, and reporting will be conducted in accordance with the Hydrologic Monitoring System Plan in place at the time of monitoring. The leachate monitoring system in place at the time of this Plan development consists of six monitoring locations as depicted in Table 2.

	•
Monitoring Location ID	Monitoring Location ID
MW-9	MW-10
UL-1	UL-2
UL-3	L-Sump

Table 2 – Leachate	• Monitoring	Locations
--------------------	--------------	-----------

Leachate monitoring and reporting will be conducted in accordance with the general requirements contained within IAC 567-115.26 and the most recent Hydrologic Monitoring System Plan. Leachate monitoring results will be submitted annual to the IDNR in accordance with IAC 567-115.26(8).

#### 3.4.3 Lower Lysimeter Monitoring

The lower lysimeters will continue to be monitored during the 30-year post-closure care period. Lower lysimeter samples will be collected in accordance the Hydrologic Monitoring System Plan in place at the time of monitoring and the terms and conditions of the IDNR permit. Semi-annual sampling, analysis, and reporting will be conducted in accordance with the Hydrologic Monitoring System Plan in place at the time of monitoring. The lower lysimeters in place at the time of this Plan development consists of three monitoring locations as depicted in Table 3.

Lower Lysimeter ID	
LL-1	
LL-2	
LL-3	

 Table 3 – Lower Lysimeter Monitoring Locations

Leachate monitoring and reporting will be conducted in accordance with the general requirements contained within IAC 567-115.26 and the most recent Hydrologic Monitoring System Plan. Leachate monitoring results will be submitted annual to the IDNR in accordance with IAC 567-115.26(8).

#### 3.5 Miscellaneous Site Maintenance

Miscellaneous site maintenance activities will include perimeter fence and gate maintenance, quarry dewatering sump maintenance or replacement, and drainage channel maintenance. The

Continental Closure, Post Closure Buffalo, Iowa



perimeter fences and gates will be maintained and repaired to restrict unauthorized site access. The permanent surveying monuments will be maintained and repaired or replaced, as necessary. The quarry dewatering sump will be maintained, repaired, or replaced, as necessary. The perimeter drainage channels will be maintained and repaired, as necessary. The site roads will be maintained and repaired as necessary to maintain access to features such as the leachate collection systems as well as the environmental monitoring locations.

#### 3.6 Recordkeeping

During the post-closure care period, semi-annual reports will be submitted to IDNR. The reports will contain information concerning the general conditions at the site, groundwater monitoring results, quantity of leachate collected and treated, and other information as required by the closure permit. The locations and elevations of permanent monuments required by IAC 567.115.26(13) will be determined at least once every three years, or more frequently in the event of obvious disturbance of the monument. The semi-annual reports will be provided to the IDNR by April 30 and October 31 each year and cover the preceding 6-month period.

The post-closure care contact for the CKD Landfill will be:

Continental Cement Company Mr. Damion Sadd/Environmental & Public Affairs Manager 301 East Front Street Buffalo, Iowa 52728 Telephone: (563) 328-6204

The Environmental and Public Affairs Manager should be contacted regarding questions or issues with the landfill or access to the landfill. During this period, landfill records will be maintained by Continental. The records will be made available to the IDNR representatives upon request for review.

#### 3.7 Remedial Action

If Continental is required to develop a corrective action or remediation action plan for the CKD Landfill during the life of the landfill or during the post-closure care period, then cost estimates will be prepared and additional financial assurance will be secured as appropriate. At this time, there are no remedial action requirements.

#### 4.0 FINANCIAL ASSURANCE

The most recent closure and post-closure cost estimate and associated financial assurance for the CKD Landfill are contained in Appendix B. The financial assurance instrument for the site has been updated annually in accordance with IAC 567-115.31 requirements. New cost estimates will be submitted for approval and the amount of financial assurance adjusted appropriately as changes in site conditions that impact closure and or post-closure care costs are implemented. If

Continental Closure, Post Closure Buffalo, Iowa



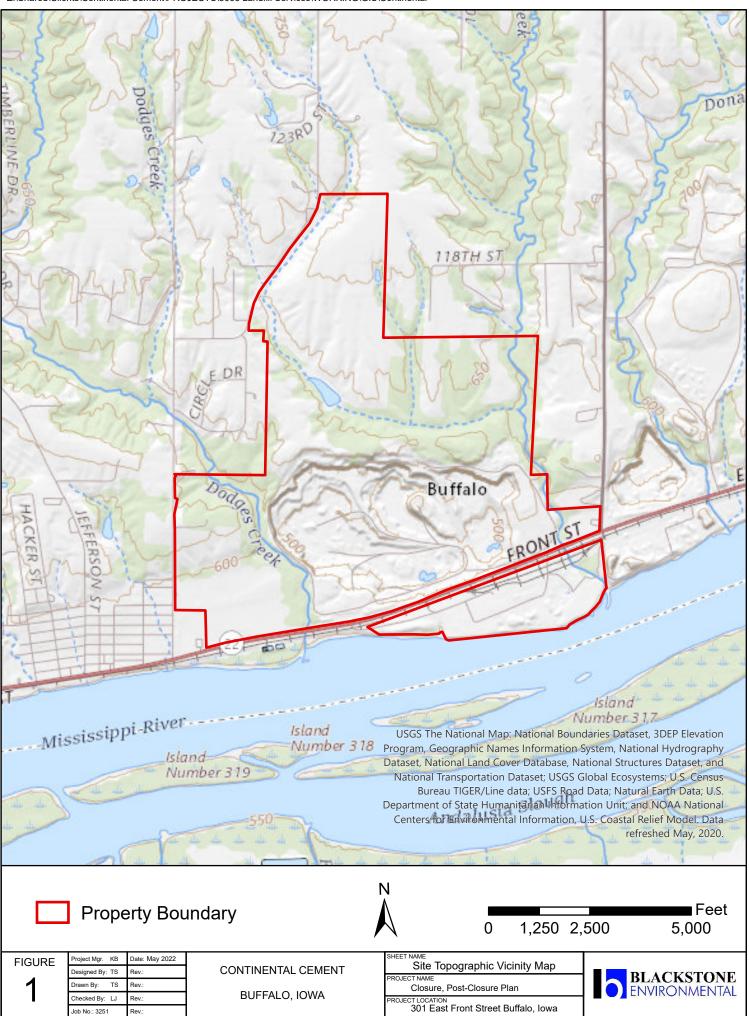
no site conditions impacting costs are completed during a given year, then the most recent closure and post-closure cost estimate will be adjusted annual for inflation.

#### 5.0 LIMITATIONS

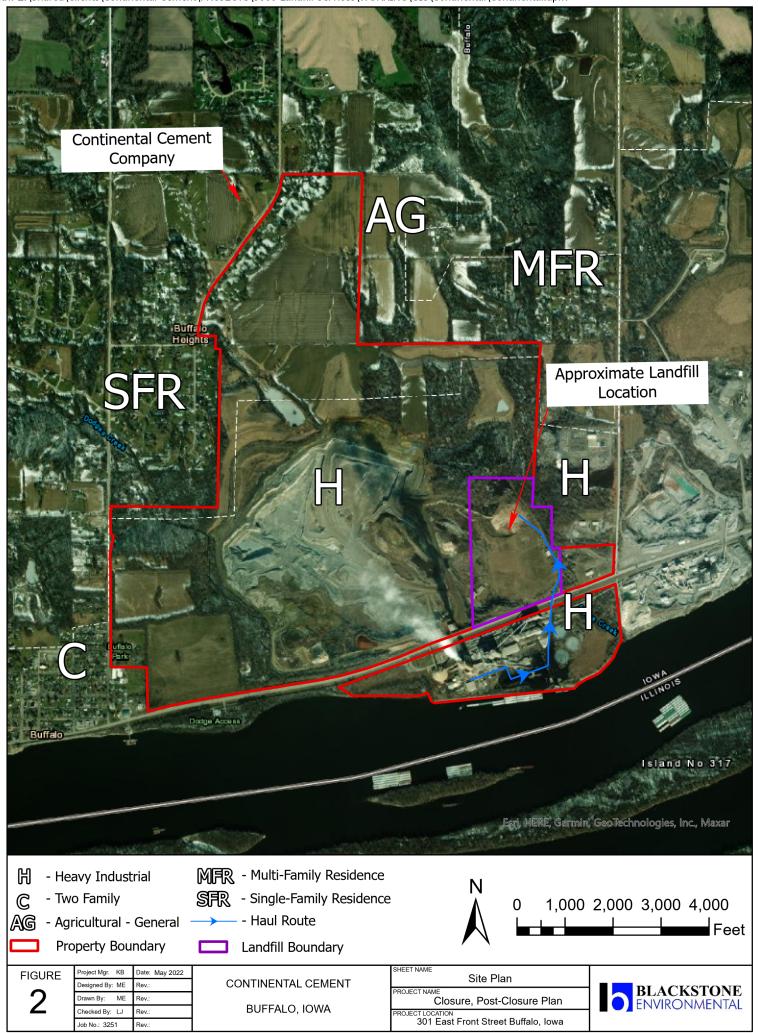
This report was prepared in accordance with that level of skill and care ordinarily exercised by other members of Blackstone's profession practicing in the same locality and under similar conditions when the services were provided. No warranties, express or implied, are intended or made.

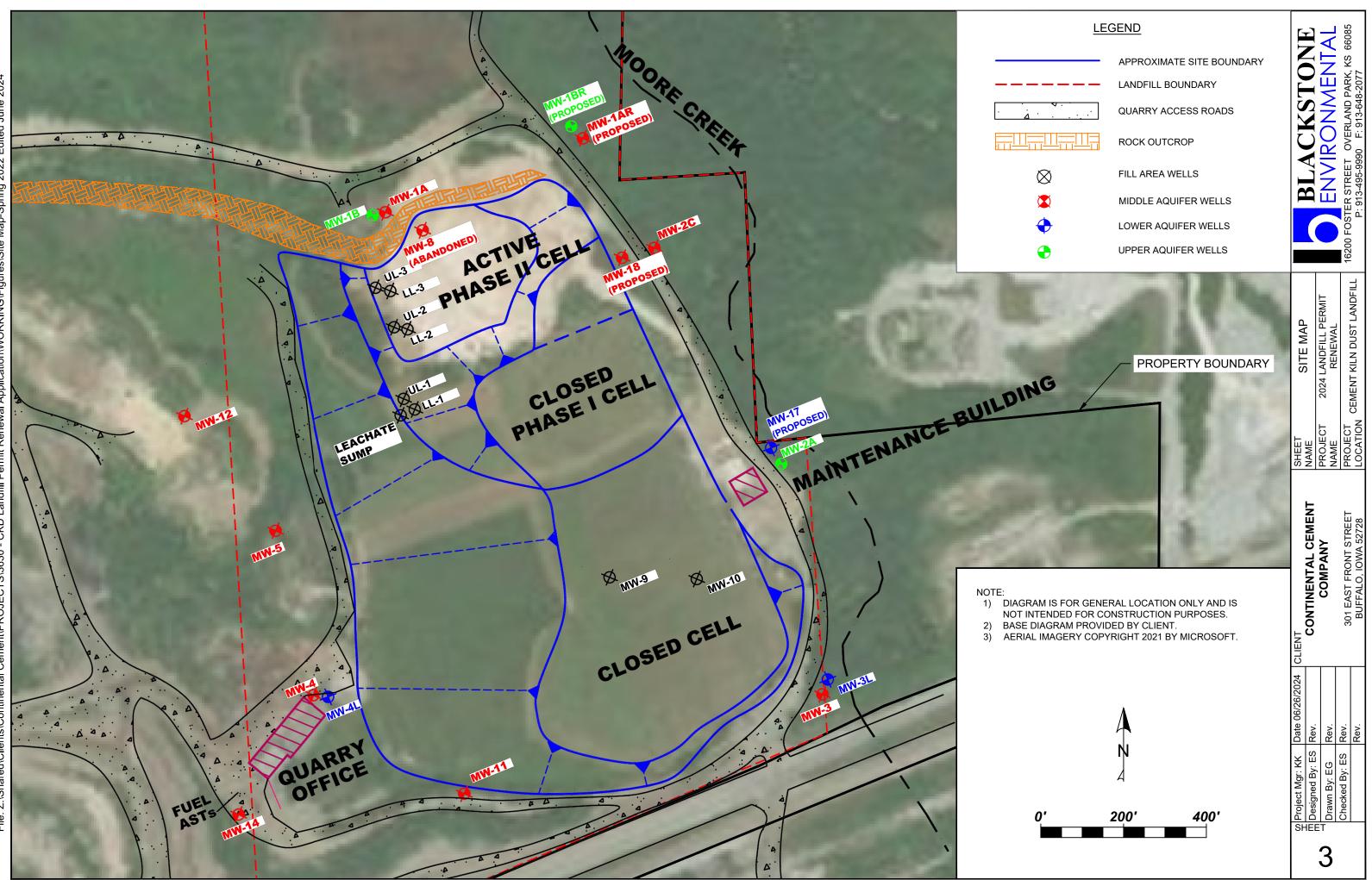
FIGURES

Z:\Shared\Clients\Continental Cement\PROJECTS\3066 Landfill Services\WORKING\GIS\Continental



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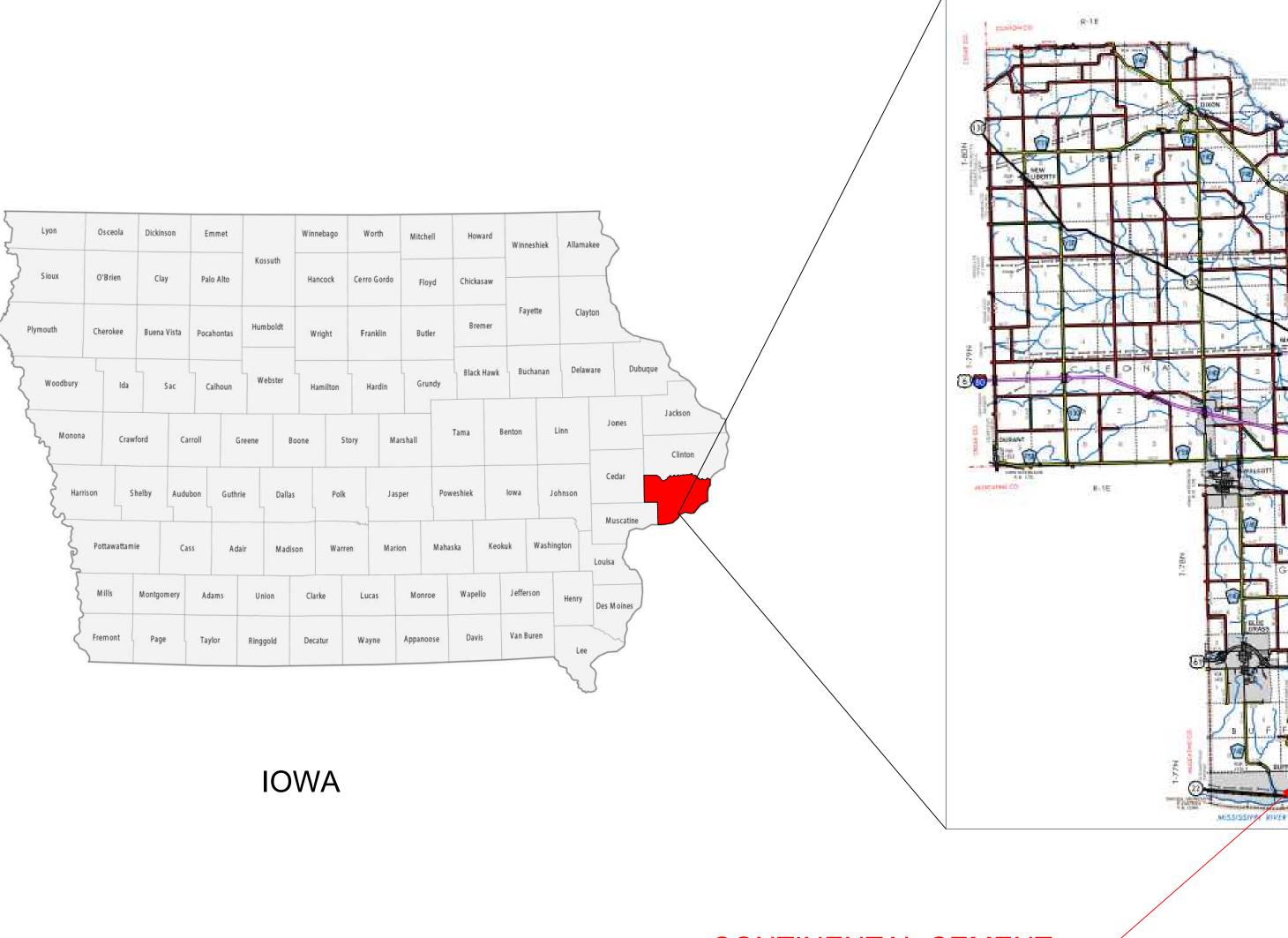




## **APPENDIX A**

**Closure Drawings** 

DRAWING INDEX			
DRAWING NO. TITLE			
0	COVER SHEET		
1	EXISTING CONDITIONS		
2	FINAL COVER PLAN		
3	CROSS-SECTIONS		
4	DETAILS		



# PREPARED FOR:



CONTINENTAL CEMENT 301 EAST FRONT STREET BUFFALO, IA 52728

**PREPARED BY:** 

BLACKSTONE ENVIRONMENTAL

> 1465 41ST STREET, SUITE 13 MOLINE, ILLINOIS 61265

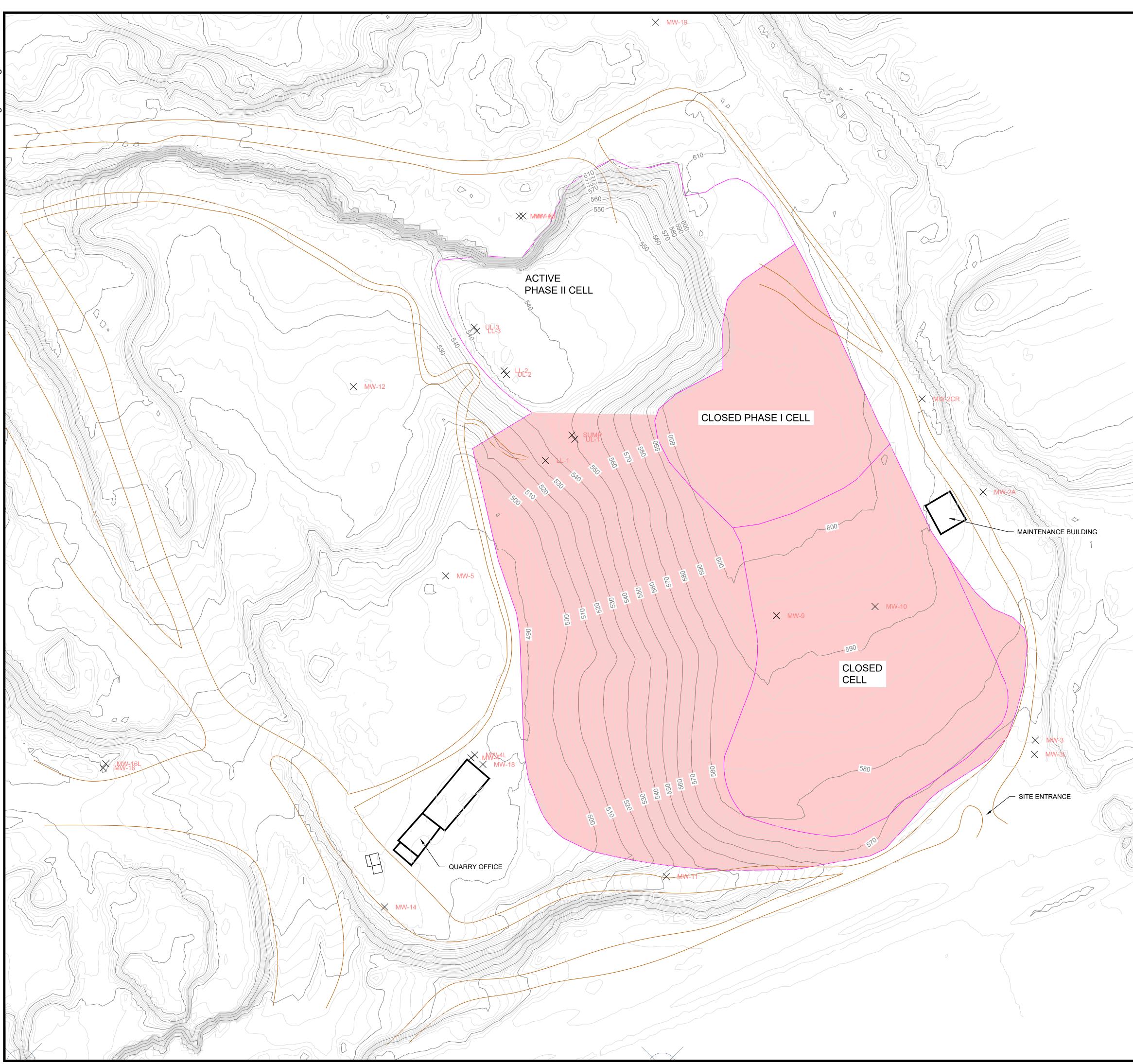
> > PROJECT NO. 3251 MAY 2022

# CLOSURE DRAWINGS CONTINENTAL CEMENT CKD MONOFILL SCOTT COUNTY, IOWA IOWA LANDFILL PERMIT NO. 82-SDP-16-97P MAY 2022

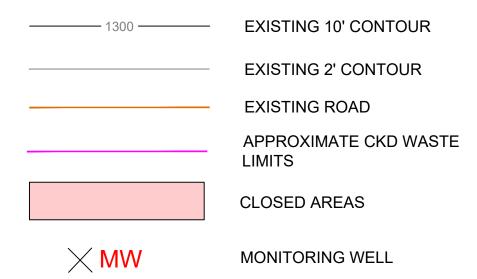
CONTINENTAL CEMENT MONOFILL

# VICINITY MAP

I HEREBY CERTIFY THAT THIS ENGINEERING DOCUMENT WAS PREPARED BY ME OR UNDER MY DIRECT PERSONAL SUPERVISION AND THAT I AM A DULY LICENSED PROFESSIONAL ENGINEER UNDER THE LAWS OF THE STATE OF IOWA. May 31, 2022 SIGNATURE DATE ERIC SONSTHAGEN LICENSE NUMBER: P24844 MY LICENSE RENEWAL DATE IS DECEMBER 31, 2023 SONSTHAGEN P24844 P24844 PAGES OR SHEETS COVERED BY THIS SEAL: SHEETS 0-4

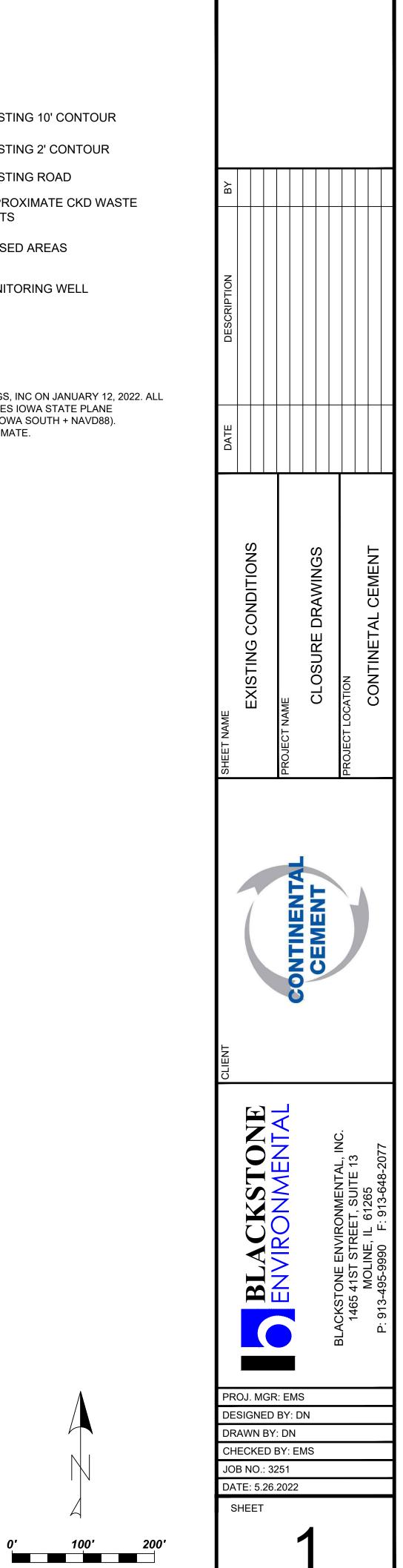


# LEGEND

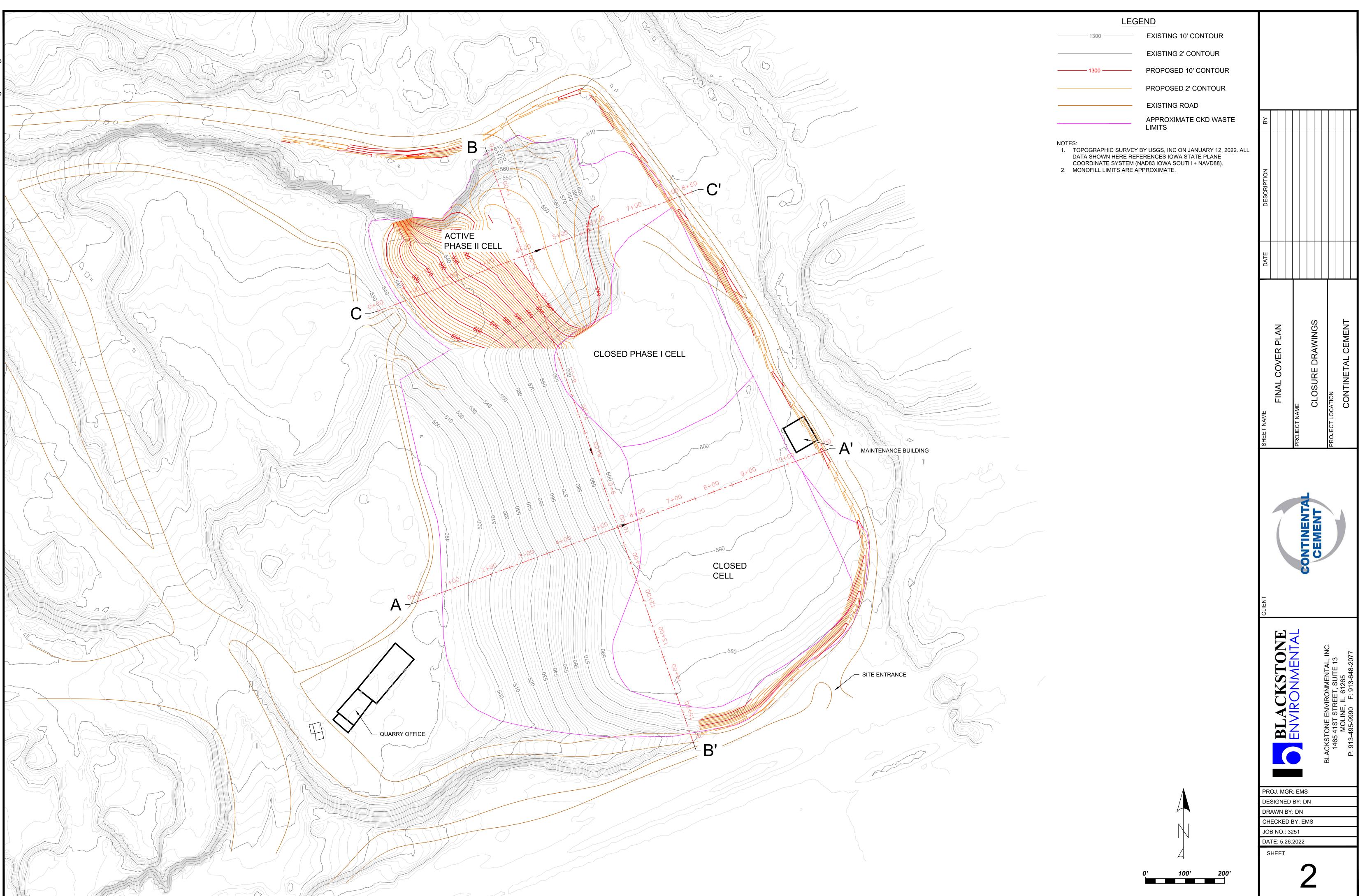


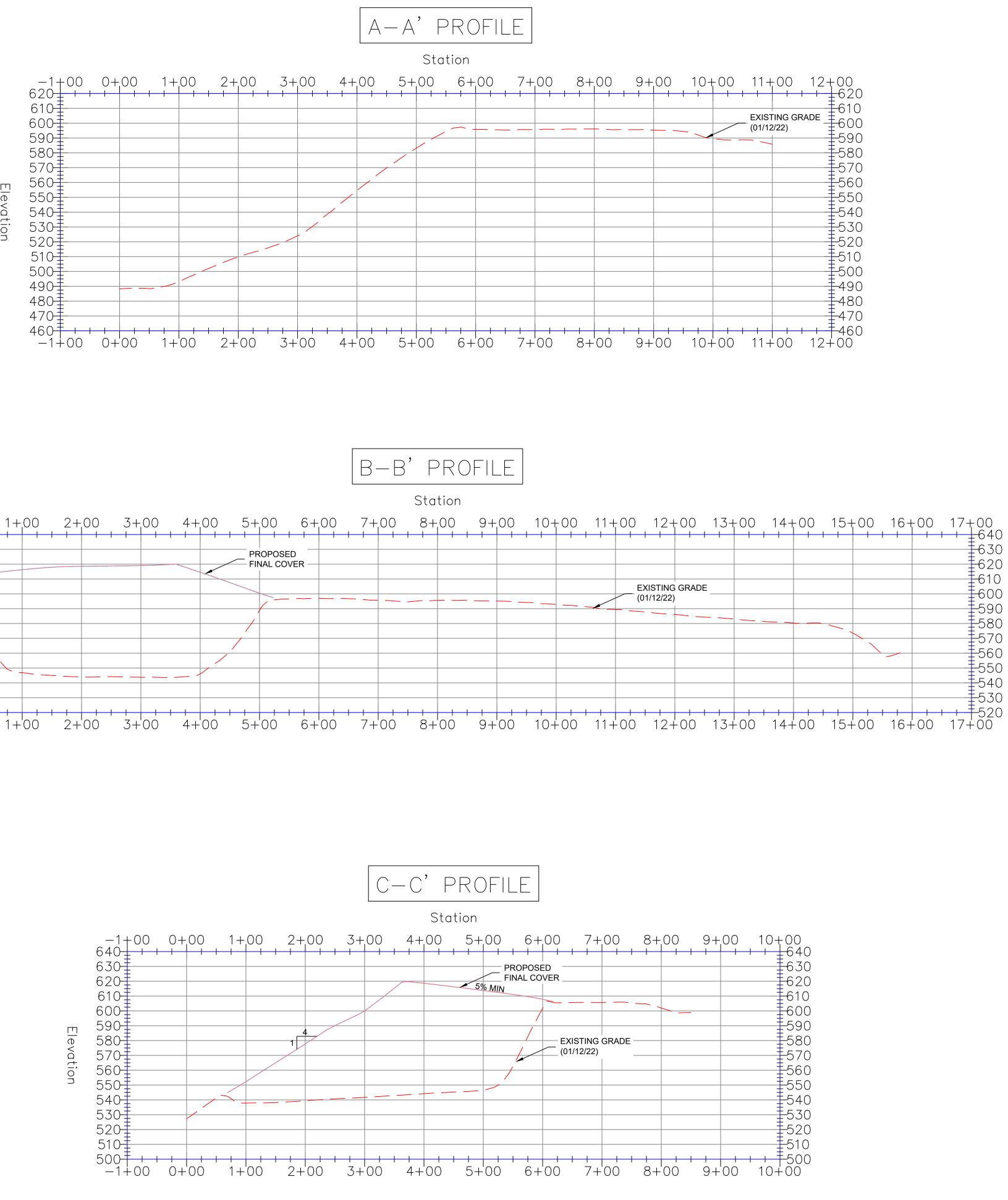
#### NOTES:

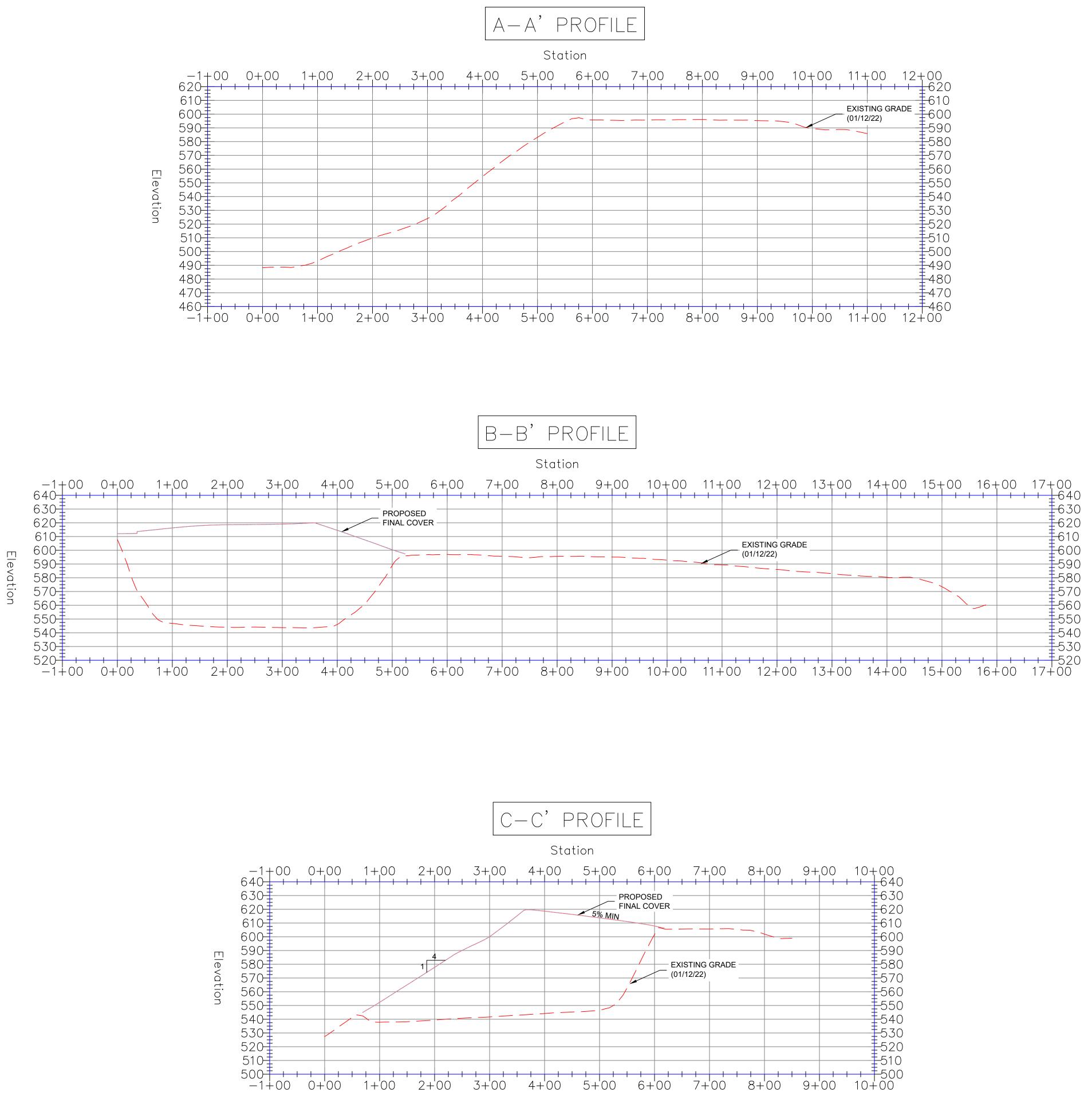
1. TOPOGRAPHIC SURVEY BY USGS, INC ON JANUARY 12, 2022. ALL DATA SHOWN HERE REFERENCES IOWA STATE PLANE COORDINATE SYSTEM (NAD83 IOWA SOUTH + NAVD88).
2. MONOFILL LIMITS ARE APPROXIMATE.

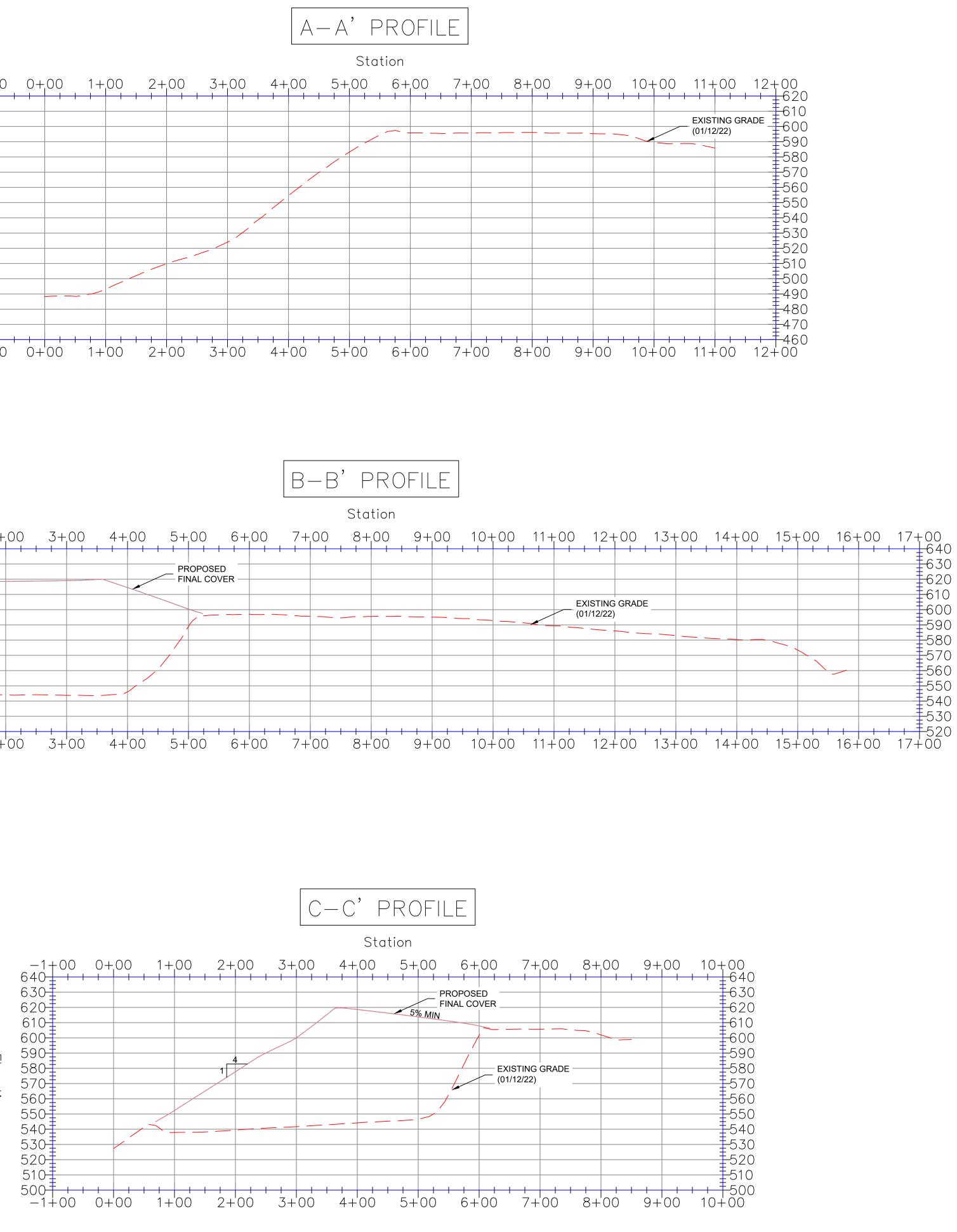


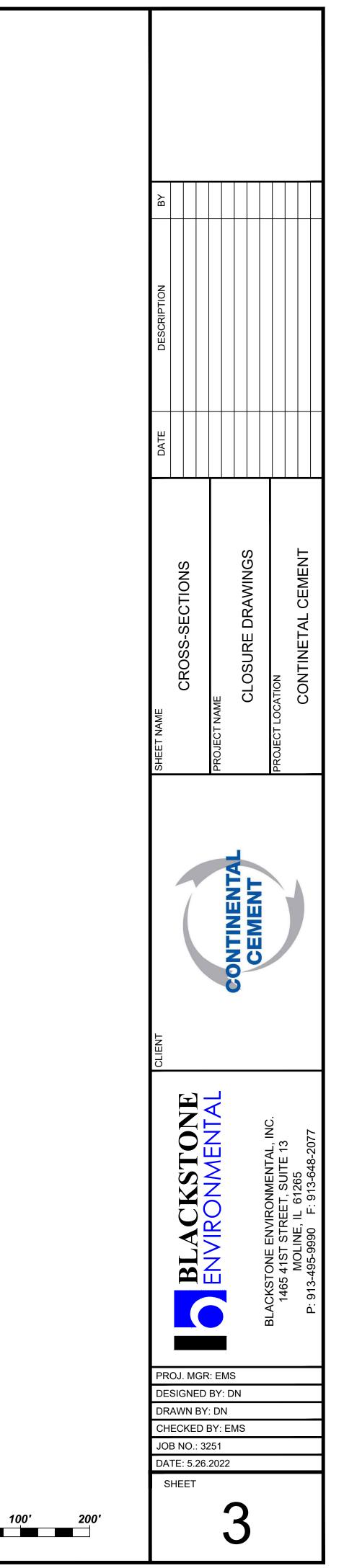
9: D:\CC Closing Drawings

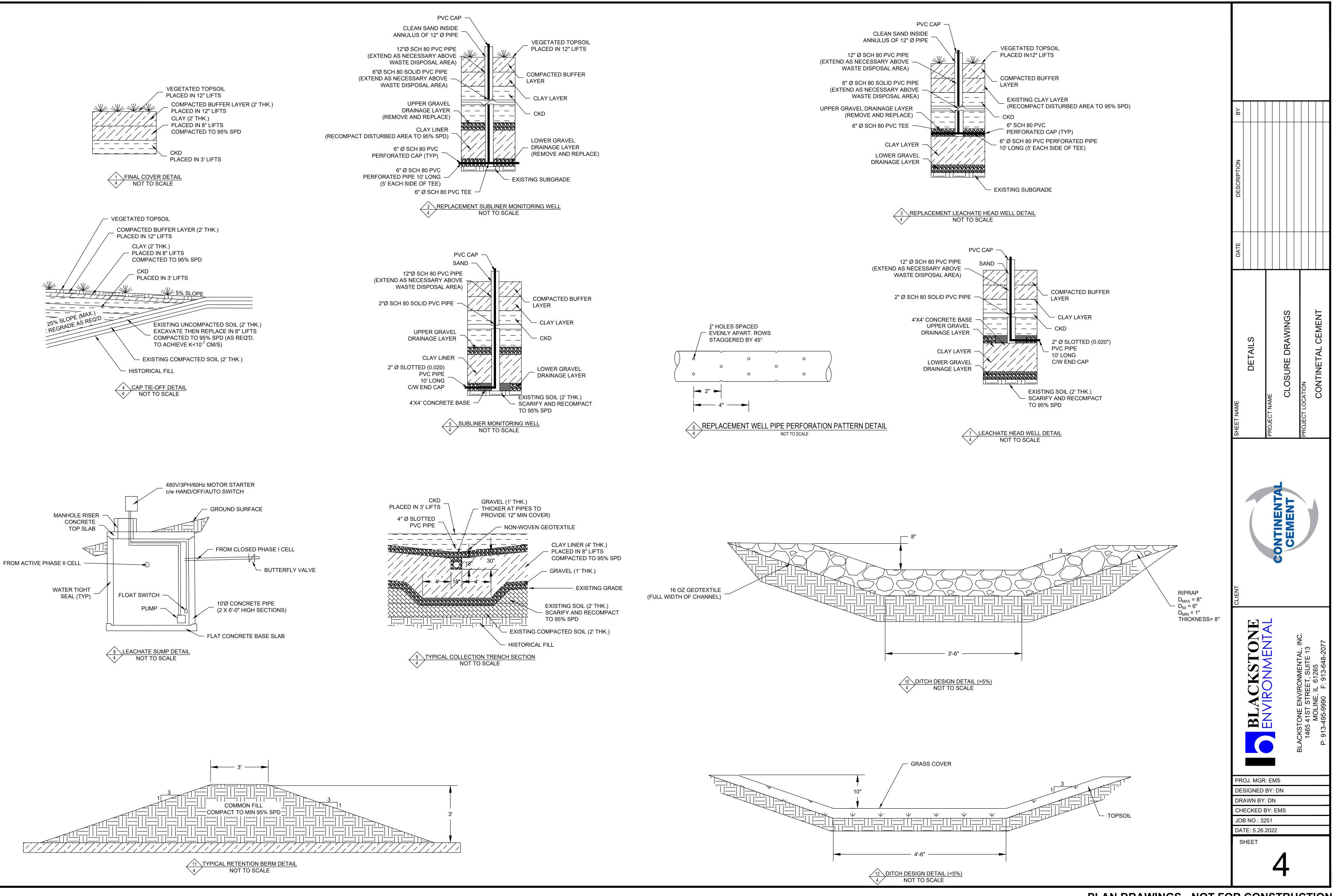












**PLAN DRAWINGS - NOT FOR CONSTRUCTION** 

### **APPENDIX B**

**Closure and Post-Closure Cost Estimate** 



March 28, 2022

Iowa Department of Natural Resources Solid Waste Section Wallace State Office Building 901 East Grand Avenue Des Moines, Iowa 50319-0034

#### RE: Closure/Post-Closure Cost Estimate Continental Cement Company – Davenport Plant CKD Landfill Buffalo, Scott County, Iowa IDNR Permit No. 82-SDP-15-96C and 82-SDP-16-97P

Dear Sir/Madam:

Blackstone Environmental, Inc. (Blackstone) is pleased to submit the closure/post-closure (CPC) cost estimates for the Continental Cement Company Davenport Plant Cement Kiln Dust (CKD) Landfill. This CPC cost estimate has been prepared in general accordance with the requirements of Title 567 Iowa Administrative Code Chapter 115.31 (567 IAC 115.31).

Continental operates a CKD landfill located in Buffalo, Iowa. A portion of the landfill is closed under Iowa Department of Natural Resources (IDNR) Permit No. 82-SDP-15-96C. The rest of the site is operated as a monofill for disposal of CKD under IDNR Permit No. 82-SDP-16-97P.

A summary of the closure and post-closure cost estimates are provided below. Detailed cost estimate tables are provided on the follow pages.



#### Table 1 – Closure and Post-Closure Cost Estimate Summary

Total Closure Costs	\$484,956.09
Total Post-Closure Costs	\$1,051,768.06
Total CPC Costs	\$1,536,724.15

This cost estimate was prepared in accordance with applicable requirements and generally accepted environmental engineering practices.

If you have any questions, please contact Eric Sonsthagen with Blackstone at 402-208-2014 or Damion Sadd with Continental Cement at <u>Damion.Sadd@continentalcement.com</u> or 563-328-6204.

Respectfully, **BLACKSTONE ENVIRONMENTAL, INC.** 

bic Southager

Eric Sonsthagen, P.E. Senior Project Engineer

II AAM

Krista A. Brodersen Senior Project Manager



#### CERTIFICATION

I hereby certifies the portion of this engineering document described below was prepared by me and that I am a licensed Professional Engineer under the laws of the State of Iowa.



License No. P24844

Pages covered by this seal: All

Eric Sonsthagen, P.E.

License Renewal Date: 12/31/2023

Closure Cost Estimate - Continental Cement Com	pany			
		FACILITY OWNER:	Continental Ceme	nt Company
		FACILITY NAME:	Davenport Plant C	CKD Landfill
		DATE:	3/10/2022	
		PERMIT NUMBER:	82-SDP-16-97P	
		ESTIMATOR:	Eric Sonsthagen, P	P.E.
Permit No.: 82-SDP-16-97P				
ITEM	QUANTITY	UNITS	UNIT COST	COST
INITIAL CLOSURE PREPARATION				
CPC Plan Document Revisions	1	Each	\$7,037.24	\$7,037.24
FINAL COVER				
Site preparation earthwork and grading for final cover	5	Days	\$2,463.02	\$12,315.12
Final cover construction	18,000	СҮ	\$12.67	\$228,064.41
VEGETATIVE LAYER				
Final cover vegetation soil	14,000	CY	\$11.25	\$157,525.97
Seeding, mulching, and fertilizing	4.1	ACRE	\$1,407.45	\$5,770.52
EROSION CONTROL				
Erosion Control structures, ponds, terraces	5	Days	\$2,463.02	\$12,315.12
GROUNDWATER MONITORING SYSTEM				
Upgrade or repair existing wells	1	EACH	\$1,407.45	\$1,407.45
Well abandonment	0	EACH	\$0.00	\$0.00
LEACHATE COLLECTION SYSTEM			`	
Leachate system modifications	1	EACH	\$4,222.27	\$4,222.27
FACILITY OPERATIONS				
Facility modifications	1	EACH	\$14,074.49	\$14,074.49
PROFESSIONAL SERVICES				
Engineering Services	1	EACH	\$21,111.77	\$21,111.77
ADMINISTRATION AND CONTINGENCY				
Legal, Financial, and Administration Services	1	EACH	\$14,074.49	\$14,074.49
Closure Compliance Documentation	1	EACH	\$7,037.23	\$7,037.23
		Total	Closure Costs	\$ 484,956.09

Post-Closure Cost Estimate - Continental Ceme	nt Company			
	• •	FACILITY OWNER	: Continental Cement Co	ompany
		FACILITY NAM	E: Davenport Plant CKD L	andfill
	DATE: <u>3/10/2022</u>			
		PERMIT NUMBE	R: 82-SDP-16-97P	
		ESTIMATO	R: Eric Sonsthagen, P.E.	
Permit No.: 82-SDP-16-97P				
ITEM	QUANTITY	UNITS	UNIT COST	COST
MAINTENANCE ITEMS				
General Maintenance	30	Years	\$1,548.19	\$46,445.82
Cap and Vegetation Maintenance	30	Years	\$3,096.38	\$92,891.31
Drainage and Erosion Control Maintenance	30	Years	\$0.00	\$0.00
Waste Systems Maintenance	30	Years	\$0.00	\$0.00
Gas Control Maintenance	30	Years	\$0.00	\$0.00
Leachate Control Maintenance	30	Years	\$2,500.00	\$75,000.00
Groundwater Monitoring System Maintenance	30	Years	\$1,407.45	\$42,223.35
LEACHATE SYSTEM				
Leachate Management and Disposal	30	Years	\$0.00	\$0.00
Leachate Control Performance Evaluations	30	Years	\$0.00	\$0.00
GROUNDWATER MONITORING SYSTEM				
Groundwater Monitoring Performance Evaluations	30	Years	\$2,814.87	\$84,446.07
Groundwater Monitoring and Reporting	30	Years	\$18,296.86	\$548,905.82
INSPECTIONS			`	
Facility Inspections	30	Years	\$2,814.87	\$84,446.07
ADMINISTRATION AND ENGINEERING				
Legal, Financial, and Administration Services	1	EACH	\$14,074.49	\$14,074.49
Engineering Services	1	EACH	\$21,111.77	\$21,111.77
Financial Assurance Accounting	30	Years	\$1,407.45	\$42,223.35
		Total Post	-Closure Costs \$	1,051,768.06

## Industrial Monofill Financial Assurance Report Form

#### Section 1: FACILITY INFORMATION (please print or type)

Information Requested	
Facility Name	Davenport Plant CKD Landfill
Permitted Agency/Entity	Continental Cement Company
Permit Number	82-SDP-16-97P

#### Section 2: CLOSURE/POSTCLOSURE OR CORRECTIVE ACTION COST ESTIMATES

Information Requested	Cost Estimate	Date of Cost Estimate
Updated Closure Cost Estimate	\$ 484,956.09	3/10/22
Updated Postclosure Cost Estimate	\$ 1,051,768.06	3/10/22
Initial or Updated Corrective Action Cost Estimate	\$	

\*Attach closure/postclosure cost estimate(s) signed and certified by an lowa-licensed professional engineer. Cost estimates shall include, at a minimum, each of the cost line items defined in 115.31(3)"c" for closure and 115.31(4)"c" for postclosure. Please provide closure and/or postclosure site area acreage information with the estimates.

Provide a cost estimate for corrective action only if corrective action is required and a corrective action plan has been approved by the Department. Attach the corrective action cost estimate signed and certified by an Iowa-licensed professional engineer. The cost estimate shall account for total costs of the activities described in the approved corrective action plan for the corrective action period.

#### Section 3: FACILITY WASTE TONNAGE INFORMATION

Information Requested	Tons
Remaining permitted capacity as of the beginning of permit holder's current fiscal year	747,088
Amount of waste disposed of at the facility during the prior year	2,531

#### Section 4: PROOF OF COMPLIANCE

Publicly Owned Industrial Monofills	(ATTACH AUDIT REPORT)
Owner's Most Recent Annual Audit Report	
Prepared by:	
For fiscal year ending:	_
Privately Owned Industrial Monofills	(ATTACH AFFIDAVIT)
Attach owner/operator's affidavit indicating that an annual review has be accountant to determine whether the privately owned monofill is in comp	• • •

accountant to determine whether the privately owned monofill is in compliance with IAC 567 Chapter 115. The affidavit shall state the name of the certified public accountant, the dates and conclusions of the review, and the steps taken to rectify any deficiencies identified by the accountant.

#### Section 5: FINANCIAL ASSURANCE INSTRUMENT

Type and Value of Financial Assurance Instrument(s)		(ATTACH INSTRUMENT(	s)
Assurance Instrument	Establishment Date	Mechanism Covers	Instrument Value
Trust Fund 567 IAC 115.31(6)"a"		Closure 🗌 Postclosure 🔲 Corrective Action 🗌	\$
Surety Bond 567 IAC 115.31(6)"b"	March 1, 2016	Closure 🛛 Postclosure 🖾 Corrective Action 🗌	\$ 1,536,724.15
Letter of Credit 567 IAC 115.31(6)"c"		Closure 🗌 Postclosure 🗌 Corrective Action 🗌	\$
Insurance 567 IAC 115.31(6)"d"		Closure 🗌 Postclosure 🗌 Corrective Action 🗌	\$
Corporate Financial Test 567 IAC 115.31(6)"e"		Closure 🗌 Postclosure 🗌 Corrective Action 🗌	\$
Local Gov't. Financial Test 567 IAC 115.31(6)"f"		Closure 🗌 Postclosure 🗌 Corrective Action 🗌	\$
Corporate Guarantee 567 IAC 115.31(6)"g"		Closure 🗌 Postclosure 🗌 Corrective Action 🗌	\$
Local Gov't Guarantee 567 IAC 115.31(6)"h"		Closure 🗌 Postclosure 🗌 Corrective Action 🗌	\$
Local Gov't. Dedicated Fund 567 IAC 115.31(6)"i"		Closure 🗌 Postclosure 🗌 Corrective Action 🗌	\$

#### **Section 7: FUND PAYMENTS** (only if using dedicated or trust fund)

Completion of the following fund information complies with the annual financial statement requirements of IAC 567 115.31(3)"a" and 115.31(4)"a" by indicating the current balance(s) of the dedicated/trust fund and the projected amount(s) to be deposited in the fund(s).

Under "Beginning Balance", please state the fund balance 30 days after the start of the previous fiscal year, for "Ending Balance", indicate the fund balance 30 days after the close of the previous fiscal year, and for "Projected Deposit", indicate the amount to be deposited within 30 days of the close of the permit holder's fiscal year.

Information Requested	Beginning Balance	Ending Balance	Projected Deposit
Dedicated Fund Balance (see formula below)	\$	\$	\$
Trust Fund Balance (see formula below)	\$	\$	\$

**Formula for Projected Deposits** 

Dedicated/Trust Fund

<u>CE - CB</u> Y

Where "CE" is the closure or postclosure cost estimate, "CB" is the balance 30 days after close of the previous fiscal year, and "Y" is number of years remaining in the pay-in period.

If needed, the space below can be used to show calculations for projected deposit(s)

Γ

SUBMITTAL OF THIS COMPLETED AND ENDORSED FORM A NOTIFICATION AND PROOF OF PERMIT HOLDE			
Damion Sadd	Environmental and Public Affairs Manager		
Name of Official	Title		
Continental Cement Company			
Agency/Entity			
301 E. Front Street			
Address			
Buffalo	ΙΑ	52728	
City	State	Zip	
563-328-6204			
Telephone	Fax		
Damion.Sadd@continentalcement.com			
Email Address			

Signature of Official	Title	Date

Questions? Contact Bill Blum at (515) 725-8376 or Bill.Blum@dnr.iowa.gov

To be attac	hed to and form a part of	
Bond No.	019052863	
dated effective	March 1, 2016	
cheelive	(MONTH-DAY-YEAR)	
executed by	Continental Cement Co., LLC	, as Principal,
	(PRINCIPAL)	
and by	Liberty Mutual Insurance Company , as Surety,	
in favor of	Iowa Department of Natural Resources	
	(OBLIGEE)	
	ration of the mutual agreements herein contained the Principal and the Surety hereby consent to changing	
The Bond A	mount from:	
Six Hundre	d Thirty-nine Thousand Six Hundred Fifty-two & 95/100 Dollars (\$639,652.95)	
<b>T</b>		
To:	Five Hundred Thirty-six Thousand Seven Hundred Twenty-four & 15/100 Dollars (\$1,536,724.15)	
Nothing b	erein contained shall vary, alter or extend any provision or condition of this bond except as herein expressly state	ed
This rider is effective	March 16, 2022 (MONTH-DAY-YEAR)	
Clanadian	d Sealed March 16, 2022	
Signed an	(MONTH-DAY-YEAR)	
	Continental Cement Co., LLC	
_	(PRINCIPAL)	
B	(PRINCIPAL) DOV (D LOOMES: PRESIDENT	
	Liberty Mutual Insurance Company	
	(SURETY)	
E	y: Share a start of the start o	
	Linda Lee Nipper, Attorney-in-Fact	
-0443/GEEF 10/9	9	



This Power of Attorney limits the acts of those named herein, and they have no authority to bind the Company except in the manner and to the extent herein stated.

> Liberty Mutual Insurance Company The Ohio Casualty Insurance Company West American Insurance Company

Certificate No: 8204866

please call 610-832-8240 or email HOSUR@libertymutual.com

bond and/or Power of Attorney (POA) verification inquiries,

For

#### POWER OF ATTORNEY

KNOWN ALL PERSONS BY THESE PRESENTS: That The Ohio Casualty Insurance Company is a corporation duly organized under the laws of the State of New Hampshire, that Liberty Mutual Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and West American Insurance Company is a corporation duly organized under the laws of the State of Massachusetts, and the s organized under the laws of the State of Indiana (herein collectively called the "Companies"), pursuant to and by authority herein set forth, does hereby name, constitute and appoint, Linda Lee Nipper

each individually if there be more than one named, its true and lawful attorney-in-fact to Salt Lake City all of the city of Utah . state of make, execute, seal, acknowledge and deliver, for and on its behalf as surety and as its act and deed, any and all undertakings, bonds, recognizances and other surety obligations, in pursuance of these presents and shall be as binding upon the Companies as if they have been duly signed by the president and attested by the secretary of the Companies in their own proper persons.

IN WITNESS WHEREOF, this Power of Attorney has been subscribed by an authorized officer or official of the Companies and the corporate seals of the Companies have been affixed thereto this 15th day of February, 2021.



Liberty Mutual Insurance Company The Ohio Casualty Insurance Company West American Insurance Company

lary d Bv:

David M. Carey, Assistant Secretary

STATE OF PENNSYLVANIA COUNTY OF MONTGOMERY

On this 15th day of February, 2021, before me personally appeared David M. Carey, who acknowledged himself to be the Assistant Secretary of Liberty Mutual Insurance Company, The Ohio Casualty Company, and West American Insurance Company, and that he, as such, being authorized so to do, execute the foregoing instrument for the purposes therein contained by signing on behalf of the corporations by himself as a duly authorized officer.

IN WITNESS WHEREOF, I have hereunto subscribed my name and affixed my notarial seal at King of Prussia, Pennsylvania, on the day and year first above written.

Teresa Pastella, Notary Public

Commission number 1126044

PAS Commonwealth of Pennsylvania - Notary Seal Montgomery County My commission expires March 28, 2025 OF RY PI Member, Pennsylvania Association of Notaries

Teresa Pastella

March

day of

This Power of Attorney is made and executed pursuant to and by authority of the following By-laws and Authorizations of The Ohio Casualty Insurance Company, Liberty Mutual Insurance Company, and West American Insurance Company which resolutions are now in full force and effect reading as follows:

ARTICLE IV - OFFICERS: Section 12. Power of Attorney.

Any officer or other official of the Corporation authorized for that purpose in writing by the Chairman or the President, and subject to such limitation as the Chairman or the President may prescribe, shall appoint such attorneys-in-fact, as may be necessary to act in behalf of the Corporation to make, execute, seal, acknowledge and deliver as surety any and all undertakings, bonds, recognizances and other surety obligations. Such attorneys-in-fact, subject to the limitations set forth in their respective powers of attorney, shall have full power to bind the Corporation by their signature and execution of any such instruments and to attach thereto the seal of the Corporation. When so executed, such instruments shall be as binding as if signed by the President and attested to by the Secretary. Any power or authority granted to any representative or attorney-in-fact under the provisions of this article may be revoked at any time by the Board, the Chairman, the President or by the officer or officers granting such power or authority.

ARTICLE XIII - Execution of Contracts: Section 5. Surety Bonds and Undertakings.

Any officer of the Company authorized for that purpose in writing by the chairman or the president, and subject to such limitations as the chairman or the president may prescribe, shall appoint such attorneys-in-fact, as may be necessary to act in behalf of the Company to make, execute, seal, acknowledge and deliver as surety any and all undertakings, bonds, recognizances and other surety obligations. Such attorneys-in-fact, subject to the limitations set forth in their respective powers of attorney, shall have full power to bind the Company by their signature and execution of any such instruments and to attach thereto the seal of the Company. When so executed such instruments shall be as binding as if signed by the president and attested by the secretary.

Certificate of Designation - The President of the Company, acting pursuant to the Bylaws of the Company, authorizes David M. Carey, Assistant Secretary to appoint such attorneysinfact as may be necessary to act on behalf of the Company to make, execute, seal, acknowledge and deliver as surety any and all undertakings, bonds, recognizances and other surety obligations.

Authorization - By unanimous consent of the Company's Board of Directors, the Company consents that facsimile or mechanically reproduced signature of any assistant secretary of the Company, wherever appearing upon a certified copy of any power of attorney issued by the Company in connection with surety bonds, shall be valid and binding upon the Company with the same force and effect as though manually affixed.

I, Renee C. Llewellyn, the undersigned, Assistant Secretary, of Liberty Mutual Insurance Company, The Ohio Casualty Insurance Company, and West American Insurance Company do hereby certify that this power of attorney executed by said Companies is in full force and effect and has not been revoked. 2022

16th IN TESTIMONY WHEREOF, I have hereunto set my hand and affixed the seals of said Companies this





**APPENDIX G** 

**Emergency Response and Remedial Action Plan** 





# Emergency Response and Remedial Action Plan (ERRAP)

Continental Cement Davenport Plant CKD Landfill 301 East Front Street Buffalo, Iowa IDNR Landfill Permit Number 82-SDP-16-97P

# Prepared for:

Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by: Blackstone Environmental, Inc. 16200 Foster Street Overland Park, Kansas 66085



August 30, 2024



EMERGENCY RESPONSE AND REMDIAL ACTION PLAN CONTINENTAL CEMENT DAVENPORT PLANT CKD LANDFILL 301 EAST FRONT STREET BUFFALO, IOWA IDNR LANDFILL PERMIT NUMBER 82-SDP-16-97P

Prepared for: Continental Cement 301 East Front Street Buffalo, Iowa 52728

Prepared by:

Maren Williams

Maren Williams Project Engineer

**Reviewed by:** 

Kyle Kukuk, P.E. Senior Project Manager

#### TABLE OF CONTENTS

Sectio	on	Page
TABL	E OF CONTENTS	ii
1.0	FACILITY INFORMATION	1
2.0	REGULATORY REQUIREMENTS	1
3.0	EMERGENY RESPONSE AND REMEDIAL ACTION PLAN	2
3.1	Failure of Utilities	2
3.2	Weather Related Events	2
3.3	Fires and Explosions	2
3.4	Regulated Waste Spills and Releases	2
3.5	Hazardous Material Spills and Releases	3
3.6	Mass Movement of Land and Waste	3
3.7	Emergency and Release Notifications and Reporting	4
3.8	Emergency Waste Management Procedures	4
3.9	Primary Emergency Equipment Inventory	4
3.10	) Emergency Aid	4
3.11	I Training	5

#### APPENDICES

A Figures

#### Page



#### 1.0 FACILITY INFORMATION

Continental Cement Company, LLC (Continental) is located at 301 Front Street in Buffalo, Scott County, Iowa (Site). Quarrying and manufacturing of Portland cement products have been conducted at the Continental facility since 1924 and other uses are not anticipated in the future. The cement manufacturing process includes the heating of limestone with silica, alumina, and iron minerals to form clinker. The clinker (nodules of sintered material) is ground into a fine powder and mixed with gypsum to form cement. As part of the manufacturing process, removal of particulate is required to control the composition of the cement product. This material is known as cement kiln dust (CKD). Continental Cement Company operates an approximately 20-acre monofil for the disposal of CKD. The southern portion of the monofill has been filled to original grade and closed in general accordance with the requirements of the Iowa Department of Natural Resources (IDNR) Permit Number 82-SDP-15-96C. An active monofill disposal cell (Phase II) is operated under IDNR Permit Number 82-SDP-16-97P. The amount of CKD per day disposed at the monofill varies by day. Continental continues to operate with the overall goal of minimizing landfilled CKD and beneficially reusing material when able.

The Continental facility is located approximately four miles west of Davenport, Iowa within Sections 14,15,22, and 23, of Township 77 North, - Range 2 East (Buffalo Township), Scott County as shown on the attached Figure 1, Appendix A. The facility has been in operation, under various ownership, from 1924 for the quarrying of limestone rock and the manufacture of Portland cement. The CKD landfill is located in an inactive portion of the quarry approximately 2000 feet east of the active quarry area and comprises approximately 20 acres. A site diagram of the landfill is attached as Figure 2, Appendix A.

The Certified Operator responsible for the operation of the project is as follows:

Damion Sadd, Environmental Manager 301 East Front Street P.O. Box 690 Buffalo, IA 52728 (563)328-6204

#### 2.0 REGULATORY REQUIREMENTS

In accordance with Iowa Code section 455B.306(6)(d) an Emergency Response and Remedial Action Plan (ERRAP) was submitted as part of the December 27, 2021, permit renewal application. Condition X.2.h of the new permit issued by IDNR on January 6, 2022, required submission of a revised ERRAP for subsequent permit renewal applications.



#### 3.0 EMERGENY RESPONSE AND REMEDIAL ACTION PLAN

#### 3.1 Failure of Utilities

The landfill is utilized for the disposal of CKD, which is a byproduct manufactured at the same site. Since no utilities are located within the landfill, operations at the plant will also be affected if a failure of utilities occurs. Due to this fact, it is possible to cease operations at the landfill, if necessary, without adversely affecting CKD storage and disposal for short-term and long-term events.

#### 3.2 Weather Related Events

Disposal operations of CKD are primarily performed during winter when tornadoes, windstorms, intense rainstorms and erosion, lightning strikes, and flooding are historically not factors. Because the landfill is utilized for the disposal of CKD, which is manufactured the same site, if weather related events occur, operations at the plant will also be affected. Due to this fact, it is possible to cease operations at the landfill, if necessary, without adversely affecting CKD storage and disposal.

#### 3.3 Fires and Explosions

The CKD landfill is a monofil constructed and operated to dispose of CKD, a material generated through the manufacture of Portland cement. This material is created in a pyro processing system at temperatures in excess of 2600°F. Once the material leaves the pyro processing system, it has been thoroughly fired, therefore, CKD as a landfilled material being stored, transported, unloaded, or placed cannot: Be altered by fire, support a flame, be susceptible to creating an explosion, or assist in a runaway reaction needed to generate an explosion.

There are no buildings, equipment, utilities, stored fuels, facilities, or working areas located within the landfill that can catch on fire. CKD does not break down to form methane gas, so methane gas does not accumulate in the landfill and lead to explosive atmospheres.

#### 3.4 Regulated Waste Spills and Releases

Continental's current operation procedures were created to minimize the release of CKD to the ambient air during storage, transport, unloading, and placement of the material. These procedures include:

- After processing, CKD is stored within an enclosed structure (e.g., silo).
- During the process of loading for transport to the landfill, CKD is conditioned with water to minimize dusting during transport and placement.



- Conditioned CKD tends to agglomerate in the truck which makes it less vulnerable to spillage during transport.
- Employees operating landfill transport trucks are trained in the correct operating procedures, which include instruction regarding the amount of material suitable for one truckload. Employees are encouraged not to overfill trucks to ensure that material does not leave the truck during transport prior to unloading at the landfill.
- The time between transport and placement in the landfill is minimized to reduce drying time which could lead to wind erosion during placement.
- Employees operating landfill placement equipment are trained in the correct operating procedures, which include instruction regarding proper placement of material in the landfill.
   Employees are aware that CKD is not to be pushed into the bermed sides of the landfill, ensuring that all placed material is well contained withing the landfill bed.
- The landfill is inspected weekly to ensure that CKD is not being released to the surface water including the quarry sump and that the CKD is well within the bermed area so that releases do not occur during storm events.
- A four-foot clay liner compacted to 1x10-7 cm/sec is in place underlying the CKD material to prevent releases to the groundwater.
- Monthly water level monitoring and semi-annual sampling is conducted to monitor for CKD release to the groundwater utilizing wells located both inside and outside of the landfill.

#### 3.5 Hazardous Material Spills and Releases

The CKD landfill is a monofil constructed and operated to dispose of CKD, a material generated through the manufacturing of Portland cement. This material is created in a pyro processing system at temperatures in excess of 2600°F. Once the material leaves the pyro processing system, it has been thoroughly fired. Only CKD, a non-hazardous solid waste, is disposed of at the facility. Except for small quantities of fuels, oils, and other materials contained in transport vehicles and earth moving equipment, hazardous materials are not stored, used, or disposed of at the landfill site.

#### 3.6 Mass Movement of Land and Waste

Due to the cementitious nature of the conditioned CKD, the material tends to bind together when placed at the landfill forming a relatively uniform and solid deposit. The material is able to stand at a relatively steep angle of repose with negligible risk of slumping or slope failure. Further, the material is relatively impervious thereby reducing the likelihood of saturation which could reduce the shear strength and lead to slope instability.

Employees with duties associated with the storage, handling, transport, or disposal of CKD are trained to place CKD in a manner which will reduce the likelihood of slope failures, waste shifts,



and waste subsidence. Transport vehicle drivers are instructed to place material at a safe distance back from the edge of the active cell to avoid surcharging the edge of the cell. Accumulated material is periodically pushed into the active cell with earthmoving equipment. The landfill is also inspected weekly so that situations which would lead to mass movement of waste are avoided or quickly corrected.

#### 3.7 Emergency and Release Notifications and Reporting

CKD, a non-hazardous material generated through the manufacturing of Portland cement, is not subject to release notification and reporting requirements. If releases of fuel, oils, or other materials occur from the transport vehicle or excavating equipment, Continental will provide proper notification to the IDNR and/or the United States Environmental Protection Agency in accordance with applicable requirements.

Due to the cementitious nature of the CKD material, windblown emissions from the face of the landfill or CKD piles are negligible. Further, the runoff from the exposed material is directed into the lined portion of the active cell allowing suspended sediment to settle out on site. The small quantities of fuel, oils, and other materials contained in transport vehicles or excavating equipment, if released, would likely be absorbed by surficial materials at the site. The likelihood of a release of materials affecting off-site properties is negligible. As such, notification to the city and county agencies, news media, or special populations will not be required.

#### 3.8 Emergency Waste Management Procedures

Since the landfill is utilized for the disposal of CKD, which is manufactured at the same site, operations at the plant will also be affected. Due to this fact, it is possible to cease operations at the landfill, if necessary, without adversely affecting CKD storage and disposal for long-term emergency events. In case of a short-term emergency, CKD is stored in a silo at the plant site. Hauling of CKD can be temporarily discontinued until the emergency is resolved.

#### 3.9 Primary Emergency Equipment Inventory

The landfill is staffed only during CKD unloading activities or while shaping and/or capping placed CKD material. The actual time on-site is less than 25 hours per month. Further, combustible materials are not stored, used, or disposed of at the site. As such, emergency equipment is not maintained at the site and water sources/hydrants are not located at the site. In the event of an emergency, equipment resources would be provided by the City of Buffalo, Iowa and/or Scott County.

#### 3.10 Emergency Aid

In the event of an emergency requiring aid, local authorities will be contacted.



#### 3.11 Training

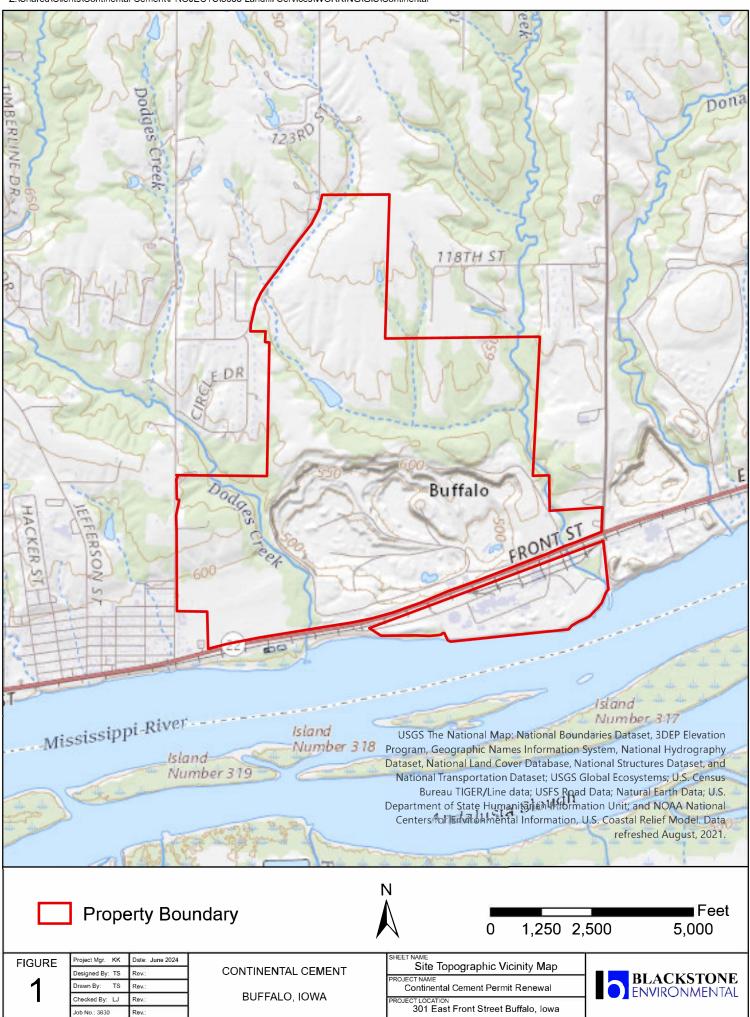
Employees operating landfill transport trucks and/or landfill placement equipment will be trained on the provisions of the ERRAP along with correct operating procedures. Training will be provided by the Environmental Manager or their designee. Training will be conducted for employee's firsttime assignment to duties associated with the storage, handling, transport, or disposal of CKD and periodically thereafter in conjunction with modifications to the ERRAP or issuance of an updated landfill operating permit. Training will be documented in accordance with Continental procedures.



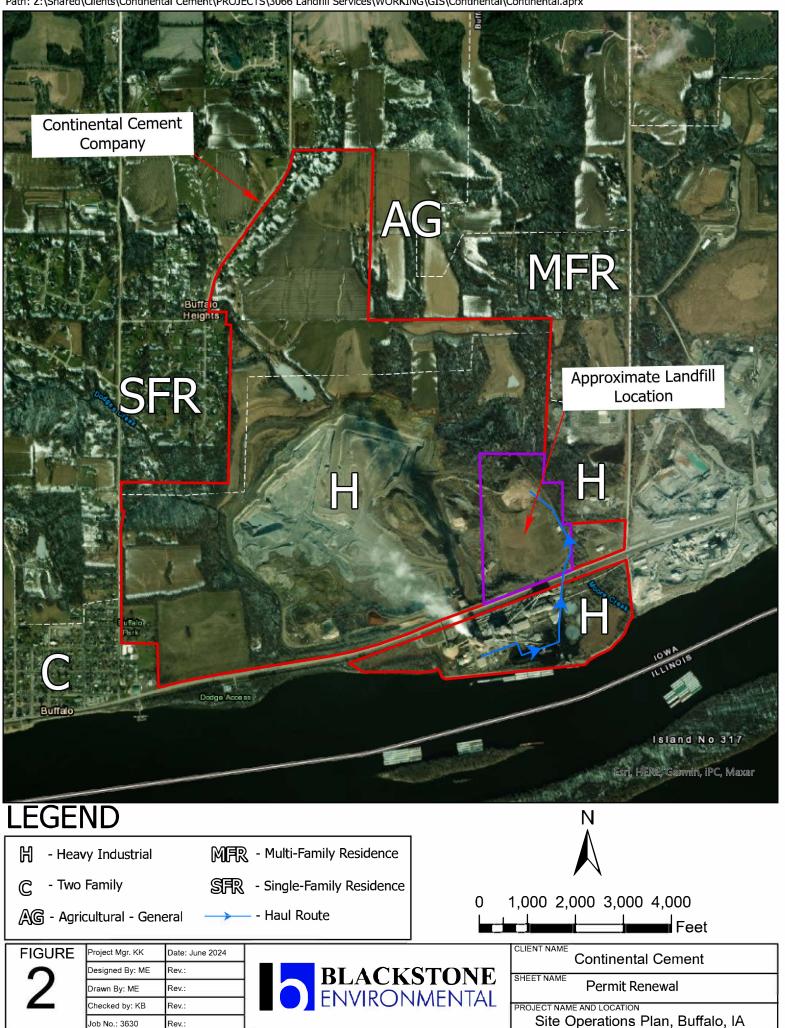
**APPENDIX A** 

Figures

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**APPENDIX H** 

**Comprehensive Waste Plan** 

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Suite 100, 4500 - 16th Avenue N.W. Calgary, Alberta, Canada T3B 0M6 Telephone: (403) 247-0200 Fax: (403) 247-4811 or 247-0779 e-mail: komex@komex.com web: www.komex.com

KOMEX INTERNATIONAL LTD.

ENVIRONMENTAL AND ENGINEERING CONSULTANTS

Kondo 82-SDP-15-96 PdS Loppy in article



June 30, 1997

OUR FILE: KI96-4161

Con 12-1-1 Doc # 44825

Waste Management Assistance Division Department of Natural Resources Wallace State Office Building Des Moines, Iowa, 50319-0034

Attention: Garth Frable

Dear Sir:

**Re:** .

Comprehensive Plan - Lafarge Davenport Cement Plant Cement Kiln Dust Closure and Development Permit DNR File No. 82-SDP-15-96

Accompanying this letter, please find 3 copies of the Comprehensive Plan for Lafarge's Cement Kiln Dust (CKD) management activities at the above-noted site. The Plan focusses on issues relevant to CKD, a mineral by-product of the cement manufacturing process. Issues related to management of municipal waste are not included, as the CKD management area is strictly a CKD monofill utilized only for the Davenport Cement Plant.

We understand that approval of the Comprehensive Plan is required to obtain a permit for CKD landfilling activities. Hence, we would appreciate your timely review. Please do not hesitate to contact the undersigned or Brian Gasiorowski of Lafarge at (248) 354 9050 if you have any questions. We trust that the Plan satisfies the relevant components of the Iowa statutes.

Respectfully,

KØMEX INTERNATIONAL LTD. M.J. Johnson, M.S., P.Eng.

cc. Cyrus Rustin, IDNR Brian Gasiorowski, Heinz Knopfel, Lafarge

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DEPT OF MATURAL RESOURCES

# **GMATE STAD**



Suite 100, 4500 - 16th Avenue N.W. Calgary, Alberta, Canada T3B 0M6 Telephone: (403) 247-0200 Fax: (403) 247-4811 or 247-0779 e-mail: komex@komex.com web: www.komex.com



#### KOMEX INTERNATIONAL LTD.

ENVIRONMENTAL AND ENGINEERING CONSULTANTS

#### COMPREHENSIVE WASTE MANAGEMENT PLAN - LAFARGE DAVENPORT CEMENT KILN DUST MANAGEMENT AREA

#### **PREPARED FOR:**

#### LAFARGE CORPORATION

#### **JUNE, 1997**

# **TABLE OF CONTENTS**

#### Page No.

1. INTRODUCTION 1	L
1.1 BACKGROUND 1	l
1.2 GENERAL 1	l
1.3 PURPOSE AND SCOPE 1	l
1.4 SITE DESCRIPTION	3
2. CEMENT KILN DUST	5
2.1 CEMENT KILN DUST ORIGIN	5
2.2 COMPOSITION	5
2.3 REGULATORY REQUIREMENTS	7
3. PLANNING	3
3.1 RESPONSIBILITIES	3
3.2 SCHEDULING	3
3.3 FUNDS	)
4. WASTE REDUCTION 10	)
4.1 PREVOUS WASTE REDUCTION INITIATIVES	)
4.2 ANALYSIS OF ALTERNATIVES 12	2
4.3 MEETING THE STATE VOLUME REDUCTION AND RECYCLING GOALS 13	3
5. IMPLEMENTATION SCHEDULE 14	1
6. REFERENCES	
7. DISCLAIMER	6

#### **LIST OF TABLES**

TABLE 1	CEMENT KILN DUST COMPOSITION
TABLE 2	ROLES AND RESPONSIBILITIES
TABLE 3	VOLUME REDUCTION SUMMARY
TABLE 4	IMPLEMENTATION SCHEDULE

#### **LIST OF FIGURES**

FIGURE 1	LOCATION MAP
FIGURE 2	CKD MANAGEMENT AREA

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#### **LIST OF APPENDICES**

APPENDIX I ALTERNATE USES OF CEMENT KILN DUST APPENDIX II COMPREHENSIVE SOLID WASTE MANAGEMENT PLAN REVIEW CHECKLIST

### 1. INTRODUCTION

#### 1.1 BACKGROUND

Lafarge Corporation operates a cement manufacturing facility that is located at 301 East Front Street, Buffalo, Iowa (Figure 1). The plant generates Cement Kiln Dust (CKD) as part of the cement manufacturing process and currently places this material in the quarry (Figure 2). Accordingly, Lafarge has recently applied for a permit for this activity in accordance with the Iowa Administrative Code (IAC Chapters 100 to 101). The State has requested that Lafarge submit a Comprehensive Plan for management and minimization of the landfilled materials in accordance with IAC Subrule 101.5 (IDNR, 1997). This report provides Lafarge's Comprehensive Plan (Plan) and addresses the relevant portions of Guidelines for Solid Waste Comprehensive Plans Part I: Solid Waste Mangement Alternatives (Guidelines) (IDNR, 1990).

#### 1.2 GENERAL

Review of the Guidelines indicates that the primary purpose of a Comprehensive Plan is to reduce the volume of municipal solid waste that requires landfilling and to allow for beneficial reuse wherever practical. The Guidelines generally focus on issues related to the public and to management of municipal solid waste. Hence, a considerable portion of the Guidelines is not relevant to CKD, which is a non-organic mineral material, or to Lafarge's landfill, which is a monofill comprising materials generated from a single source (Lafarge's cement manufacturing process). For these reasons, this Plan focuses on the following issues included in the Guidelines that are relevant to CKD management at Davenport:

- purpose and scope;
- description of the CKD;
- planning;
- previous waste reduction initiatives;
- analysis of alternatives;
- meeting the State's volume reduction and recycling goals;
- implementation schedule; and,
- checklist.

#### **1.3 PURPOSE AND SCOPE**

The Plan is a document that will help Lafarge implement programs to reduce the volume of CKD being landfilled at the Davenport Plant. Alternatives to landfills reduce the potential for groundwater contamination, preserve valuable natural resources, and enhance energy and economic savings. It will be submitted to the Waste Management Authority Division (WMAD) of the Iowa Department of Natural Resources (IDNR).

The Plan is a part of a legislated, comprehensive approach to solid waste management that complies with statewide solid waste management policy included as part of the Groundwater Protection Act. The Act identifies a hierarchy of preferred management options: The Waste Management Hierarchy. These options are prioritized according to their potential groundwater impacts, their overall environmental impacts, and their ability to conserve resources. The incorporation of these policies will ensure the protection of groundwater, the minimization of impacts on other environmental media and the wise use of natural resources. The potentially relevant Iowa laws state the following:

#### The Groundwater Protection Act

Pursuant to the Iowa Code, section 455B.306, a private agency operating or planning to operate a solid waste management project is required to prepare a Comprehensive Solid Waste Management Plan and to file it with the Department of Natural Resources.

According to 455B.306 of the Iowa Code, as Solid Waste Comprehensive Plan shall:

"...incorporate and reflect the waste management hierarchy of the state solid waste management policy and shall at a minimum address the following general topics to the extent appropriate to the technology employed by the applicant at the sanitary disposal project:

- 1. The extent to which the solid waste is or can be recycled.
- 2. The economic and technical feasibility of using other existing sanitary disposal project facilities in lieu of initiating or continuing the sanitary disposal project for which the permit is being sought.
- 3. The expected environmental impact of alternative solid waste disposal methods, including the use of sanitary landfills.
- 4. A specific plan and schedule for implementing technically and economically feasible solid waste disposal methods that will result in minimal environmental impact."

Iowa Code section 455B.301A (1987 Code Supplement) contains the state solid waste management policy as follows:

"The protection of the health, safety, and welfare of Iowans and the protection of the environment require the safe and sanitary disposal of solid wastes. An effective and efficient solid waste disposal program protects the environment and the public, and provides the most practical and beneficial use of the material and energy values of the solid waste. While recognizing the continued necessity for the existence of landfills, alternative methods of managing solid waste and reduction in the reliance upon land disposal for solid waste are encouraged. In the promotion of these goals, the following waste management hierarchy in descending order of preference, is established as the waste management policy of the state:

- 1. Volume reduction at the source.
- 2. Recycling and reuse.
- 3. Combustion with energy recovery and refuse-derived fuel.
- 4. Combustion for volume reduction.
- 5. Disposal in landfill."

#### The Waste Reduction - Recycling Act

In 1989, the Waste Reduction - Recycling Act (Iowa Code, Chapter 455D) placed additional requirements on the Comprehensive Plan. The law sets a statewide waste volume reduction goal of 25 % by 1994 and 50 % by 2000 through the use of waste reduction at the source and recycling. July 1, 1988 is the baseline year. Comprehensive Plans, Part I, shall provide details of a methodology for meeting the state volume reduction goal.

This Plan includes examination and development of alternative solid waste management systems that incorporate all of the <u>relevant</u> elements contained in these regulatory requirements and Guidelines. As such, the Plan develops technically and economically feasible alternatives to landfilling the CKD at the Davenport Plant. The Plan is a working document that Lafarge will use to develop, implement, and assess programs that will not only extend the life of their landfill area, but will produce a number of other benefits.

#### **1.4 SITE DESCRIPTION**

#### General

This section provides a description of the site in accordance with requirements of the Guidelines. The description refers to Lafarge's property, only and does not include description of the surrounding lands, populations, or transprotation corridors because these issues are not relevant to Lafarge's CKD management program.

The CKD management area is located at the east end of the quarry, approximately 2,000 feet from the active area of mining, and comprises approximately 20 acres (see Figure 2). Quarrying and cement manufacturing operations on the Site are approved through Lafarge's operating permits and licenses. The Site has been used and will continue to be used for the manufacture of Portland cement and related products. No other use is anticipated in the foreseeable future.

The quarry is approximately 90 feet deep in the vicinity of the CKD management area and has been filled to original grade over the eastern and southern portion of the management area. The northern portion of the area has been filled to an elevation of approximately 540 ft AMSL. In the past, the CKD has been placed directly in the quarry, essentially as a monofill.

The management area has historically been used for quarrying and then placement of CKD and off-specification cement materials similar in nature to CKD. On occasion, the area has been used for overburden and waste rock excavated as part of quarry development. Minor amounts of plant trash may have also been deposited in the area, although this volume is expected to be small. The CKD management area comprises only a small proportion of the current quarry.

#### **Siting Criteria**

The following characteristics and conditions have been established for the CKD management area:

Property Boundaries:	The management area is located more than 20 feet from an adjacent property line. The eastern property boundary of the Site is generally located 100 feet to the east of the management area. East Front Street (Highway 22) is located approximately 100 feet to the south of the area. No other property boundaries are located within 500 feet of the CKD management area.
<u>Floodplain</u> :	The management area is located outside of the 1 in 100 years floodplain of the Mississippi River. East Front Street separates the management area from the Mississippi River. The base of the quarry is located below the elevation of the river and is maintained dry by a central sump and pumping system which discharges water into the Mississippi River through NPDES 001 (Figure 2).
Nearby Residences:	The area is located more than 500 feet from any existing habitable residence. The nearest residence is located approximately 2,000 feet to the north.
<u>Site Stability</u> :	The Site has been used for more than 70 years for the manufacture of Portland cement and related products. During this time there has been no record of seismic events, active faulting or instability of the quarry walls. This area of Iowa has been established as one of low seismic activity. Hence, the Site is considered geologically stable.

Airports: The Site is located more than 10,000 feet from any airport, airfield, or runway. CKD dust does not attract birds or pests and hence the management area does not pose a risk to airplane traffic. Soil Conservation: The management area is located in a limestone quarry that has been developed to provide raw materials for cement manufacturing. There is no soil in the quarried area. Soil excavated in support of quarry expansion will be reused in the CKD area. The final grade is designed to conform to the surrounding pre-quarry landscape. Plants and Animals: Because the management area has and continues to be utilized for quarrying there are no plants that inhabit the management area and few animals. Hence, the CKD management activities will not impact potentially threatened species. Archeology: Similarly, due to past quarrying activities, the property is not of archeological or historical significance. Potential Human Impacts: The management area is well isolated from adjacent residences and farming areas. Hence, potential for impacts to human health are limited and do not include direct exposure. Potential environmental impacts are related to fugitive dust, which is controlled by conditioning and compacting the CKD, as well as groundwater quality, which is monitored in accordance with the Code.

#### 2. CEMENT KILN DUST

#### 2.1 CEMENT KILN DUST ORIGIN

The cement manufacturing process involves heating carbonate rock (limestone) with minor amounts of silica, alumina and iron minerals to form clinker. The clinker is ground into a fine powder and is mixed with gypsum to form cement. The heating process occurs in the cement kiln. Large quantities of air are used in the cement kiln to support combustion. The air and combustion products entrain particles of clinker, raw materials, and partially calcined materials. These particles are removed from the exhaust gases as an air pollution prevention measure and are recycled into the cement manufacturing process as kiln feed. Some removal of particulate from the clinker manufacturing process is required to control the composition of the final product. This material is known in the industry as cement kiln dust (CKD).

#### 2.2 COMPOSITION

The average chemical composition of CKD reflects the composition of the feed rock and soils and includes the following compounds:

CaCO <sub>3</sub>	SiO <sub>2</sub>
CaO	K <sub>2</sub> SO <sub>4</sub>
Al <sub>2</sub> O <sub>3</sub>	KCl
Ca(OH) <sub>2</sub>	CaMg(CO <sub>3</sub> ) <sub>2</sub>
Ca(MgFe)(CO <sub>3</sub> ) <sub>2</sub>	

#### Table 1: Cement Kiln Dust Composition

Metal oxides are present in trace amounts because these compounds condense in the kiln, on the particulates as the gases move counter-current to the material flow. CKD composition is primarily a function of the layout and operation of the kiln. Hence, the composition is stable over time.

CKD consists of relatively uniform silt size particles, in the range of 5 to 20 microns mean particle size diameter, and has a high affinity for water. The addition of water initiates a hydration process that causes kiln dust to set in a manner similar to cement. Because of its fine particle size distribution, the CKD can retain a high proportion of water before reaching saturation. This water is held to the particles by surface tension, resulting in relatively low hydraulic conductivity, on the order of  $10^{-6}$  cm/sec if the CKD is in a compact state (> 90% Standard Protor Density).

In its dry state, the CKD exhibits an angle of internal friction of approximately 34°. Once the hydration process is complete, the material can develop unconfined compressive strengths well in excess of 100 psi, depending on its initial composition.

#### 2.3 **REGULATORY REQUIREMENTS**

CKD is a non-hazardous solid mineral that is excluded from the Resource Conservation and Recovery Act (RCRA) Subtitle C through the Bevill Amendment. Lafarge has completed discussions with the State of Iowa regarding the regulation of CKD management activities at the Site. It was concluded that the CKD would be regulated as a non-hazardous solid waste, in accordance with Iowa Code Section 567, Chapters 100 to 111 (IDNR, 1996).

## 3. PLANNING

#### 3.1 **RESPONSIBILITIES**

The first step in the planning process is to identify key individuals that will be responsible for developing and implementing the Plan. In this case, the generation and management of CKD are controlled entirely by the Lafarge Davenport cement plant and corporate support groups. Hence, the individuals responsible for implementation of the Plan are Lafarge employees and subcontractors. The positions, individuals currently holding the position, and the present area of responsibilities are listed below.

Job Function	Present Individual	Responsibilities
Plant Environmental Manager	Heinz Knopfel	<ul> <li>CKD management</li> <li>regulatory issues</li> <li>funding</li> <li>program implementation</li> </ul>
Regional Environmental Mgr.	Brian Gasiorowski	<ul> <li>implementation of env. programs</li> <li>regulatory representation</li> <li>quality assurance</li> </ul>
Director of Geology & Raw Materials	Jean-Guy Levaque	<ul> <li>quarry planning</li> <li>assessment of raw materials</li> <li>CKD management</li> </ul>
Alternate Raw Materials	Greg Daderko	<ul> <li>beneficial reuse of CKD</li> <li>scheduling alternate raw materials</li> </ul>
Consultant	Gordon Johnson	<ul><li>landfill design</li><li>hydrogeological monitoring</li></ul>

#### **Table 2: Roles and Responsibilities**

#### 3.2 SCHEDULING

Lafarge implemented a CKD task force in 1992 to address the following:

- controlling cement manufacturing raw materials to minimize generation;
- potential beneficial reuse;
- potential process modifications to reduce generation; and,
- management of placement operations.

Each Lafarge facility, including the Davenport Plant was addressed by the program. Measures were taken to minimize the rate of CKD generation by the plant and to investigate potential

beneficial reuses of CKD. Initiation of the program has essentially been completed. Measures adopted for the Davenport Plant continue to be revisited on a regular basis with the goal to continuous improvement.

#### 3.3 FUNDS

Funds for implementation of the Plan are made available through the Plant's annual operating budget, which include allowances for CKD management and related issues. Plant operations result in the sale of approximately 1 million tons of cement annually. Income from these operations provide Lafarge with the financial resources necessary to effectively manage its CKD and to effectively address related issues such as the implementation of this Plan.

# **4. WASTE REDUCTION**

#### 4.1 PREVOUS WASTE REDUCTION INITIATIVES

Lafarge Corporation is an active member of the Portland Cement Association (PCA), an organization of cement manufacturers dedicated to improving and extending the uses of portland cement and concrete through market development, engineering, research, education and public awareness. In 1995, the PCA commissioned a study of the Alternate Uses of Cement Kiln Dust (Bhatty, 1995) which is provided as Appendix I. This study addresses all currently known alternative uses of CKD.

As previously stated, Lafarge implemented a CKD task force in 1992 to more effectively manage the dust generated by its cement manufacturing facilities. A major focus of the task force was to investigate means of reducing the CKD generated by active cement plants. To this end, Lafarge implemented a program that embraced all of the alternate uses of CKD as summarized in Appendix I. For the Davenport cement plant, the following landfill reduction initiatives were implemented:

- recycling of all spilled cement materials, kiln brick and like debris into the cement manufacturing process;
- regular geological assessments and quarry mining plans with the goals of coordinating raw materials management to minimize the rate that CKD is generated by the plant;
- utilization of alternate raw materials;
- recirculating dust in the cement manufacturing systems;
- supervising and controlling the CKD management area so that only CKD is placed in this area; and,
- investigating beneficial uses for CKD in the Davenport area.

#### Recycling

Since the early 1990's, all used kiln brick, off-specification clinker, spilled cement materials and the like are recycled in the cement manufacturing process. Up to this time, these materials were placed in the CKD management area. Although accurate records of the volumes placed in 1988 are not available, an average of approximately 30 tons per day have been recycled.

#### Raw Materials Control

Geological assessments of the quarry are completed on a regular basis. Mine plans are developed by Lafarge Corporate Technical Services approximately once every 5 years. The purpose of the plans is to control raw feed to maximize the efficiency of the cement manufacturing operations, which in turn minimizes the rate that CKD is generated. Efforts to date include controlling raw materials to limit the concentrations of alkali metals in the raw feed which ultimately reduces the proportion of dust that is removed from the process. These efforts have resulted in reduced rates of CKD generated, although it is not possible to quantify percent reduction because the cement product has changed since 1988, necessitating a change in the manufacturing process.

#### Substitute Raw Materials

The plant has initiated a program to utilize substitute raw materials in the cement manufacturing process. These materials are low-alkali in nature and result in reduced CKD production. They are also byproducts from other industrial operations that would otherwise be disposed in a commercial landfill. The plant currently utilizes approximately 50,000 tons of alternate raw materials each year.

#### **Recirculation**

Over 90 percent of the dust collected in the cement manufacturing process is recirculated into that process. The remaining dust is removed from the process to control the composition of the cement product (Section 2). Lafarge maximizes the percentage of dust recycled in the process to maximize cement productivity. These recirculation measures were in place in 1988.

#### Control of CKD Management Area

Placement of materials into the CKD management area has been controlled since the early 1990's so that the area is essentially a CKD monofill. It is estimated that approximately 10% of the materials entering into the area in 1988 would have been non-cementititous in nature. These materials are now either recycled or legally disposed off-site.

#### **Beneficial Use**

The Davenport plant has trialed beneficial use of CKD generated by the plant on two separate occasions, as follows:

- as an agricultural amendment to increase soil pH; and
- as an admixture to improve the characteristics of animal sewage.

While these trial programs confirmed the potential beneficial uses of CKD they have not yet been implemented on a predictable and consistent scale. At its peak, the beneficial reuse program accounted for up to 50% of the CKD generated by the plant.

#### 4.2 ANALYSIS OF ALTERNATIVES

Lafarge continues to investigate alternative measures that will reduce the volume of CKD requiring landfill at the Davenport Plant. In general, the alternative uses of CKD described in Appendix I have, and continue to be investigated by Lafarge. In accordance with state goals specified in the Guidelines, the following measures will be taken.

<u>Waste Reduction</u> Future quarrying plans will be designed to reduce alkali content of the raw feed which will in turn reduce CKD production. A 10% reduction is targeted by controlling kiln feed.

<u>Recycling</u> The recycling of dust in the cement manufacturing process will be continued and will account for over 90% of the dust collected in the manufacturing process.

Lafarge will continue to optimize the use of substitute raw materials to improve the quality of the kiln feed and to reuse materials that would otherwise be disposed in a commercial landfill. A volume of 50,000 tons per year is budgeted for the foreseeable future.

Alternate uses for CKD will continue to be investigated by Lafarge. At this point, no alternate uses have been established on a consistent and reliable basis. Reuse of CKD for soil stabilization or waste amendment appears to be the most likely option at this time.

<u>Incineration</u> CKD is a non-combustible, non-organic material and thus incineration options are not applicable.

# Landfilling This is the base option that addresses the CKD generated by the facility that remains following implementation of the aforementioned reduction measures. At the present time, on-site management of CKD is required in order to produce low-alkali cement. An estimated 100 tons/day of CKD will be generated by the facility on an ongoing basis, although the rate of generation is a function of the volume of cement produced which in turn is a function of market conditions. CKD is managed in accordance with the Closure and Development Plan for management of CKD which has been submitted to the IDNR for approval. The management plan ensures suitable environmental protection by implementing recognized, effective solid waste management techniques.

The Plan includes conditioning and compaction of the CKD which will reduce the placed volume by up to 20%.

#### 4.3 MEETING THE STATE VOLUME REDUCTION AND RECYCLING GOALS

The underlying table provides a summary of the solid waste reduction and recycling efforts implemented at Lafarge's Davenport cement plant. Generation rates are provided for 1988 (base data), 1997 (current rates) and 2000 (predicted) in accordance with the Waste Recycling and Reduction Act. Current rates are essentially representative of the conditions in place in 1994. A review of this table indicates that Lafarge's Davenport operations currently meets the legislated goal of 50% reduction by 2000.

Lafarge will continue to investigate and implement volume reduction alternatives with the goal of eliminating the need for CKD landfilling at the Davenport plant. However, until a beneficial use for CKD can be established with confidence, there will continue to be a need to manage CKD at the Davenport Plant.

Item	Initiative	Base Case 1988	Existing Initiative 1997	
			Volume Reduced	%
CKD	Control Raw Materials	46,000 tons/yr	10,000 tons/yr	22%
Clinker/Bricks	Recycle	10,000 tons/yr	10,000 tons/yr	100%
Substitute Raw Materials	Recycle	50,000 tons/yr	50,000 tons/yr	100%
*CKD	Beneficial Use	46,000 tons/yr	up to 23,000 tons/yr	up to 50%
Total	Various	106,000 tons/yr	70,000 tons/yr	66%

#### Table 3: Volume Reduction Summary

#### **Planned Initiatives**

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Item	Initiative	Base Case 1997	Future Initiative 2000	
			Estimated Volume Reduced	%
CKD	Control Raw Material	36,000 tons/yr	4,000 tons/yr	10%
CKD	Compaction	40,000 yd <sup>3</sup> /yr	8,000 yd <sup>3</sup> /y	20%
*CKD	Beneficial Reuse	36,000 tons/yr	up to 36,000 +/y	up to 100%
Total	Various	40,000 yd <sup>3</sup> /yr	12,000 yd <sup>3</sup> /yr	30%

\* not included in total (not continuous).

# 5. IMPLEMENTATION SCHEDULE

The schedule for implementation of the waste reduction initiatives described in this plan is presented below. Although key dates are prescribed, Lafarge deals with the issue of plant operations in general, and CKD generation in particular, on a regular basis with the goal of achieving continuous improvement. Alternate uses for CKD will be addressed by Lafarge both within the corporation and as part of the Portland Cement Association. These programs will continue to ensure that the legislative goals of the State of Iowa continue to be met or exceeded at the Davenport Cement Plant.

Table 4:	Implementation	Schedule
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Initiative	Implementation Date	<b>Review Schedules</b>
Comprehensive Plan	July, 1997	Every 3 years
Substitute Raw Materials	early 1990's	Ongoing
Clinker / Brick Recycling	early 1990's	Ongoing
Quarry Planning	1997	every 5 years
Beneficial Use	early 1990's	Ongoing
CKD Compaction	1997	Ongoing
Assess Generation Rates	1997	Annually

Appendix II provides a completed checklist for issues related to this Comprehensive Plan.

Reported By:

KOMEX INTERNATIONAL LTD. J. Johnson, M.S., P.Eng.

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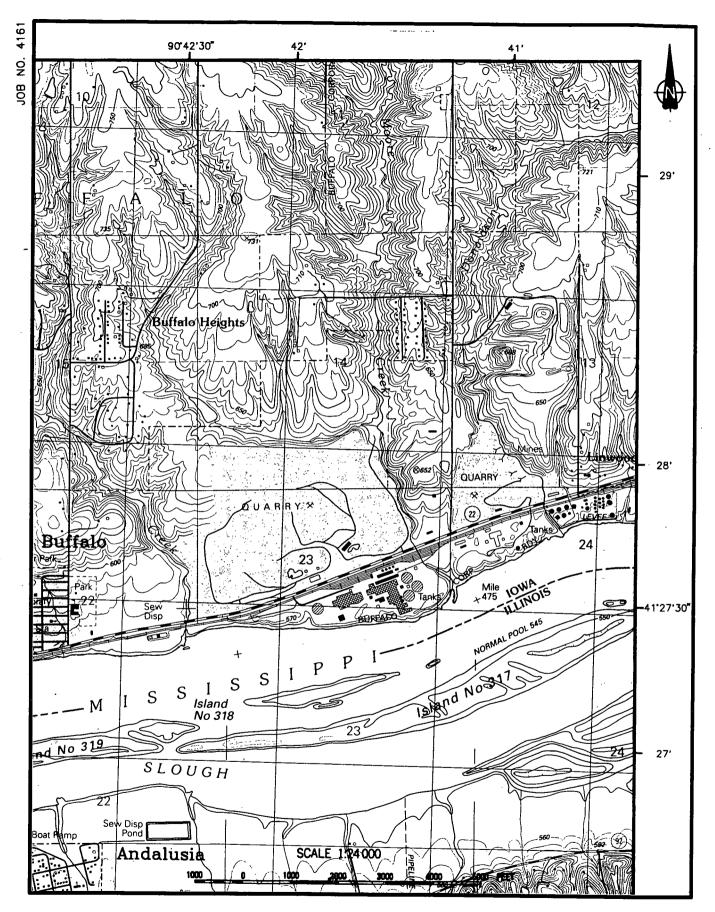
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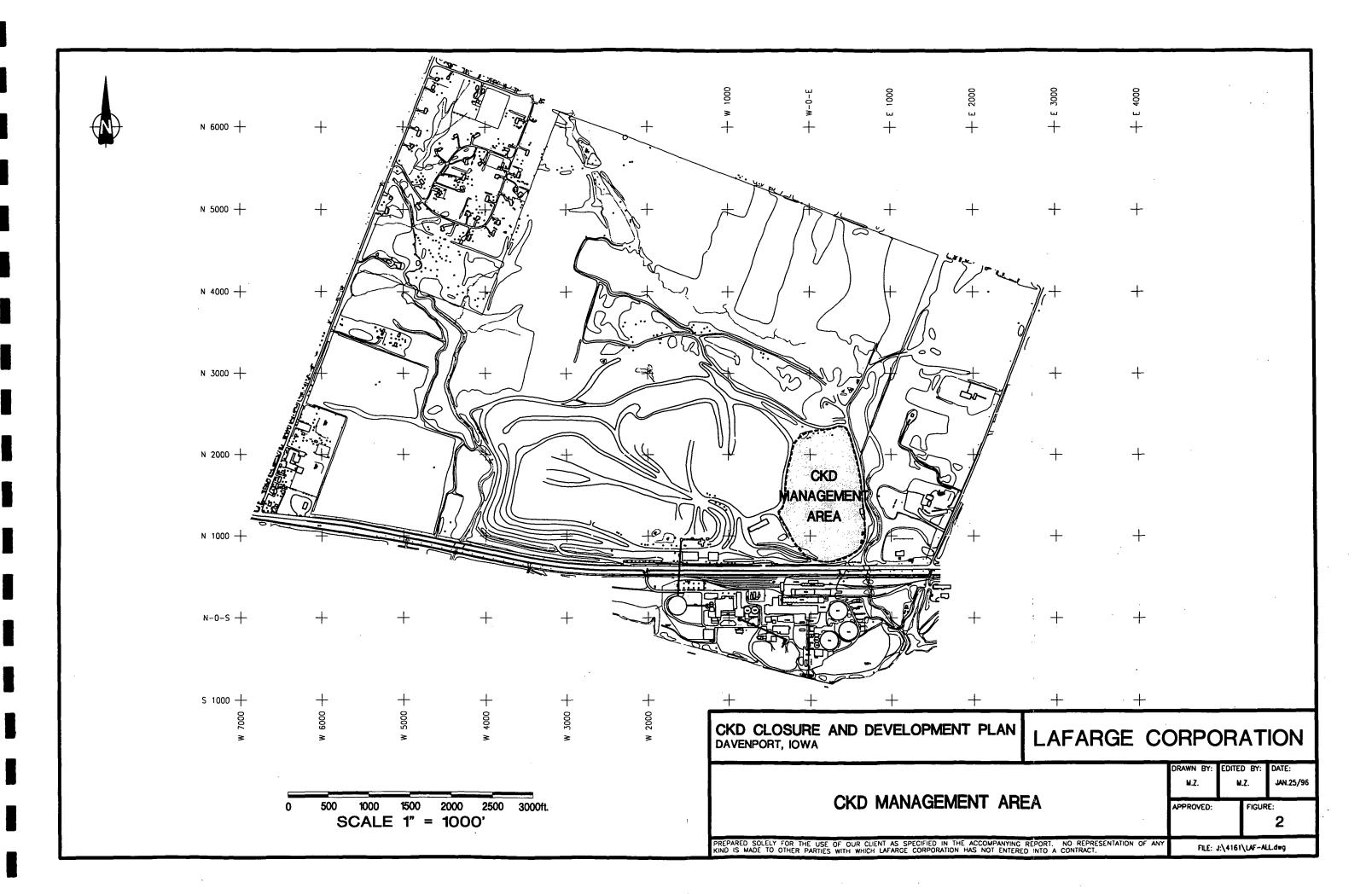
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LOCATION MAP DAVENPORT CEMENT PLANT

Figure 1



### **APPENDIX I**

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### ALTERNATIVE USES OF CEMENT KILN DUST

**Portland Cement Association** 



# Alternative Uses of Cement Kiln Dust

by Javed I. Bhatty

#### ABSTRACT

This report contains up-to-date information on the utilization of cement kiln dust. The bulk of the cement kiln dust (CKD) generated is recycled as a raw feed substitute in cement manufacturing and a portion of it is used as a secondary material for selected commercial applications. The remaining CKD is often landfilled. Such applications are dependent upon the chemical and physical characteristics of CKD. The major parameters that determine the CKD characteristics are the initial raw material, type of kiln operation, dust collection systems, and fuel type. Since each plant has its own geological and operational position, the CKD use is generally considered on a plant-to-plant basis.

A brief description of the physical and chemical composition of typical CKDs is given in the beginning of the report, followed by their applications that have been reported in the literature thus far. These include recycling of CKD back into cement manufacturing because of similarities to the raw feed, and a variety of other applications that rely upon its fineness and high lime contents. The use of CKD in blended cements, subbase and soil stabilization, waste treatments, and in scrubbing acidic emissions is getting increasing attention. Application of CKD as fertilizers and in chemical processing to recover alkali salts is based on its high potassium contents. Miscellaneous applications include mine backfilling, glass making, coagulant in waste-water treatments, and absorptive agent for oil spillages. Direct landfilling of CKD after appropriate moisture adjustment and compaction has also been reported.

Thus, as can be seen, CKD has extensive application potential. The proper use of CKD, however, will depend upon its composition and availability in order to help consume the large quantity generated without any environmental and management problems.

#### **KEYWORDS**

blended cements, cement kiln dust, fertilizer, portland cement manufacturing, recycling, soil stabilization, subbase, waste management, waste treatment

## **Alternative Uses of Cement Kiln Dust**

by Javed I. Bhatty\*

#### INTRODUCTION

Millions of tons of cement kiln dust are generated annually from cement plants operating in North America. The bulk of the dust is recycled into clinker manufacturing as kiln raw feed. About 3.35 million metric tons of this dust, mostly with high alkali contents, is landfilled while about 0.75 million metric tons enters commerce as by-products (Abeln et. al., 1993)." The generation of waste kiln dust—that which cannot be reused in cement manufacturing--is responsible for a significant financial loss to the cement industry in terms of the value of raw materials, processing (quarrying, grinding, storage), energy usage during pyroprocessing, dust collection, and disposal. In terms of quarrying, crushing, grinding, etc., dust represents a significant investment that can be directly translated into an additional requirement for raw materials and loss of potential clinker production. This net loss can exceed 15% in some plants (Klemm, 1980).

Cement kiln dust consists mainly of partially calcined kiln feed and, as such, is generally suitable for recycling back to the kiln. The principal obstacle to such a preferred use has been the requirement of many states for a low alkali cement because of concerns for potential alkali-silica reaction (ASR) with reactive aggregates in concrete. The reduction of the alkali content of many plant clinkers to less than 0.6% equivalent of Na<sub>2</sub>O results in a significant increase in CKD production especially in alkali bypass dust from plants so equipped. A further reduction of alkalies in cement to below 0.4% equivalent Na<sub>2</sub>O, as done in certain states, would further exacerbate the excess CKD generation problem.

Thus, it is clear that any steps that can be taken by the cement industry to either reduce CKD generation, permit more recycling in the pyroprocessing stage to increase clinker production, or to develop additional uses for CKD as value-added product, would be of great importance. Disposal or landfilling of dust may be necessary, but this constitutes an undesirable alternative and expense.

#### OBJECTIVE

The objective of this report is to provide a general overview of the existing and proposed methods of reducing waste by utilizing CKD in other industrial applications. The resources of the Portland Cement Association (PCA) Library, the services of several other computerized databases, and relevant reports and files of the CTL staff were used in this study.

#### **DUST GENERATION**

Although it is difficult to quantify a direct correlation between dust generation and plant operation, the production of CKD strongly depends upon the type of process and the design of gas velocities in the kiln. Other factors such as kiln performance and dust collection systems also play vital roles. CKD, a fine particulate material, is readily entrained in the gases moving through the kiln. Since each kiln system markedly differs in the amount of dust contact and gas velocities, the quantity of CKD generated varies accordingly.

According to Steuch (1992), the largest amount of dust is generated from long dry kilns in which the dust is stirred up by chains and the gas velocities are high. In contrast, in preheater kilns, feed loading is high and the resulting dust contact with kiln gases is short. Thus, the CKD generation is fairly low. Some of the wet kilns produce the lowest amounts of dust, mainly because these kilns contain pebble-size dust agglomerates that are difficult to sweep away by the moving kiln gases. Yet, the range of dust generated from these kilns does vary. Figure 1 shows the range of kiln dusts generated by each operation type.

These results contrast with those of Müller (1977), which indicated that the amount of dust produced from wet kilns exceeded those from dry and semidry/semi-wet kilns, as shown in Table 1. Müller's data is cumulative of both the returned dusts (that recycled to the raw mix for clinker making) and the discarded dusts originated from the then commonly used manufacturing processes. Those processes included long-dry kilns, long-dry kilns fed by nodules, Lepol-kilns (semi-dry kilns) fed by meal nodules, Lepol-kilns fed by filtration nodules, dry kilns with suspension preheaters, long-wet kilns, and short-wet kilns with drum preheaters. The CKD information for these kilns is collectively grouped as "wet", "semi," and "dry" kilns as presented in Table 1.

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 \*\* See Bibliogrophy for references in parentheses

#### **CEMENT KILN DUST CHARACTERISTICS**

#### **Chemical Composition**

The composition of CKD does not vary significantly from the original raw feed. CKD is a particulate mixture of partially calcined and unreacted raw feed, clinker dust, and ash, enriched with alkali sulfates, halides, and other volatiles. The Bureau of Mines (Haynes and Kramer, 1982) reported a typical dust composition, as given in Table 2.

In practical terms, however, there is no typical or average CKD, as the dust from each plant varies markedly in chemical, mineralogical, and physical composition, depending upon the raw material, type of operation, dust collection facility, and type of fuel used at that plant (Klemm, 1993). CKD from three different types of operations: long-wet, long-dry, and alkali by-pass with precalciner were characterized for chemical and physical make up by Todres et. al. (1992). CKD generated from long-wet and long-dry kilns is composed of partially calcined kiln feed fines enriched with alkali sulfates and chlorides. The dust collected from the alkali bypass of precalciner kilns tend to be coarser, more calcined, and also concentrated with alkali volatiles. Sample compositions of these CKDs are shown in Table 3.

The dusts collected from gas- or oil-fired kilns contain higher proportions of soluble  $K_2O$  compared to coal-fired kilns. This is probably due to a more favorable  $K_2O:SO_3$  molar ratio in the latter as compared to the former (Klemm, 1980).

#### Mineralogical Composition

Based on the investigations of nearly 100 European CKDs (Müller, 1977), dusts are particulate mixtures of four major components: (1) unreacted raw feed, (2) partially calcined feed and clinker dust, (3) free lime, and (4) enriched salts of alkali sulfates, halides, and other volatile compounds. The mineralogical compositions of these groups are shown in Table 4.

#### **Particle Size Distribution**

The particle size of the CKD is dependent upon the type of kiln operation. Müller (1977) showed that the dusts collected from dry kilns were finer than those from wet and semi-wet/semi-dry kilns as shown in Table 5. This was true for both the returned dust and the discarded dusts. Studies conducted at Construction Technology Laboratories, Inc. (CTL) (Todres et. al., 1992) show that for modern cement plants equipped with alkali bypass, the dust is relatively coarse compared to the CKD from both the wet and dry kilns (see Table 6). The dusts collected from the alkali bypass of precalciner kilns are predominantly calcined feed, rich in alkali sulfates and other volatiles. Although the chemical composition of CKD is assumed to be uniform over its entire size distribution, one recent study (Klemm, 1993) showed that of the total amounts present in the unseparated dust, the finer fraction collected from an alkali bypass (where 38% of mass was less than 32 $\mu$ m in diameter) contained 47% of the Ka<sub>2</sub>O, 49% of the NaO<sub>2</sub>, 49% of the SO<sub>4</sub>, and 50% of the Cl present in the dust.

#### CONSIDERATIONS FOR CEMENT KILN DUST USE

Because CKD varies in physico-chemical compositions between plants, and each plant is unique with respect to its geographical condition, the managing of dust is a plant-by-plant situation. However, other factors, such as existing plant equipment and the requirements of the marketplace, must be considered in dealing with dust utilization on a long term basis.

Since the dust has a significant monetary value as a raw material plus additional costs for material processing (Klemm, 1980), and has a chemical composition close to that of the original raw feed, a majority of plants tend to recycle their CKD in the raw kiln feed whenever possible. If they are too high in alkali, they may either be sold for other purposes or be landfilled. One must note, however, that continuous recycling of CKD soon reaches an equilibrium with respect to alkali levels in the kiln feed and the internal cycle of volatilization and condensation within the kiln, resulting in high alkali clinkers. This is not good for plants intending to make low alkali cements. Two states in the United States now require cement to have an alkali content at or below 0.4% of Na<sub>2</sub>O equivalent, rather than the usual 0.6% Na<sub>2</sub>O equivalent specified in ASTM C150 (ASTM, 1994).

CKD contains insignificant amounts of trace elements and, therefore, minor elements are usually not a concern for most applications. A recent comprehensive study reviews trace metals for 79 plants in the United States and 10 in Canada using both conventional and waste-derived fuels (PCA, 1992). In this study, each CKD was tested for the eight RCRA metals: arsenic, barium, cadmium, chromium, lead, mercury, selenium, and silver, and four additional BIF metals: antimony, beryllium, nickel, and thallium. The average levels of trace metals found in the dusts from the study are given in Table 7 and were significantly below the regulatory limits.

#### UTILIZATION OF CEMENT KILN DUST

In view of the diverse physico-chemical characteristics of CKD and the associated economical and environmental priorities, the use of CKD is best considered on a plant-by-plant basis. A number of possible options to manage the dust have been considered. As a first choice, attempts have been made to recycle CKD in-process in cement manufacturing directly as kiln feed, or to remove alkali sulfates and chlorides and use the remainder as kiln feed; to treat or modify the CKD for use as a clinker additive, or to blend it in the finished portland cement. Alternatively, the dust has been recycled outof-process as a by-product or a secondary raw feed for a variety of allied industries. A summary of the major CKD utilization and disposal practices adopted by the cement and allied industries is reported below.

#### **Recycling of CKD in Cement Manufacturing**

Directly in Raw Feed. Ideally, the CKD should be used as a partial raw feed in cement manufacturing. A large portion of the CKD recovered in cyclones, baghouses, or precipitators, is already being used as kiln raw feed. The CKD must be low in alkalies for such use, or the manufacturer should be willing to produce high-alkali cements acceptable in the market. The maximum Na<sub>2</sub>O equivalent required for Types I and II low-alkali cements is 0.6%, while two states in the United States now require low-alkali cements having no more than 0.4% Na<sub>2</sub>O equivalent. Excessive alkalies contribute to alkali-silica reaction (ASR) with reactive aggregates, which is harmful to the long-term performance of concrete.

In cement operations using the dry process, CKD has been blended directly into the raw feed, or pelletized before introduction to reduce dusting. In the wet process, blending CKD with kiln feed is more difficult because semi-calcined dusts harden when exposed to moisture and may affect the slurry viscosity and flowability. The CKD is added to the kiln feed slurry in appropriate proportions just before entering the kiln. The addition of CKD may have a thickening effect on slurry that is normally overcome by using a variety of slurry thinners such as polyphosphates and lignosulfonates.

On the other hand, for CKDs rich in alkalies, a common approach has been to remove alkalies by aqueous leaching and return the "washed" CKD to the kiln. McCord (1977), Klemm (1980), and Fraiman et. al. (1991) have reported this approach and used the "washed" CKD as kiln raw feed. A recently developed scrubber technology (Young and Morrison, 1991), recovers CKD by reducing its alkali and sulfur contents through hot aqueous scrubbing. This process permits CKD to be reused as kiln feed, while also producing saleable by-products such as potassium sulfate for fertilizers. Another recovery system (Fuller, 1992) employs fluidized bed reactor technology and converts up to 90% of the pelletized kiln dust to a clinkered product that can be interground with conventional clinker to produce cement. The volatilized alkalies are recovered separately.

In an older process (EIMCO), the CKD undergoes aqueous leaching in a contactor and later passes through a concentrator to form a 50%-60% solid feed material for the kiln. The resulting clinker is claimed to be low in alkalies. The process is applicable to both the dry and wet processes. The leachate overflow, which is rich in alkalies, could be discharged into receiving basins. It is unlikely that the U. S. Environmental Protection Agency would permit such a process under present regulations.

Insufflation/Mid-Kiln Introduction. Other methods of introducing dust back into the kiln have been either by insufflation into the burning zone or by dust scoops in the mid-section of the kiln from a collar around the kiln. The latter practice has now practically disappeared. Two disadvantages are also cited with insufflation. First, the dust tends to remain airborne for a long time because of its fineness, thus wasting energy for collection and reheating. Second, the dust clouds the area around the burner making it difficult to measure the flame temperature optically--- this generally limits the use of dust return to 15% on a kiln feed basis (Steuch, 1992). Additionally, insufflation may encourage the questionable practice of controlling the burning zone temperature by the rate of dust addition. Again, care must be taken that the dust used is low in alkali chlorides and sulfates.

CKD has also been introduced through the primary air burner pipe in coal-fired kilns, as reported by Siegert (1974). A Japanese company (Air Products and Chemicals, Inc., 1991) developed a method for recycling dust in rotary kilns, where oxygen is added to the burning zone to 21% concentration level to enhance combustion.

Blending/Intergrinding with Clinker. A somewhat different approach of intergrinding or blending alkali-free CKD with clinker to produce finished cement of acceptable performance has been employed by a number of firms. One dust recovery system (Fuller, 1992), mentioned earlier, introduced fluid bed technology whereby high alkalies in CKD are volatilized and the low-alkali clinkered residue is interground with plant clinker to produce lowalkali cement of acceptable performance.

In one case, alkalies (mainly  $K_2O$ ) had been removed from the CKD by volatilization after calcium fluoride was added, and the residues subsequently interground with cement clinker (Huber and Reath, 1917). Klemm (1980) also reported the possibility of adding calcium chloride to the dust to help volatilize  $K_2O$  salts and using the calcined solid for cement manu-facturing.

#### Applications in Construction Industry

Subbase Consolidation for Highway Construction. Because of the generally high free lime content (which sometimes can vary drastically between 3%-23% by weight) and subsequent ability to harden upon exposure to moisture, CKD has been used as binder in soil stabilization suitable for a subbase in streets and highway construction. The University of Toledo and Nicholson (1977) developed a product from CKD, waste glass cullet, fly ash, and wastewater sludge as a subbase material for highways.

Nicholson (1978,1982) patented a road-paving mass from CKD and fly ash at nearly a 1:7 mass ratio with the addition of cement or other admixtures if necessary. In another development, Nicholson (1983) has referred to the use of CKD and fly ash compositions not only for road-base systems but also for sludge stabilization. The marketability of recycled CKD as pozzolanic pavement material as well as an acid neutralization aid has also been suggested.

In a recent work, Sayah (1993), and Zaman et. al. (1992) have demonstrated the effectiveness of CKD in stabilizing highly expansive clay soils. Their data showed similarities to those of portland cement, fly ash, and lime for stabilizing expansive soils. Miller et. al. (1980) used CKD and fly ash in stabilized base courses in road construction in the form of a pozzolanic non-cement concrete with limestone as an aggregate. Such concrete mixes were also found to have autogenous healing characteristics. McCoy and Kriner (1971) reported a wide range of tests conducted on kiln dust compositions for soil consolidation.

Another possible use of CKD is in injection grouts for stabilizing concrete slabs, slabjacking, and voidfilling. The required compressive strength is about 4 MPa (600 psi) at seven days and can be achieved by using CKD without portland cement or with only a small amount of cement.

Blended Cements and Masonry Products. A great deal of work has also been done on the use of CKD in blended cements. Bhatty (1983-1986) has published of series of reports on the addition of CKD to portland cement along with fly ash and blast furnace slag, with variable results. Cements containing CKD alone reportedly had reduced strength, setting time, and workability. The strength loss was attributed to the presence of high alkalies in the dust. The addition of fly ash with CKD lowered the alkali contents and resulted in improved strength. Additions of slag generally reduced workability but increased the strengths because of activation from the high lime content of the CKD.

Bhatty's results also demonstrated that particular ratios of alkali, chlorides, and sulfates are important for better performance of cement blends. A high sulfate blend, for instance, gave the highest strength. However, the high alkali contents could result in susceptibility to alkali-aggregate reaction (ASR), which may be blocked by the slag or fly ash constituents. Based on similar data, Sanduo (1986), suggested that the use of finely ground limestone and cement kiln dust should be allowed in standard ASTM specifications for portland cements.

Daugherty and Funnell (1983) have also evaluated the use of CKD by intergrinding in blended cements. There appeared to be no evidence of adverse effects with up to 10% dust addition, on the setting time, soundness, or shrinkage. The strength results varied, however, probably because of the changing dust composition. Klemm (1980) pointed out that blended cements containing CKD can work satisfactorily only if the total alkali content is not excessive, otherwise fly ash or blast furnace slag should be added to reduce potential ASR problems.

ASTM subcommittee D 34.15 (1993) is currently preparing a specification that would permit the use of a uniform blend of Class F fly ash with CKD. This pozzolanic blended material for construction applications is tentatively designated as Type FCKD.

CKD has also been used successfully in masonry and concrete blocks without the addition of pozzolans. A study by Ravindrarajah (1982) showed that up to 15% of portland cement could be replaced with kiln dust in mixes without loss of strength and workability. However, higher proportions of CKD retarded setting, increased water demand, and reduced workability. Luther (1993) has also reported using up to 10% CKD in granulated blastfurnace slag cement to produce concrete with satisfactory performance.

Wills (1983) substituted up to 60% CKD for portland cement in producing concrete blocks of adequate physical strength after partial curing in  $CO_2$ -laden environments at 60°C (140°F). Chen and Lu (1989) produced cementitious blocks from CKD and fly ash components by steam curing treatments. They also reported using small additions of silica fume to suppress the harmful effects of excessive K<sub>2</sub>O in the CKD on compressive strength.

von Seebach and Tompkins (1992) patented a hydraulic binder from CKD by preliminary hydration of the partially calcined limestone in the dust. The product is used as a constituent in masonry mortar or plaster for construction purposes. The dust is drawn from the riser duct of the by-pass, and its calcined limestone fraction is hydrated to calcium hydroxide to form the principal binder component. Klemm (1980) reported the use of CKD as an accelerator for gypsum hydration to produce gypsum building materials.

Hydrated CKD has also been successfully evaluated as an anti-stripping agent in hot-mix asphaltic concrete (Klemm, 1993). Preliminary tests on replacing up to 3% hydrated lime by the hydrated CKD have shown favorable results. CKD has been used as an inorganic filler in bituminous paving and asphaltic roofing. Kiln dust has also been used as a filler for asphaltic insulating board sound-deadening materials (Davis and Hooks, 1975).

### Chemical Processing of CKD as an Alkali Source

Enriched levels of soluble alkalies (i.e.,  $K_2SO_4$ ) in CKD make it a promising raw material for the extraction of  $K_2O$  or its soluble salts. A number of patents have been issued on the subject, most of which require aqueous dissolution of soluble potassium salts that are later removed as a saleable commodity and the water recovered for reuse. The potassium-free dust is usually recycled as kiln feed. Studies pertinent to this approach have been reported by Dean (1972), Singleton and Bruce (1975), McCord (1977), Klemm (1980), Fernandez Lozano and Silva (1985), and Wolfe (1992) with modifications of their own.

Dean (1972) recovered a substantial amount of alkali salts from CKD by mixing it with  $H_2O$  in successive stages at temperatures between 21 to 99°C (70 to 210°F). The supersaturated solution thus produced was cooled and alkali salts crystallized and separated. Singleton and Bruce (1975) treated the dust with fresh water at elevated temperatures to essentially dissolve alkali chlorides and sulfates and subsequently remove them by crystallization. The remaining solution is carbonated to form calcium carbonates for recycling.

McCord (1977) recovered the alkalies by leaching the kiln dust at higher temperatures with an aqueous solution of KCl. The extract is cooled for crystallization of KCl and removed. The washed CKD is reclaimed for use as kiln feed. Klemm (1980) proposed the separation of alkalies as K.SO, from the high-alkali dust (~13% K<sub>O</sub>) for agricultural purposes. The K,SO, was extracted by mixing CKD with hot water followed by filtering, cooling the aqueous brine, and K,SO, crystallization. The remaining material can then be reused as raw feed substitute. A yield of more than 86% was reported by lowering the pH with carbon dioxide, thus preventing the formation of the double salt of K and Ca sulfates known as syngenite. Fernandez Lozano and Silva (1985) removed potassium and K.SO, from the CKD with water in a batch leaching tank by vigorous stirring and reported a 92% K,O separation.

Wolfe (1992) reported the usefulness of leaching to remove alkali from CKD to facilitate recycling both fresh CKD and CKD stockpiled over the years. Tests on the stockpiled CKD showed that more than 80% alkali ( $K_2O$ ) was removable by using ordinary tap water with or without additives at ambient temperature. Almost 100% more alkali was removed from stockpiled CKD than from the fresh CKD. A preferred process flowsheet (Figure 2) was proposed to remove alkalies from both the stockpiled and fresh CKD and reuse the residue as kiln feed. The process incorporated water leaching, pressure filtration, and evaporation as unit operations.

Another approach, proposed by Wilson and Anable (1986), is the removal of alkalies by pyrotreatment of pelletized dust. Here, the  $K_2O$  is volatilized in the presence of  $SO_3$  by heating the dust above 1300°C (2372°F) in a reducing atmosphere generated by coal addition. Figure 3 shows the removal of potassium under reducing conditions. In order to enhance volatilization, CaCl<sub>2</sub> or CaF<sub>2</sub> was sometimes added. The resulting low-alkali residues were used in producing cement of adequate engineering characteristics.

Earlier, Klemm (1980) reported that high-alkali kiln dusts could be fused to separate  $K_2SO_4$  as liquid. Several operational difficulties were cited, however. First, although  $K_2SO_4$  in the dust has a melting point of 920°C (1688°F), the dust itself had to be melted beyond 1400°C (2552°F) to volatilize  $K_2SO_4$  and needed to be separated from the fused dust. Second, the  $K_2SO_4$  is reactive and fuses with ceramics, and third, the  $K_2SO_4$  fumes tend to react with the furnace heating elements and eventually inhibit their proper functioning.

#### **Applications as a Fertilizer**

Because of the high lime (for acid neutralizing capacity) and potassium concentrations, CKD has already found use as a fertilizer in many parts of the world. This use of CKD is only recently being realized in the United States. If properly developed, however, the market for agricultural lime and potash fertilizer could become large enough to consume the bulk of the CKD that is currently being discarded.

Risser et. al. (1981) produced a lime-potash soil additive composed of 35% CaO, 6% MgO, 5% K<sub>2</sub>O, and 4% SO<sub>3</sub> from CKD having a controlled composition. The high pH of CKD provides neutral soils a greater efficiency of herbicides; whereas the potassium satisfies the plant withdrawal requirements. Fraiman et. al. (1991) recommended the use of bypass dust containing high levels of K<sub>2</sub>O, SO<sub>3</sub> and Cl, in fertilizer applications. Since potassium is the most valuable fertilizer element contained in the dust and the least desirable element for recycling, CKD with high potassium contents could be adequately utilized as fertilizers.

Taylor (1987) also reported the usefulness of CKD as a substitute for lime and fertilizer elements, which covers a large reserve for nutrients. Since the quality of CKD varies with each cement plant, however, the nutrient value may also change. Baker et. al. (1975) developed nonputrescible soil-like products for general agricultural applications by combining CKD with sewage sludge before vacuum filtering.

One of the concerns with using CKD as a fertilizer substitute is the level of heavy metals it may contain, especially if the CKD is produced from coal-fired kilns. Their effect on the food chain through possible extraction by soil and subsequent movement into vegetation should be determined before such applications are to be considered. However, in a specific study on the use of CKD as a fertilizer in Iowa, Preston (1993) demonstrated that heavy metals in CKD are well below the permissible levels for land application. Furthermore, the overall heavy metal content in the CKD also appears to be within the range found naturally in soils across North America (Dragun, 1991).

In addition to establishing the biological safety, other agricultural factors such as crop yield, variation of soil quality with lime, liming efficiency of CKD (when used either as powder or pellets), and dusting problems (during storing or handling) must also be considered. Nutrients such as nitrogen and phosphorus are still required from other sources.

Other related applications for CKD are its use as cattle and dairy feed additives (Ward et. al., 1979; Wheeler et. al., 1977, 1979). The alkali-buffering nature of CKD appears to have a positive effect on ruminant nutrition for cattle. Steers fed with a diet containing CKD showed improved average daily gain compared to the control group. Again, the level of trace metals should be carefully determined before CKD is used as an animal food supplement (Bush and Nicholson, 1985).

#### **Applications in Waste Treatment**

CKD has been used as a substitute for lime in stabilizing waste-water streams. This is possible primarily because of the high neutralizing potential of the CKD (high CaCO<sub>3</sub> and CaO) and fine particle size distribution, having Blaine finenesses often greater than 800  $m^2/kg$ . Up to a 35% addition of CKD has satisfactorily met the specified pathogen control level in sewage sludge. High pH, an exothermic reaction, and the resulting accelerated drying when CKD was added were the factors mainly responsible for the pasteurizing effects on municipal waste-water sludge (Nicholson, 1988; Burnham, 1987; Nicholson and Burnham, 1988).

Burnham and Bennett (no date) produced an easyto-handle granular soil-like material by mixing CKD with the sludge cake in a pugmill. This material, termed an advanced, stabilized, dewatered sludge, was subjected to secondary thermal treatment from the exothermic heat generated by further CKD addition, and by maintaining pH 12 and a temperature between 50-60°C (120-140°F) for 12 hours. The resulting material was a stabilized, environmentally compatible, saleable commodity.

Anglebeck (1987) applied CKD for alkali control in sewage sludge where it could respond to the stabilizing needs should the character of the sludge change. Due to its high pH and liming potential, CKD also absorbed residual odor from the sludges. In some cases where unbalanced sewage treatments result in an acidic and highly odorous sludge that may be simply trucked to landfills, the CKD could aid in neutralizing the sludge for proper handling and stabilization.

As mentioned earlier, Baker et. al. (1975) used CKD as an aid for vacuum filter processing of sewage sludge on site. The report showed that CKD was at least equal to hydrated lime for sewage processing and could be superior if used at a rate one- to three-times greater than that normally used for lime. Potassium and magnesium in the CKD will add further benefits if the resulting sludge-cake were to be used as a nutrient for crop production. The economic benefits and energy savings from using CKD instead of hydrated lime are obvious.

CKD has also been used to purify waste water contaminated with 500-1000 ppm of zinc, manganese, copper, and cobalt (Salem, 1990). The treatment required 2%-30% of CKD per liter of waste water, and involved absorption and purification of metal hydroxides and carbonates. CKD has also been partially or totally substituted for lime in preparing the alum floc as a coagulant for removing turbidity from water (Farnham, 1960). The dust not only neutralized the water but also improved the flocculation by providing abundant nucleation sites for alum flocs.

CKD use has also been reported in a number of solidification/stabilization projects, primarily in remedial actions, and central hazardous waste management facilities. The dust functions primarily as an absorbent or bulking agent (Conner, 1990). A recent paper by MacKay and Emery (1992) describes the stabilization of contaminated soils and sludges in which CKD is used in conjunction with other cementitious products such as slag cement, lime kiln dust, flyash, hydrated lime, and portland cement. The CKD-fly ash process developed by Nicholson (1978, reissue 1982), is applicable to sewage sludge solidification, but appears to be equally appropriate for other wastes.

Another possible application of CKD is in wet scrubber slurry used for adsorbing  $SO_2$  from stack gases, where hydrated lime or limestone slurries are currently being used. Studies have indicated that the kiln dust functioned better than the limestone and almost as good as lime (Gorman, 1972). Fur-

thermore, the scaling problems with scrubbers using kiln dust were less severe than those using a lime slurry. Murdock (1993) has reported the use of a bypass dust as a suitable sorbent in capturing SO<sub>2</sub> in wet scrubbers. Owing to the finer particle distribution, a reactive CaO phase, and the presence of Mg and Na as promoters, the bypass dust exceeded the capture efficiency of standard limestone sorbents. Desulfogypsum scrubber sludge resulting from the stack gas scrubbing was suggested as a viable sulfate source for use in portland cements to control early hydration reactions.

As mentioned earlier, in a similar process by Young and Morrison (1991), an aqueous slurry of fresh CKD is used for scrubbing SO<sub>2</sub> from the kiln exit gases. This also results in the carbonation of lime in the slurry; the alkali and sulfur compounds are subsequently crystallized from cooling the hot brine. The leached CKD is safely recycled as kiln feed. Potassium sulfate is the principal product that is continuously removed from the system and may be sold as an industrial or agricultural chemical. In a recent report Young (1993) has also indicated the capture of HCl and CO<sub>2</sub> from the flue gases using CKD scrubbing. The subsequent products are a fertilizer for land application and a residue for reuse as kiln feed.

#### Applications in Mining and Metallurgical Industry

U.S. Bureau of Mines studies (Haynes and Kramer, 1982) have documented the use of CKD as a partial hydraulic filler for backfilling coal mine shafts and tunnels. Such an application alone can potentially utilize large volumes of CKD. Because of its fine particle size and high alkali contents, CKD is also being premixed to neutralize acidic media and effluent from mining and mineral processing industries. For instance, Sodyes (Klemm, 1980) used CKD to neutralize a chemical pond containing acidic sulfates. The attempts were only partially successful because the particular CKD used was very coarse. The dust also has the potential to replace fly ash for controlling the spread of fires in coal mines.

CKD has also been used as a binder in pelletizing iron ore fines for recycling in steel making. It has also found applications as coagulant for dewatering of waste sludge from tin rolling mills (Klemm, 1980).

#### **Miscellaneous Applications**

Cement kiln dust has also been used as a partial replacement for soda in the production of glass where color and high chemical stability are not essential considerations. High alkalies in CKD increase the rate of sulfate decomposition that is the main cause of foaming in glass baths (Emer, 1969). A soda-kiln-dust glass has many similarities to the conventional sodalime glass. Fraiman et. al. (1991) have also recommended the use of bypass dust in glass making.

In some Eastern European countries, kiln dust has been successfully incorporated into cementing compositions for gas and oil wells. The kiln dust appears to improve slurry pumpability and also functions as a fluid-loss additive. CKD also sufficiently retarded oil well cement slurries for use at temperatures up to 100°C (212°F), without additional retarders.

Other uses for CKD are based on its fine particle size and high absorptive capacity. It has been used as a decolorizing agent in the clarification and purification of sugar solutions. No information is available, however, on the level of impurities the dust might have contributed to the solution it was clarifying (Klemm, 1980). The U. S. Environmental Protection Agency has studied the use of quicklime or CKD in stabilizing soils contaminated with polychlorinated biphenyls (PCBs). It appears, however, that PCB's apparent loss was the result of evaporation and steam stripping at elevated temperatures (Einhaus et. al., 1991) rather than decomposition.

Kiln dusts containing small amounts of NaCl can be added to oily waste water to absorb oil, forming a sludge that can be easily removed. This technique also appears to be applicable for removing oil contamination from inland rivers or even oil slicks and spills at sea. McCants (1952) patented a process for converting CKD into an absorbent for cleaning up spills in garages and on roads. The product was claimed to be useful as a filter medium for oil clarification and also as a decontaminating agent for areas where poisonous liquids and chemicals have been sprayed or spilled.

Kiln dust may have applications as an absorbent for the removal of SO<sub>x</sub> emissions from industrial stack gases. For such uses, the dust is prepared in a porous but granulated or pelletized form to avoid contributing to particulate emissions.

#### Land Disposal of CKD

A series of investigations were conducted by CTL for land disposal applications of CKD (Todres et. al., 1992; and Todres, 1992). The report showed that, depending upon their physical and chemical composition, and after appropriate moisture adjustments, the dusts were conveniently compacted under medium compaction, to dense and extremely low permeability masses matching those of silt and fine sandstone. Heavy compaction produced an almost impervious mass comparable to clay. To verify the laboratory data under field conditions, follow-up compaction studies were conducted using a double drum vibratory roller. The objective was the eventual disposal of CKD as compact landfill, pavement, or subbase material. Based on the measured permeabilities of Shelby tube samples, an estimated density of 105% of the standard Proctor maximum was obtainable. This corresponds to a permeability coefficient of  $2.3 \times 10^{6}$  cm/s.

Studies have also been carried out to use CKD as a water-tight barrier (liner) for sanitary landfill sites (Ballivy and Breton, 1992). The dust could be consolidated and stabilized when used in conjunction with varying amounts of fly ash (Class C) and silica fume. The mixes had a water to dry-solid ratio of 0.4 and were cured at 100% relative humidity for 10 days after demolding. After consolidation the mixes showed permeability lower than the standard  $10^{-7}$  cm/sec. When tested as liners, these mixes exhibited a good capacity for absorbing heavy metals.

#### CONCLUSIONS

Most of the CKD removed from kiln exhaust gases by dust collectors is recycled as kiln feed whenever possible. However, the bulk of the waste CKD—that which is not recycled as kiln raw feed—is landfilled, and the rest is consumed in other industries as a raw material or a by-product based on its specific physical and chemical characteristics.

The physical and chemical make up of CKD depends upon the raw kiln feed and the type of cement operation. Generally, the dusts are particulate materials composed of partially calcined feed enriched with alkalies and other volatiles. Because of the diversity of their composition and the associated economical and environmental priorities, the use of CKD can best be considered on a plant-toplant basis.

The predominant factor preventing the recycling of CKD in cement manufacturing is the high alkali content that may produce clinkers exceeding the required Na<sub>2</sub>O equivalent limit. Preferential leaching has been employed to remove alkalies and reuse "washed" residue as kiln feed. Several techniques for removing alkalies and recycling the residue, most of which are still at pilot scale, have also been described in the literature.

When CKD cannot be recycled in cement manufacturing, the second best solution is its industrial use, based on a specific physical and chemical nature. The relevant properties of CKD are particle size, chemical reactivity (because of the partially calcined limestone and free lime contents), and alkali content. Quantitatively, these characteristics depend largely on the specifics of the production process.

Since finely divided calcium carbonate is its principal component, CKD can be used as a minor ingredient in blended cements and non-standard cementitious compositions. In certain cases, the addition of fly ash or blast furnace slag might be required to offset the elevated alkali levels. Although the results vary with the composition, the general outcome appears promising. For that reason, CKD has, for example, been used in making masonry blocks.

The chemical reactivity of CKD and its fineness can also be used in a number of applications for solidification/stabilization systems and neutralization of industrial wastes such as sewage sludges, acid waste streams, and stack gases. CKD is also a useful binder in stabilizing subbases for pavement. In such applications, fly ash is sometimes also needed.

The relatively high potassium content of some dusts makes them usable as low-grade fertilizers and additives for acidic soil conditioning. The market for agricultural lime and potash fertilizers appears promising and could consume a large quantity of CKD. A somewhat related application of CKD is also reported as a food supplement for dairy animals. A common concern is the presence of trace quantities of heavy metals, which must not enter the food chain at higher than permissible levels.

Aqueous extraction or other chemical processing of CKD can yield saleable products such as potassium sulfate salts. The treated CKD may be subsequently recycled as kiln feed. A number of processes are available for such extractions. CKD slurries are also being used in SO<sub>x</sub> scrubbing from cement kiln stack gases that subsequently lead to crystallization of K<sub>2</sub>SO<sub>4</sub> as a marketable product.

Miscellaneous applications of CKD also include: glass making, mine-backfilling, and oil and acid spillage control.

Depending upon their physical and chemical compositions, CKDs can also be compacted in landfills after appropriate moisture adjustment. This can result in dense beds with low permeabilities matching those of clay, and thereby reducing the potential pollution caused by rainfall or run-off water.

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Kiln operation type	Range of dust production (% of clinker produced)
Wet	10-25
Semi-dry/semi-wet	0-3
Dry	7-15

## Table 1. Production of Cement Kiln Dusts from Different Operation Types (Müller, 1977)

# Table 2. Typical Composition of Cement Kiln Dust<br/>(Haynes and Kramer, 1982)

Constituent	% by weight	Constituent	% by weight
CaCO <sub>3</sub>	55.5	Fe2O3	2.1
SiO2	13.6	ксі	1.4
CaO	8.1	MgO	1.3
K₂SO₄	5.9	Na₂SO₄	1.3
CaSO₄	5.2	KF	0.4
Al <sub>2</sub> O <sub>3</sub>	4.5	Others	0.7

# Table 3. Composition of CKDs from Different Operation Types(Todres et. al., 1992)

Constituent	Dust G (wt. %) long-wet kiln	Dust H (wt. %) long-dry kiln	Dust S (wt. %) alkali bypass
SiO₂	15.02	9.64	15.23
Al <sub>2</sub> O <sub>3</sub>	3.85	3.39	3.07
Fe <sub>2</sub> O <sub>3</sub>	1.88	1.10	2.00
CaO	41.01	44.91	61.28
MgO	1.47	1.29	2.13
SO3	6.27	6.74	8.67
Na₂O	0.74	0.27	0.34
K₂O	2.57	2.40	2.51
LOI	25.78	30.24	4.48
Free CaO	0.85	0.52	27.18

CKD component	Mineralogical compositions
Unreacted raw feed	Carbonates
	Quartz
	Others (clay minerals, Fe/AI oxides)
Partially calcined feed and clinker dust	Decomposed raw feed
	Clinker minerals
	Intermediate phases
Free lime	CaO,
	Ca(OH)2
Alkali salts and other volatile compounds	KCI, 2NaCI, (K/Na)2SO4,
	CaSO4

# Table 4. Typical Mineralogical Compositions of Selected CKDs (Müller, 1977)

### Table 5. Mean Particle Size of the Returned and Discarded CKDs(Müller, 1977)

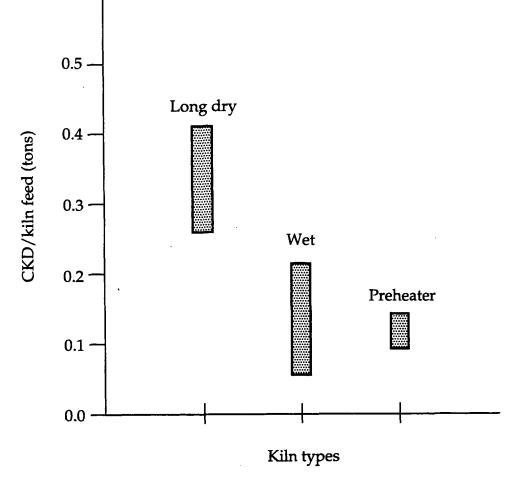
Kiln operation type	Returned CKD Mean particle size (μm)	Discarded CKD Mean particle size (µm)		
Wet process	15	12		
Semi-dry/semi-wet process	31	34		
Dry process	3	11		

### Table 6. Size Distribution and Mean Particle Size of the CKDs(Todres et. al., 1992)

Type of kiln operation	>100 (µm)	<45 (μm)	<30 (μm)	<7 (μm)	<0.6 (μm)	Mean (µm)
Long-wet process	5.0	85.0	77.3	43.0	7.5	9.3
Long-dry process	0.0	99.2	98.8	87.2	5.6	3.0
Bypass operation	2.0	84.5	66.0	14.0	2.0	22.2

RCRA and BIF metals	Average TCLP (mg/kg)	RCRA limits (mg/kg)
Antimony	0.012	1.0
Arsenic	0.066	5.0
Barium	1.04	100.0
Beryllium	0.004	0.007
Cadmium	0.0288	1.0
Chromium	0.10	5.0
Lead	0.349	5.0
Mercury	0.0018	0.2
Nickel	0.13	70.0
Selenium	0.152	1.0
Silver	0.07	5.0
Thallium	0.38	7.0

# Table 7. Levels of Trace Metals in CKDs (PCA, 1992)





r,

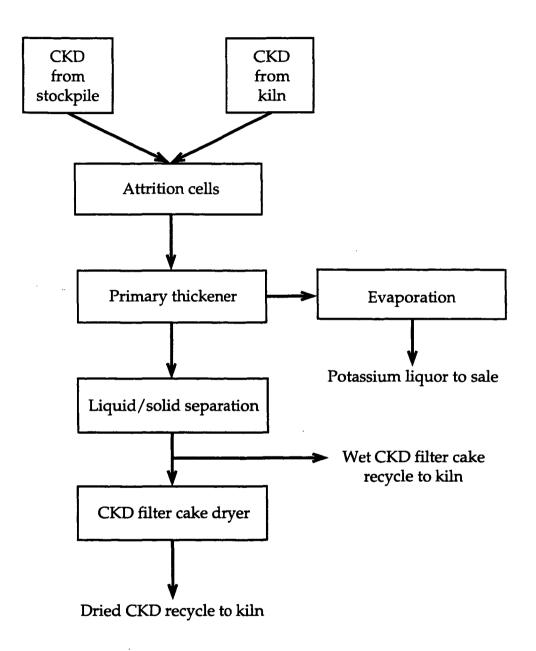
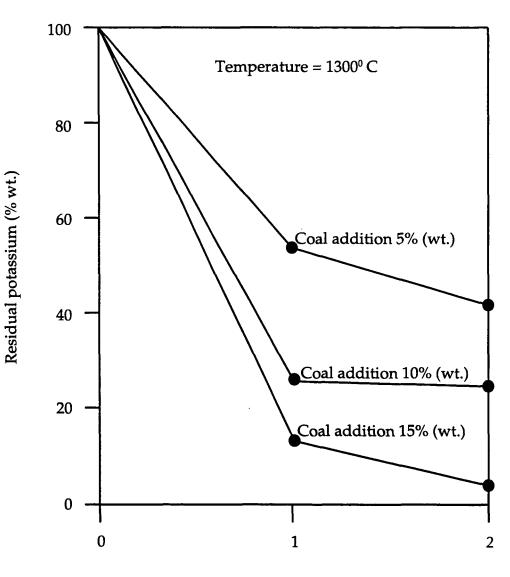


Figure 2. Flowsheet of the preferred process for alkali removal from CKD and recycling as kiln feed (Wolfe, 1992).



Time (hours)



### Metric conversion table

Following are metric conversions of the measurements used in this text. They are based in most cases on the International System of Units (SI).

1 in	= 25.40 mm
1 sq in	= 645.16 mm2
1 ft	= 0.3048 m
1 sq ft	= 0.0929 m2
1 sq ft per gallon	= 0.0245 m2/L
1 gal	= 3.785 L
1 kip = 1000 lbf	= 4.448 kN
1 lb	= 0.4536 kg
1 lb per cubic yard	= 0.5933 kg/m3
1 psf	= 4.882 kg/m2
1 psi	= 0.006895 MPa
No. 4 sieve	= 4.75 mm
No. 200 sieve	≃ 75 mm
1 bag of cement (U.S.)	= 94 lb = 42.6 kg
1 bag of cement (Canadian)	= 88 lb = 40 kg
1 bag per cubic yard (U.S.)	= 55.8 kg/m3
deg. C	= (deg. F - 32)/1.8

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An organization of cement manufacturers to improve and extend the uses of portland cement and concrete through market development, engineering, research, education, and public affairs work.

### **APPENDIX II**

### COMPREHENSIVE SOLID WASTE MANAGEMENT PLAN REVIEW CHECKLIST

### APPENDIX A

COMPREHENSIVE SOLID WASTE MANAGEMENT PLAN, PART I Review Checklist

PLAN CONTENTS	YES	<u>NO</u>	INCOMPLETE
Identification of Responsible Agencies	$\checkmark$		
Advisory Committee			
Identification of members Description of role, activities Documents reviewed Meeting dates, locations			 
Public Hearings or Meetings			
Date, location of hearing/mtg. #1 Date, location of hearing/mtg. #2			NIA NIA
Evidence of Cooperation			
Letters from all local governments			NIA
Description of Planning Area			
Locations of existing facilities Population centers Transportation routes Climate			NIA
Natural, historic, archeological features		<u> </u>	
Agency jurisdictions	$\checkmark$		
<u>Description of Previous Planning</u> <u>Activities</u>	$\checkmark$		
State Volume Reduction Goals			
Report of waste stream, 7/1/88 Changes in pop., employment,	$\checkmark$	- <u></u>	
industry production since 7/1/88	<u> </u>		- <u> </u>
Waste Generation, Composition Analysis			
List of all industries in area Analysis of waste generation, comp.			~ NIA

For each option: Materials Public education Est. % of waste stream diverted Present activities Environmental impacts Costs/revenues Recommendations	YES VVV VVV	<u>NO</u>		NIA NIA NIA NIA
5. <u>Sanitary Landfills</u>				
Description of options	<u> </u>			NIA
For each option: Siting, locations				A/A
Transportation routes, costs				1-11
Capital costs	<u>·</u>			
Present available space				
Groundwater monitoring costs				
Financial assurances				$\checkmark$
Environmental impacts				
For new landfills or expansions:	,			
Plant and animal analyses	$\checkmark$		·	
Archeological, historical,				
architectural analyses				
Proposed Integrated Mgnt. System	$\checkmark$		. <u></u>	
Comparative Cost Analyses	·		·	NIA
Implementation Plan and Schedule Proposed activities, strategies for				
each applicable alternative For each alternative:	$\checkmark$	<u> </u>	·	
Reason for decision				
Methods to be used	$\checkmark$		·	
Timelines w/ yearly milestones	,		·	
Proposed locations of activities Estimated costs	<u> </u>		·	NIA
Organizations proposed to implement				
activities				
Public education strategies, methods			- <u></u>	NIA
Financial commitment				AIN
				1 - 1 - 1

NIA - NOT APPLICABLE

#### APPENDIX B: INTEGRATED MANAGEMENT SYSTEM COST ANALYSIS FIRST YEAR COST BREAKDOWN

For each of the management methods analyzed, a clear list of the costs associated with that method should be made. Reference to the section of the plan that analyzes the particular option (both method and specific costs) should be made. The assumptions that apply to the cost analysis should be clearly stated and attached to the list.

The following is an example of the information that should be included in the individual management method cost analysis. Subtotals of the various costs and/or revenues will be entered in the comparative cost analysis.

MANAGEMENT METHOD: NOT APPLICABLE (text reference)

Capital Costs:

1) 2) 3)	Building and Equipment Land	Construction		
	Subtotal Annual Cost	(include inte	rest)*	
<b>Operatio</b>	n Costs:			
1) 2) 3) 4)	Salaries Utilities Maintenance Other			
	Subtotal			
Transpor	tation Costs:	·		
1) 2)	Collection Haul		<u> </u>	
	Subtotal			
Revenues	:			
Total Me	thod Cost:			
List of	Assumptions as	sociated with	this analys	sis:

\* Annual cost for capital expenditures must include principal, annual percentage rate, and the number of years required to repay the loan.